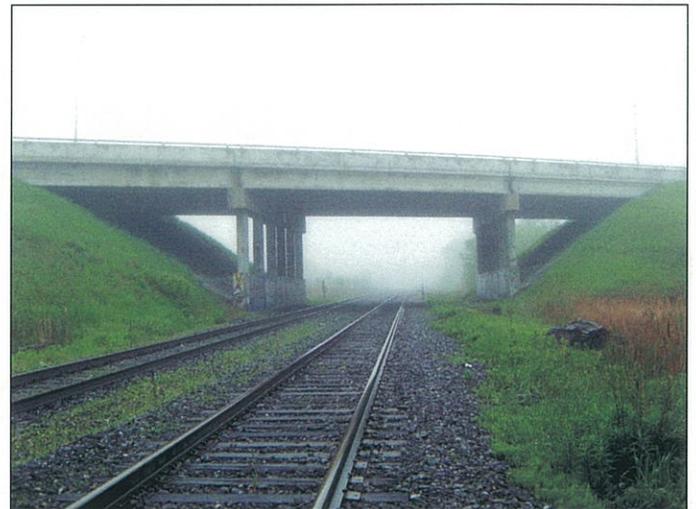
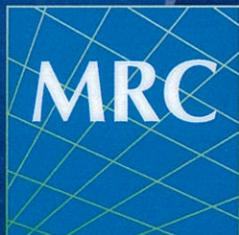

APPENDIX F2
CNR OVERHEAD BRIDGE STRUCTURAL EVALUATION REPORT 2009

**Dundas Street (Reg. Rd. 5)
Class EA Study
Brant Street (Reg. Rd. 18)
to Proudfoot Trail**



**CNR Overhead Structure
Dundas Street over CN Railways
Bridge No. 005108
MTO Site No. 010-0175**

STRUCTURAL EVALUATION REPORT



A member of  **MMM GROUP**

*Global
Transportation
Engineering*

November 2009

STRUCTURAL EVALUATION REPORT

CNR OVERHEAD STRUCTURE DUNDAS STREET OVER CN RAILWAYS CITY OF BURLINGTON, ON REGIONAL MUNICIPALITY OF HALTON MTO SITE NO. 10-175



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Trevor Small, M.Sc., P.Eng
Senior Project Manager



McCormick Rankin Corporation

A member of  MMM GROUP

October 2009

TABLE OF CONTENTS

| | Page |
|--|----------|
| 1. INTRODUCTION..... | 1 |
| 2. EXISTING CONDITIONS | 1 |
| 2.1 2003 Rehabilitation..... | 2 |
| 2.2 2006 Bi-Annual Bridge Appraisal | 2 |
| 3. ANALYSIS AND EVALUATION ASSUMPTIONS..... | 3 |
| 4. LOADING | 4 |
| 5. ANALYSIS / MODELLING..... | 4 |
| 5.1 Introduction..... | 4 |
| 5.2 Analysis Results..... | 5 |
| 6. BARRIER WALL..... | 6 |
| 7. DISCUSSION & RECOMMENDATIONS..... | 6 |

APPENDICES

| | |
|--------------|--------------------------------|
| APPENDIX 'A' | KEY PLAN & STRUCTURAL DRAWINGS |
| APPENDIX 'B' | SITE PHOTOGRAPHS |
| APPENDIX 'C' | ANALYSIS RESULTS |

1. INTRODUCTION

McCormick Rankin Corporation (MRC), a member of MMM Group, was retained by the Regional Municipality of Halton to undertake a Municipal Class Environmental Assessment (EA) for the planned widening of Dundas Street from the existing four lanes to six lanes. The study limits for the widening are from Guelph Line to Appleby Line. The CNR Overhead Structures are within the study limits and will also need to be widened to accommodate the planned increase in the number of traffic lanes.

A structural investigation of the bridges are included in the Municipal Class EA to assess the feasibility of bridge widening alternatives, existing bridge needs, and quantity of repairs required for cost analysis of the alternatives. The investigation comprised the structural evaluation and a detailed deck condition survey. This report focuses on the bridge structural evaluation. Details of the results of the condition survey may be found in the report "Dundas Street - CNR Overhead Structure, Site Number 010-0175, Bridge Deck Condition Survey Report" by MRC dated October 2009, which is bound separately.

This report includes the following:

- A summary of the rehabilitation work previously carried out;
- Results of the structural evaluation;
- Review of the barrier wall currently in place; and
- Discussions of findings from the structural evaluation.

A Key Plan showing the structure location is provided in Appendix A.

Appendices containing supplementary information such as drawings, photographs, figures, and calculations, are referenced throughout the text and included in the back of this Report.

2. EXISTING CONDITIONS

Two adjacent, yet independent, CNR Overhead bridges were constructed in 1962, one for Waterdown-bound traffic and the other for Toronto-bound traffic. Each bridge carries two (2) traffic lanes located along Dundas Street (King's Highway No.5), which crosses over the CN Railways. The superstructure layout follows along the Profile Control Line and comprises three simply-supported spans of precast, pre-stressed concrete girders supporting a cast-in-place (CIP) reinforced concrete deck, an asphalt wearing surface, and a PL2 concrete barrier wall with traffic railing and a median barrier on each deck edge. The two adjacent decks, each 11.431m wide, are separated by a 25mm longitudinal joint located between the medians.

The three spans are each 12.2± m, 17.8± m, and 12.2± m in length, supported by piers and abutments that are skewed relative to the Profile Control Line, in order to accommodate the rail lines passing underneath the bridges. Approach slabs, each 4.267m

long, flank both ends of the bridges. General views of the structure are shown in photographs found in Appendix B.

In 2003, the structure was rehabilitated. More recently, bi-annual appraisals have been carried out on the bridge. Summaries of the work and findings are presented.

2.1 2003 Rehabilitation

In 2003, the structure was rehabilitated under Contract No. R-1853B-2003. The scope of work included the following:

- Removed deteriorated concrete from deck soffit & diaphragm ends and repaired
- Removed deteriorated concrete from pier caps and repaired
- Constructed new concrete crash walls on pier columns
- Repaired concrete slope paving
- Removed traffic railings, steel beam guide rails, curbs and gutters. Removed north and south edges of approach slab.
- Installed new concrete barriers & steel beam guide rails. Modified existing approach slabs by placing new curb and gutter.
- Removed existing caulking/seal from longitudinal expansion joint
- Installed new longitudinal expansion joint
- Milled existing pavement and place surface course asphalt
- Reinstated pavement markings
- Installed asphaltic plug seals at abutment and pier expansion joints

2.2 2006 Bi-Annual Bridge Appraisal

The 2006 bi-annual was completed by TSH for the Regional Municipality of Halton. The following summarizes the findings of their inspection:

- The asphalt wearing surface is in good condition.
- Concrete barrier walls and steel barrier rails are in good condition with surface rust stains noted.
- Concrete median is in generally good condition with localized cracking.
- A longitudinal expansion joint in the median is sealed and is in poor condition. Localized leakage was noted.
- Deck expansion joints are paved over and are in poor condition with leakage noted.
- Concrete deck soffit is in good condition with localized water staining along the deck fascias at piers and longitudinal expansion joint. Localized patching was noted on both the south and north deck cantilever. Localized spalling and delaminations were

noted along longitudinal joints. Exposed corroded rebar chains were also noted along joint.

- Precast concrete girders are in generally good condition with delaminations and spalling of several girders at the support points.
- Elastomeric bearing pads are in good condition.
- Concrete piers are in generally good condition with extensive water staining, localized cracking and patching of the pier caps. The pier columns are in good condition. Railway crash walls are in good condition.
- Concrete abutments are in good condition with extensive water staining and localized vertical cracking.
- Concrete wingwalls are in good condition.
- Slope paving is in good condition.
- Steel beam guiderail and channel on the bridge approaches are in good condition with extruder end treatments complete with hazard markers in all four quadrants.
- Concrete approach slabs are in good condition
- Asphalt paved approach roads are in good condition.
- Raised concrete median on the approaches is in generally good condition.
- Concrete curb and gutter on the approaches are in good condition
- Asphalt paved boulevards are in good condition

3. ANALYSIS AND EVALUATION ASSUMPTIONS

The following points should be considered when reviewing this report:

- The structure was evaluated in accordance with the Canadian Highway Bridge Design Code, CAN/CSA-S6-06 (CHBDC), using the software program CANBAS Version 2.0.1 to determine girder demands and capacities.
- The structure was evaluated using Ultimate Limit States (ULS) with load combination factors provided in CHBDC, Table 3.1.
- CIP deck slab and AASHTO Type III girder properties were calculated based on their gross (un-cracked) section properties. The structure was evaluated based on the assumption that any and all defects have been repaired.

The following assumptions were made throughout the evaluation:

- The reinforcing steel material properties were estimated based on considering the date of bridge construction in accordance with Clause 14.7.4.4 of CHBDC. The assumed yield strength, F_y , and elastic modulus, E , of the original rebar was taken as 275 MPa and 200 GPa, respectively [Table 14.2 of CHBDC].
- According to the structural drawings, the concrete compressive strengths were:
 - 34.5 MPa for the pre-stressed girders
 - 27.6 MPa for the CIP concrete deck

4. LOADING

The dead load contributors are as follows:

- Pre-stressed girder self-weight
- 177.8 mm thick CIP deck slab

Superimposed dead load contributions include:

- 76.2 mm thick asphalt plus waterproofing
- barrier walls and curbs

Other loads include:

- Pre-stressing axial forces on girder strands

The structural drawings found in Appendix A were used to determine loads. Standard material densities in accordance with CHBDC were used.

The CNR Overhead is required to carry vehicle trains in normal traffic, for which the governing live load model is the CL1-ONT-625 Truck [CHBDC, S6.1-06 Commentary, Cl. C3.8.1].

5. ANALYSIS / MODELLING

5.1 Introduction

The bridge analysis was performed using the structural analysis program CANBAS Version 2.0.1. Interior and exterior pre-stressed beams were analysed to determine load demands and capacities along each girder.

The resistance of the members or “Capacity” (C) have been calculated. The moment of resistance, M_r , and shear resistance, V_r , of each member is calculated based on its gross (un-cracked) sectional properties in accordance with CHBDC.

Capacity-to-demand (C/D) ratios are calculated for exterior and interior members at critical locations to evaluate the theoretical condition of the bridge. Throughout this evaluation, members with a C/D ratio less than 1.0 have been considered to be under capacity.

An evaluation check was completed to confirm the results of the above-noted evaluation calculations.

5.2 Analysis Results

The evaluation is based on the assumptions outline above. The following results at the critical sections were obtained and the results are presented in Tables 5.1 and 5.2 based on ULS loading. Interior girder C/D ratios governed in all cases. Detailed analysis results and discussions are found in Appendix C.

Table 5.1 – End Span, Interior Girder ULS Load Combination Results

| Point | Capacity / Demand Ratio ¹ | | Location ² |
|-------|--------------------------------------|-------|----------------------------|
| 1 | $M_r (+) / M_f (+)$ | 1.63 | Midspan ($x/L = 0.5$) |
| | V_r / V_f | n / a | Midspan ($x/L = 0.5$) |
| 2 | V_r / V_f | 1.35 | At Piers ($x/L = 0$) |
| | V_r / V_f | 1.27 | Near Piers ($x/L = 0.1$) |

Table 5.2 – Main Span, Interior Girder, ULS Load Combination Results

| Point | Capacity / Demand Ratio ¹ | | Location ² |
|-------|--------------------------------------|-------|----------------------------|
| 1 | $M_r (+) / M_f (+)$ | 1.37 | Midspan ($x/L = 0.5$) |
| | V_r / V_f | n / a | Midspan ($x/L = 0.5$) |
| 2 | V_r / V_f | 1.24 | At Piers ($x/L = 0$) |
| | V_r / V_f | 1.11 | Near Piers ($x/L = 0.1$) |

¹ Footnote: "Capacity/Demand Ratio" is defined as factored resistance divided by the factored response. A Demand/Capacity ratio greater than or equal to 1.0 is desirable
 $M_r (-)$ is defined as factored negative flexural resistance
 $M_f (-)$ is defined as the factored applied negative bending moment
 $M_r (+)$ is defined as factored positive flexural resistance
 $M_f (+)$ is defined as the factored applied positive bending moment
 V_r is defined as factored shear resistance
 V_f is defined as factored applied shear

² Footnote: L denotes the span length, equal to 17831mm for main spans and 12192mm for end spans.
x denotes the distance from pier supports for main spans, and abutment supports for end spans.

6. BARRIER WALL

The barrier wall currently in use was designed according to OHBDC 1991, Highway Class A. These PL-2 barriers were installed in 2003. Using information gathered from the Bi-Annual Bridge Appraisal in 2006 and the Condition Survey in 2009, it was determined that PL-2 barriers on both north and south sides are in good condition and still satisfy barrier performance level requirements in CAN/CSA-S6-06, Clause 12.4.

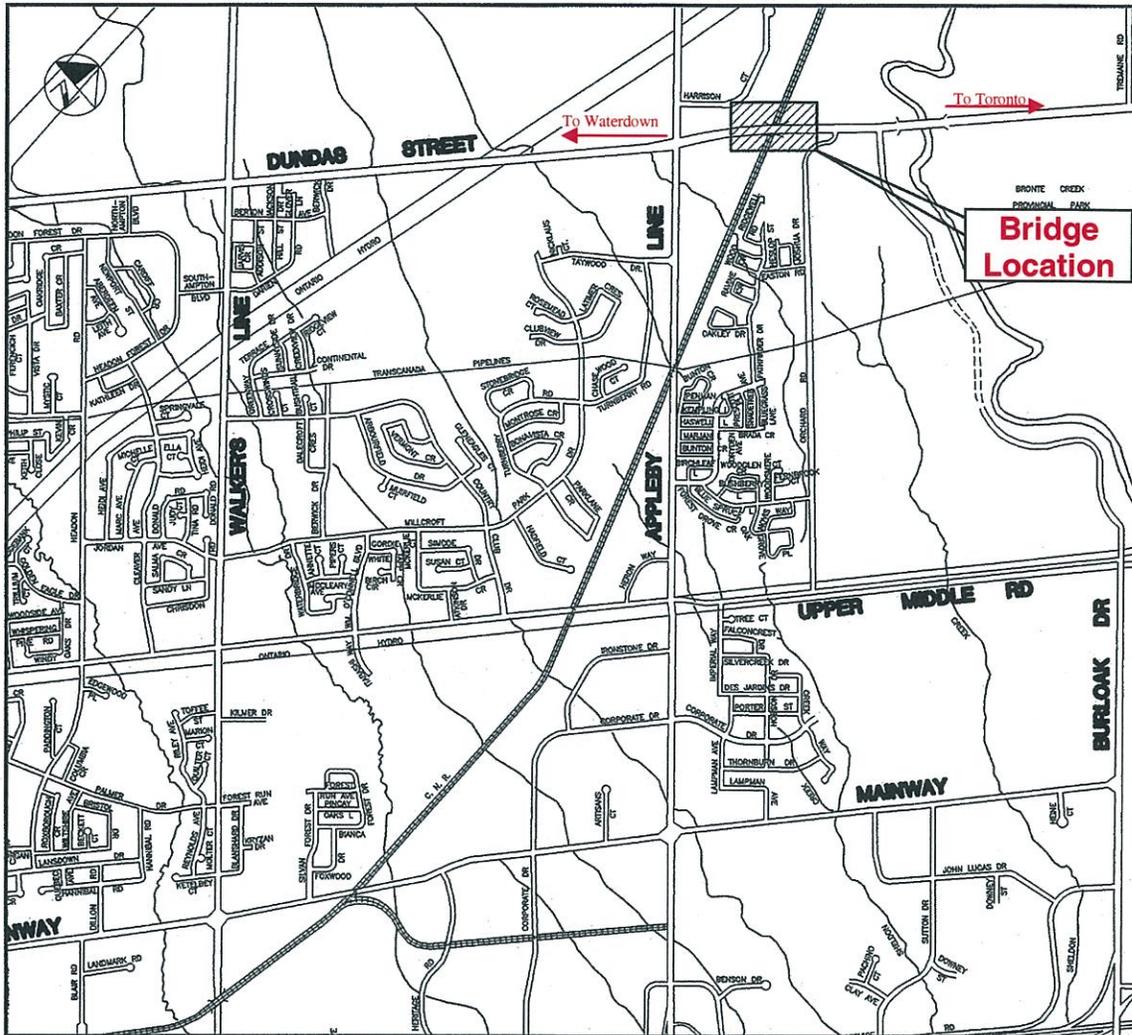
7. DISCUSSION & RECOMMENDATIONS

The results of the evaluation suggest that the CNR Overpass is theoretically adequate in bending moment and shear. Furthermore, the barrier wall currently conforms to current MTO standards and is reported to be in good condition.

The response of the structures to live load was also evaluated to determine the feasibility of increasing the concrete slab thickness from 178 mm to 225 mm with an asphalt thickness of 90 mm. Results of the analysis indicate that an increased deck slab thickness of 225 mm is feasible for the future widening of each overhead structure to carry three (3) traffic lanes.

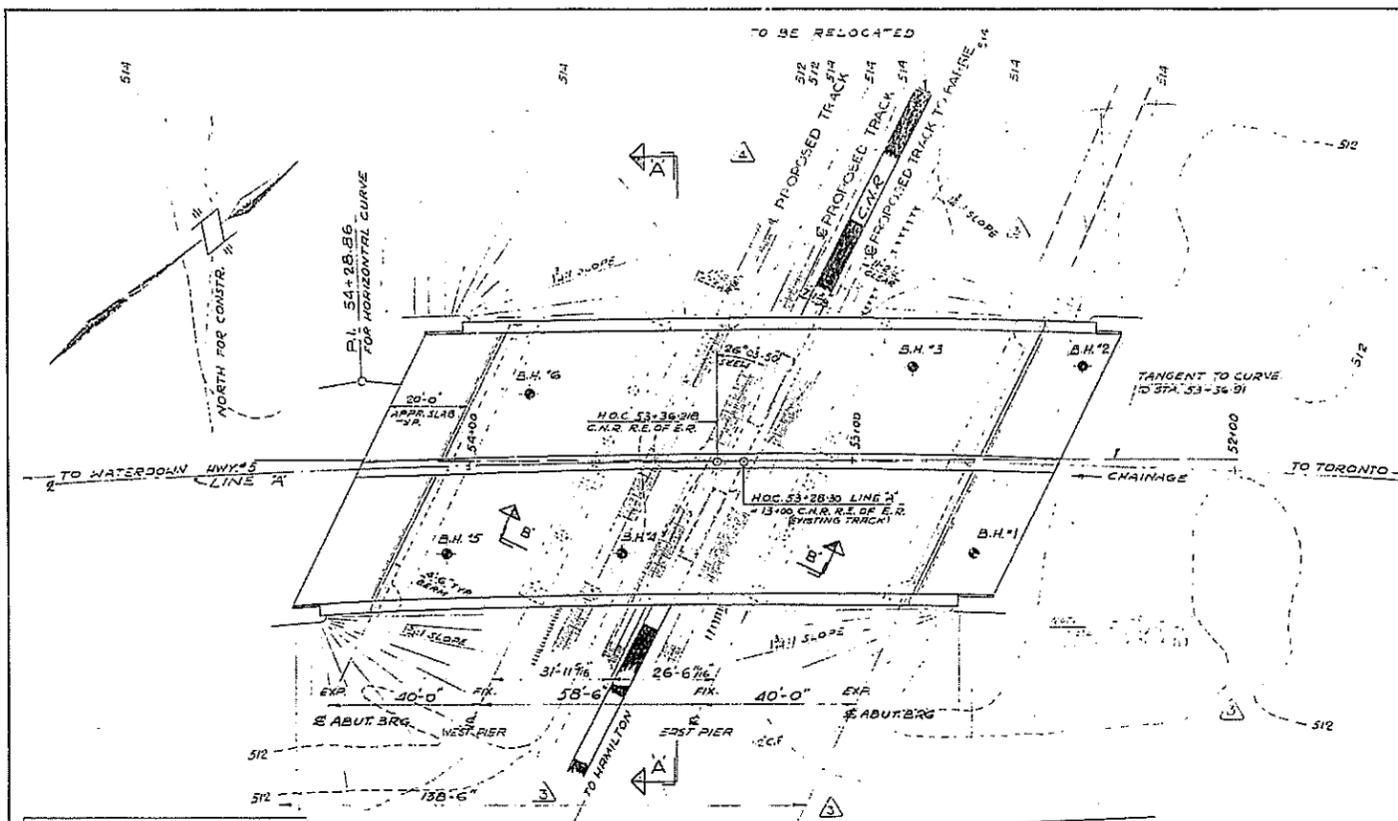
In summary, the structural evaluation found that the pre-stressed girder structures have adequate load capacity and may be incorporated into the widening of Dundas Street.

APPENDIX A
KEY PLAN & STRUCTURAL DRAWINGS



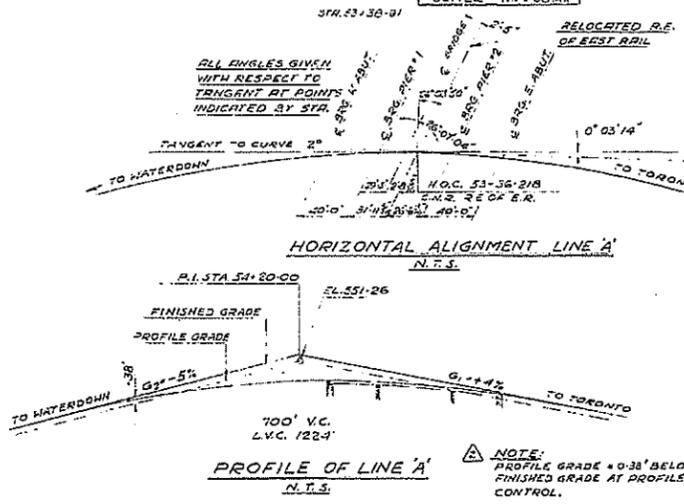
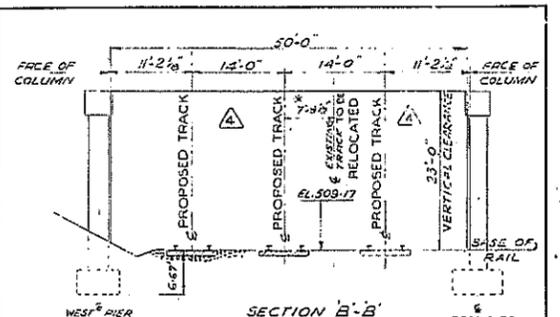
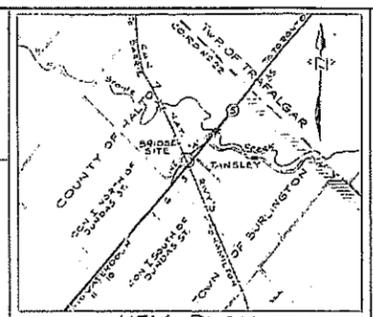
CNR Overhead Structure, Dundas Street Over CN Railways
0.50 km East of Appleby Line

KEY PLAN
N.T.S.



C.R.M. No 194 EL. 334.994
 4.175 GIRDER BRIDGE ON C.N.R. 1 1/2 MILES NORTH-EAST OF STATION AND AT MILEAGE 24.41 FROM TORONTO, 1200 FEET NORTH EAST OF R. ROAD CROSSINGS, NORTH-WEST OF NORTH STONE WINGWALL AT NORTH EAST END OF BRIDGE, TOP COURSE, SOFT SET HORIZONTALLY.
 PUBLICATION No. 13

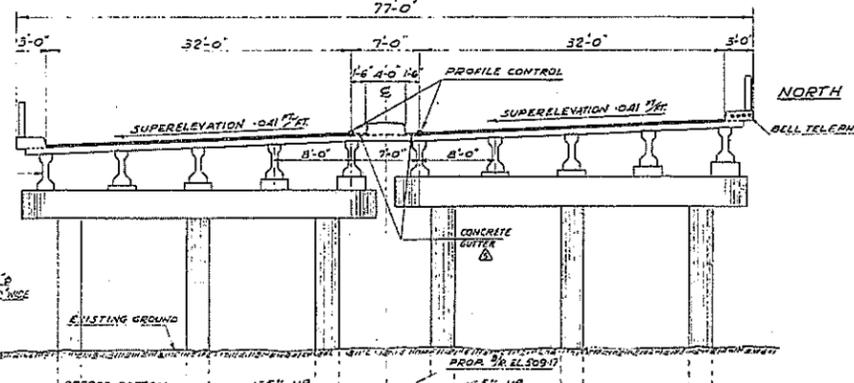
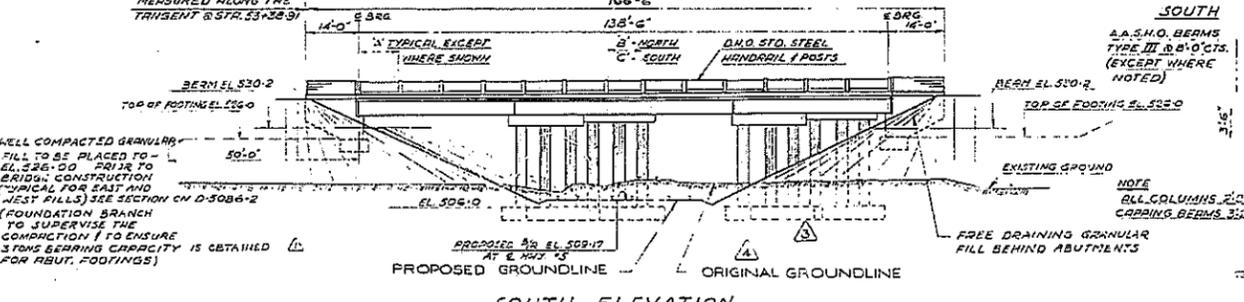
| CURVE DATA | | SPIRAL DATA | |
|--------------------------|--------------------------|-------------------------|--------------------------|
| Δ = 14° 31' | R = 2864.79 | Q ₁ = 19.45' | L ₁ = 175.00' |
| Δ _e = 11° 07' | L _c = 533.33' | Q ₂ = 19.45' | L ₂ = 453.70' |
| D = 2° 07' | E ₁ = 23.75' | | |



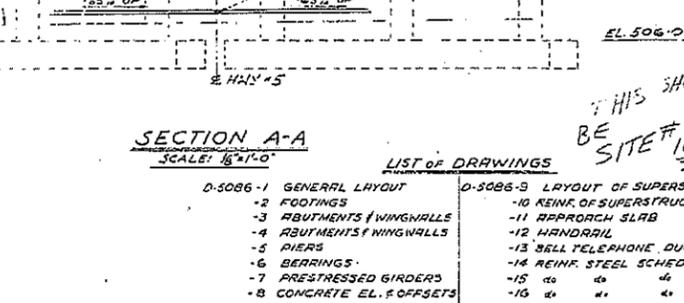
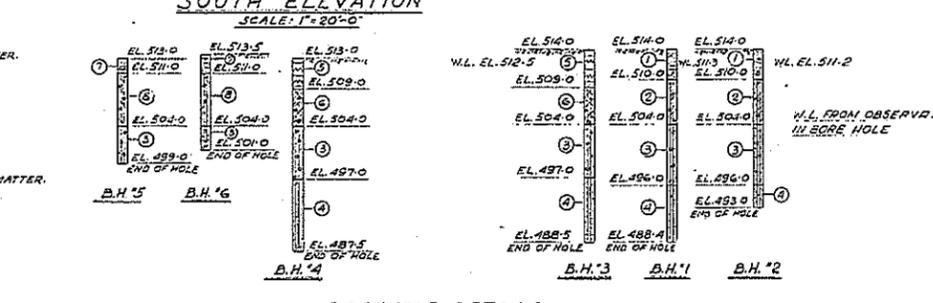
NOTES
 TO DISTRICT ENGINEER
 CONCRETE WORK ON THIS STRUCTURE MUST NOT BE COMMENCED UNTIL MONUMENTS TO FIX CONTROL POINTS HAVE BEEN ERRECTED AND CHECKED BY THE DISTRICT ENGINEER TO CONTRACTOR
 STRUCTURE TO BE BUILT IN ACCORDANCE WITH FORM NO. 9 AND THE SPECIAL PROVISIONS, EXTRA COPIES OF WHICH MAY BE OBTAINED FROM THE DISTRICT ENGINEER.
 CONCRETE MIX 3000 P.S.I. OF AGGREGATE
 PRESTRESSED BEAMS 5000 P.S.I. MAX. SIZE 3/4"
 DECK 4000 P.S.I. 3/4"
 REMAINDER APPROVED ADMIXTURES SUPPLIED BY THE CONTRACTOR WILL BE ADDED TO ALL CONCRETE AS SPECIFIED BY THE ENGINEER.
 BORING DATA
 THE COMPLETE SOIL INVESTIGATION REPORT FOR THIS STRUCTURE MAY BE EXAMINED AT THE BRIDGE OFFICE AND FOUNDATION OFFICE, DOWNSVIEW, AT ANY REGIONAL OFFICE AND AT THE HAMILTON DISTRICT OFFICE. THE DEPARTMENT DOES NOT GUARANTEE THE ACCURACY OF THIS REPORT OR THE ABBRIDGED VERSION SHOWN ON THESE PLANS.
 CLEAR COVER ON REINFORCING STEEL
 FOOTINGS 3"
 PIER CAPS 3"
 PIER COLUMNS 3"
 DIAPHRAGMS OR AS NOTED 3"
 DECK SLAB 2"
 HANDRAILS END POST 2"
CONSTRUCTION NOTES
 ALL EXPOSED EDGES TO BE CHAMFERED 1/4" EXCEPT AS NOTED.
 ALL CONSTRUCTION JOINTS MUST BE APPROVED BY THE BRIDGE ENGINEER.
 THE GENERAL CONTRACTOR IS RESPONSIBLE FOR FINISHING THE BRIDGE SEATS DEAD LEVEL TO THE SPECIFIED ELEVATIONS WITH A TOLERANCE OF PLUS OR MINUS 1/8 INCH. IF THEY ARE CAST TOO HIGH THEY SHALL BE GRINDING DOWN BY THE GENERAL CONTRACTOR. IF THEY ARE CAST TOO LOW THE GENERAL CONTRACTOR SHALL PROVIDE FULL BEARING SHIMS TO BRING THEM UP TO THE CORRECT ELEVATIONS.
 THE GENERAL CONTRACTOR SHALL BE RESPONSIBLE FOR ENSURING THAT THE FINAL DECK ELEVATIONS CONFORM WITH THE ELEVATIONS SHOWN.
 NO CONCRETE SHALL BE PLACED ABOVE THE BRIDGE SEAT UNTIL EPOXY RESIN TO BE SUPPLIED BY G.M.C. AND APPLIED BY CONTRACTOR.
 GRANULAR FILL
 THE COMPACTION OF GRANULAR FILL UNDER BOTH ABUTMENT FOOTINGS TO BE SUPERVISED BY G.M.C. FOUNDATION BRANCH

HANDRAIL

| No. of PANELS | MARK | LENGTH OF PANEL (EXC. TO EDGE OF POST) |
|---------------|------|--|
| 24 | A | 10'-0" |
| 1 | B | 11'-1 1/2" |
| 1 | C | 11'-11 1/2" |



- RECORD OF BOREHOLES**
- SAND WITH GRAVEL AND ORGANIC MATTER. LOOSE - BROWN.
 - CLAYEY-SILT WITH SAND AND GRAVEL. VERY STIFF BROWN.
 - SILTY-SAND WITH GRAVEL. VERY DENSE BROWN.
 - SANDY-SILT. VERY DENSE BROWN.
 - RAILWAY-FILL CONDENSED WITH ORGANIC MATTER. DENSE - BLACK.
 - CLAYEY-SILT WITH SAND AND GRAVEL. VERY STIFF TO HARD BROWN.
 - TOP SOIL. LOOSE - BROWN.
 - CLAYEY-SILT WITH SAND AND GRAVEL. HARD - BROWN.



TWR# 133-175

DEPARTMENT OF HIGHWAYS ONTARIO
 BRIDGE DIVISION

C.N.R. OVERHEAD
 (2.5 MI. WEST OF E. JCT. OF HWY. 25)

KING'S HIGHWAY No. 5 DIST. No. 4
 CO. HALTON
 TWP. TOWN OF BURLINGTON INT. 445 CO. 1405

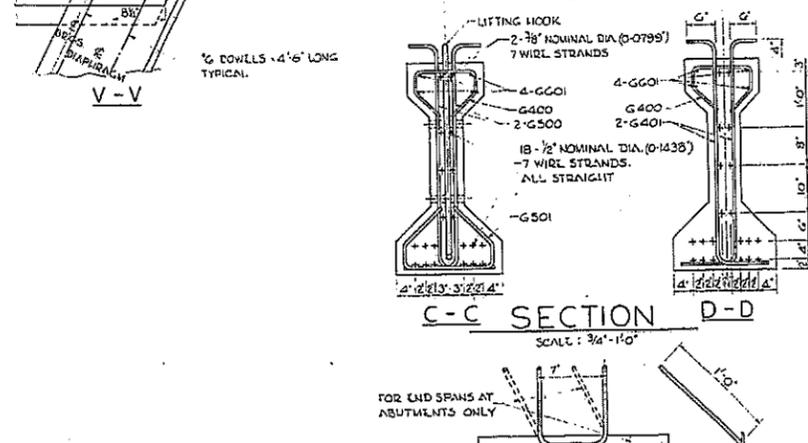
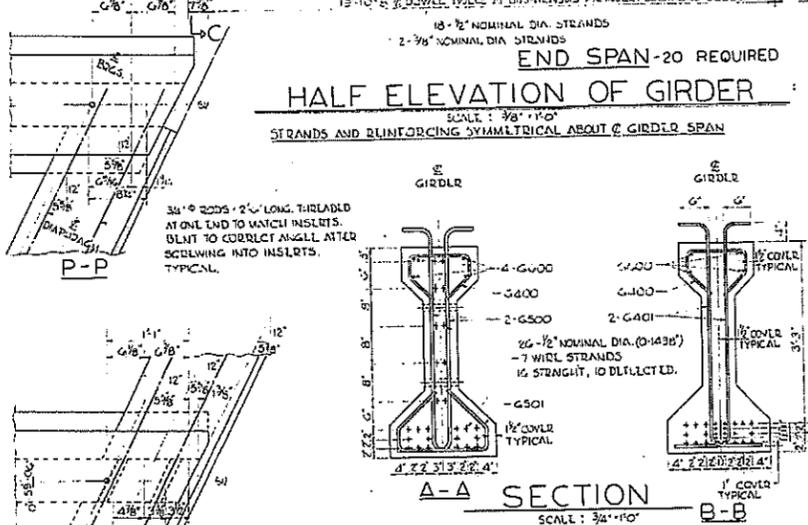
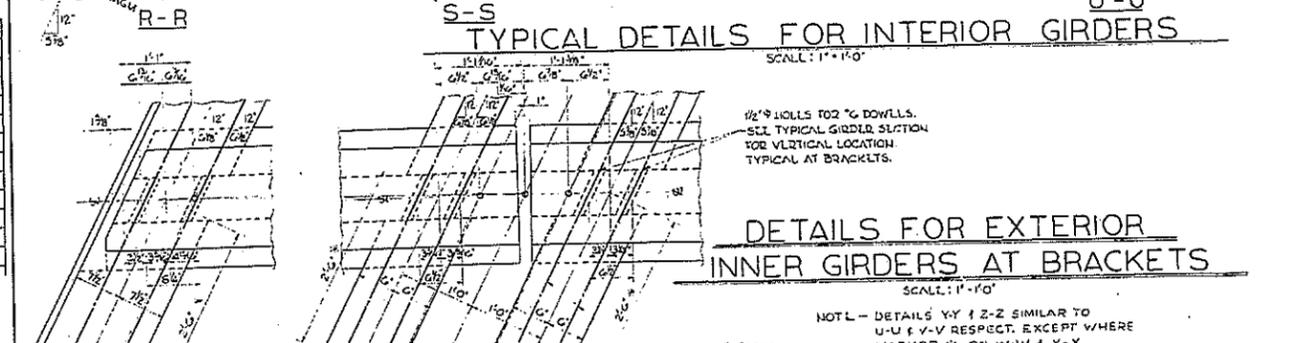
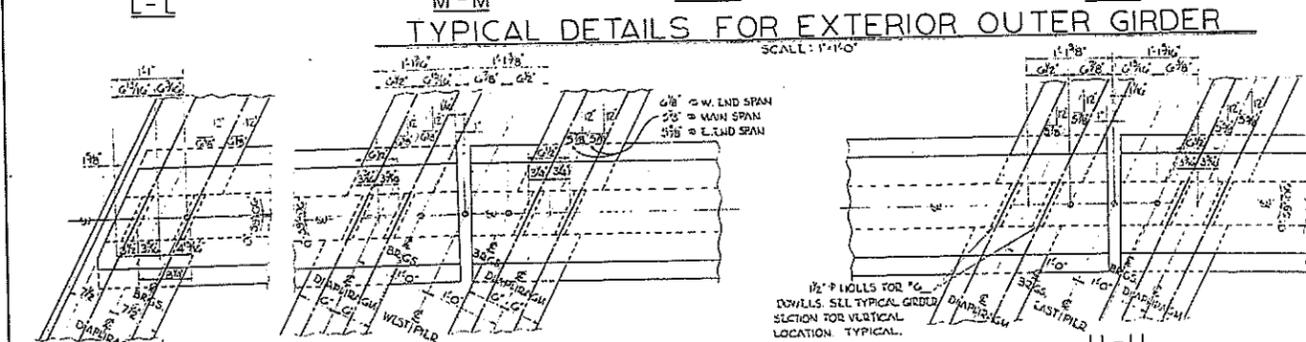
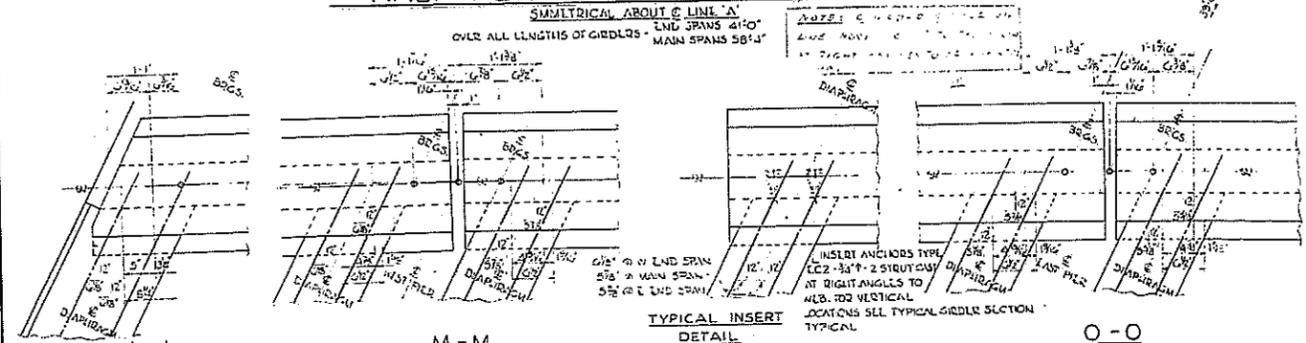
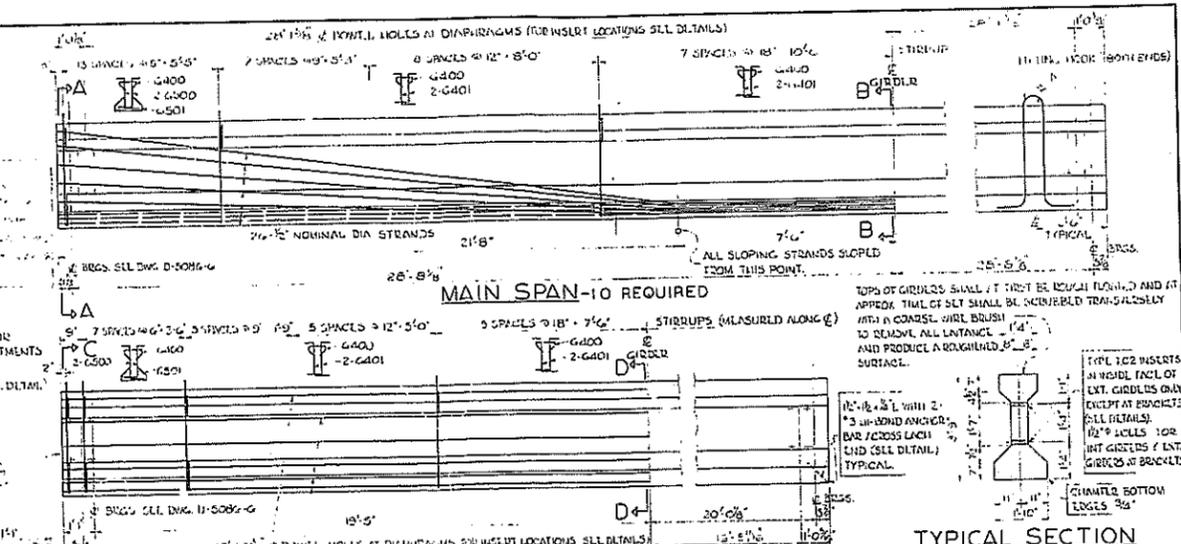
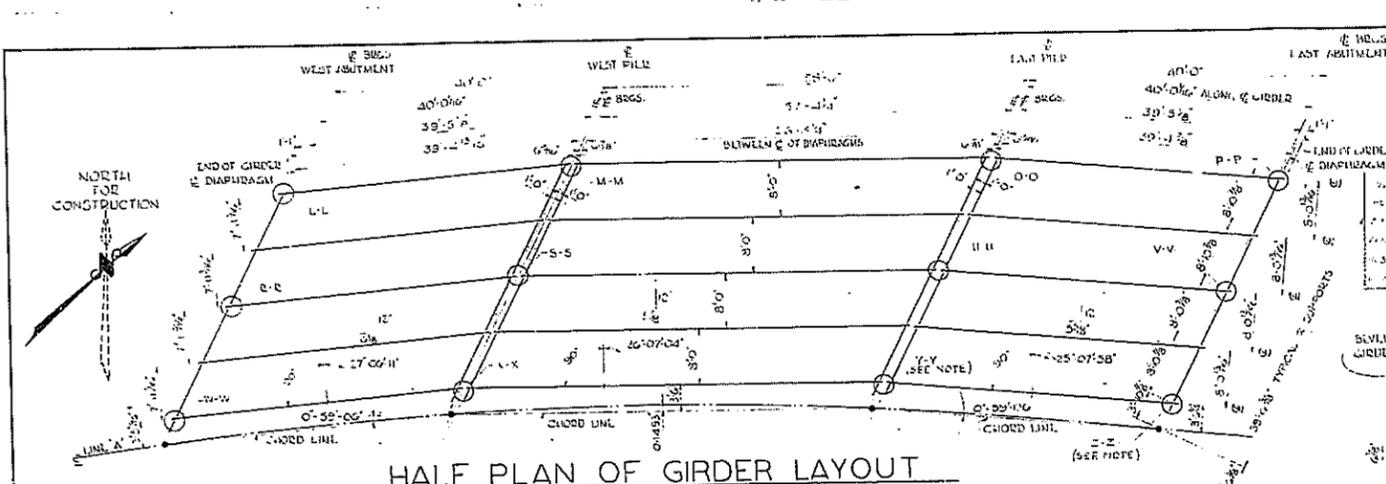
GENERAL LAYOUT

| DESIGN | CHECK | DATE | CONTRACT | NO. |
|--------|--------|--------|----------|-------------------------------|
| A.L. | J.M.R. | 11-175 | | 249-1 |
| G.P. | | | | 63-2, 63-4, 63-6, 63-8, 63-10 |

DATE: Nov. 1962
 LOADING: H 20, S 16
 DRAWING No. D-5086-1

PRINT RECORD

| No. | FOR | DATE |
|-----|--|------|
| 1 | 2, 26, 4, 7, 11, 12, 13, 14, 15, 16, 17, 18, 19, 20, 21, 22, 23, 24, 25, 26, 27, 28, 29, 30, 31, 32, 33, 34, 35, 36, 37, 38, 39, 40, 41, 42, 43, 44, 45, 46, 47, 48, 49, 50, 51, 52, 53, 54, 55, 56, 57, 58, 59, 60, 61, 62, 63, 64, 65, 66, 67, 68, 69, 70, 71, 72, 73, 74, 75, 76, 77, 78, 79, 80, 81, 82, 83, 84, 85, 86, 87, 88, 89, 90, 91, 92, 93, 94, 95, 96, 97, 98, 99, 100 | |



- NOTES**
- WORKING FORCE FOR GIRDER AFTER ALL LOSSES INCLUDING THOSE DUE TO CREEP AND SHRINKAGE OF CONCRETE AND COLLAP OF STEEL SHALL BE:
 FOR MAIN SPAN - 26 + 18.27 + 506.22 KIPS
 FOR END SPANS (18 + 19.39) (2-10-78) - 370.58 KIPS
 THE TOTAL LOSS IN STEELS IN PRESTRESSING STEEL SHALL BE ASSUMED TO BE
 FOR MAIN SPAN - 35,000 P.S.I.
 FOR END SPANS - 28,000 P.S.I.
 - CONCRETE STRENGTH AT 28 DAYS 5,000 P.S.I., 4,000 P.S.I. AT TIME OF STRAIN RELEASE.
 - PRESTRESSING STEEL - SEE ENCL. FORM NO. 9 AND SPECIAL PROVISIONS.
 - ANCHOR INSERTS FOR 3/4" DOWELS SHALL BE CAPABLE OF DEVELOPING FULL STRENGTH OF DOWELS. 3/4" DOWELS FOR EXTERIOR GIRDERS SHALL BE BURIED AT ONE END TO MATCH INSERTS. ALL DOWELS AND INSERTS SHALL BE SUPPLIED AND SET (OR GRouted) BY THE PRESTRESSED CONCRETE CONTRACTOR.
 - ENDS OF STRANDS SHALL BE BURIED AND GROUND FLUSH WITH THE GIRDER END AND PAINTED WITH ROOFING ASPHALT OR COAL TAR.
 - GIRDERS MUST BE MAINTAINED HORIZONTAL AND IN AN UPRIGHT POSITION AT ALL TIMES. THEY SHALL BE HANDLED ONLY BY MEANS OF THE LIFTING HOOPS WHICH ARE PROVIDED AT ENDS.
 - CAMBER - GIRDER SOFT TO BE CAST STRAIGHT.
 - NON-PRESTRESSED REINFORCING SHALL BE INTERMEDIATE OR STRUCTURAL GRADE III-BOND.
 - ALL GIRDER ENDS ARE TO BE CUT STRAIGHT.
 - ALL GIRDERS ARE A.A.S.I.C. TYPE III.
 - PRESTRESSED CONCRETE CONTRACTOR TO GRout ALL 1/2" HOLES IN INTERIOR GIRDERS AFTER REINFORCING FOR DIAPHRAGMS HAVE BEEN PLACED. DOWEL HOLES IN GIRDERS MAY BE PLACED AT 3/8" 12" BEVEL.

| REVISIONS | NO. | DATE | DESCRIPTION |
|-----------|-----|------|-------------|
| | | | |
| | | | |

TWP# 1337-175-7-1A

DEPARTMENT OF HIGHWAYS ONTARIO
 BRIDGE DIVISION

C.N.R. OVERHEAD
 2.5 MILES WEST OF THE JUNCTION OF HIGHWAY No. 25

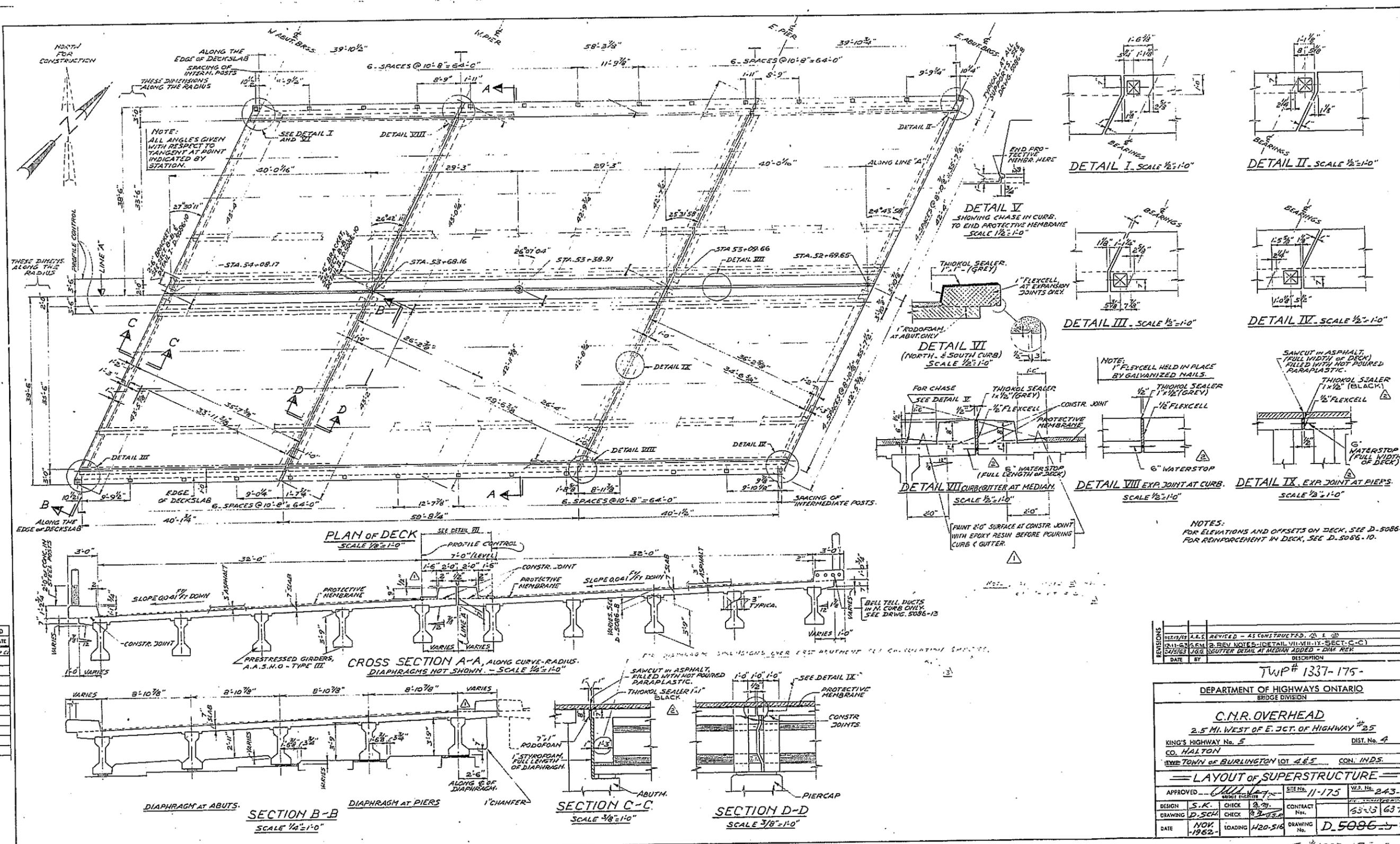
KING'S HIGHWAY No. 5 DIST. No. 4
 CO. MANTON
 TWP. TOWN OF BURLINGTON LOT 4 C 5 CON. INDS.

— PRESTRESSED GIRDERS —

| | | | | | |
|----------|-----------|---------|--------|----------|-------------|
| APPROVED | DESIGNER | DATE | 11-175 | W.P. No. | 243-61 |
| DESIGN | S.K. | CHECK | 1/1/71 | CONTRACT | 63-33 63789 |
| DRAWING | J.H.I. | CHECK | 3/2/68 | NO. | 63-33 63789 |
| DATE | NOV. 1962 | LOADING | SIG | DRAWING | D-5086-7 |

PRINT RECORD

| No. | FOR | DATE |
|-----|------|------|
| 3 | 10-4 | 1962 |
| | | |
| | | |



NOTE:
ALL ANGLES GIVEN
WITH RESPECT TO
TANGENT AT POINT
INDICATED BY
STATION.

DETAIL I. SCALE 1/2"=1'-0"

DETAIL II. SCALE 1/2"=1'-0"

DETAIL III. SCALE 1/2"=1'-0"

DETAIL IV. SCALE 1/2"=1'-0"

DETAIL V (NORTH & SOUTH CURB)
SCALE 1/2"=1'-0"

DETAIL VIII EXP. JOINT AT CURB.
SCALE 1/2"=1'-0"

DETAIL IX. EXP. JOINT AT PIERS.
SCALE 1/2"=1'-0"

NOTE:
1" FLEXCELL HELD IN PLACE
BY GALVANIZED NAILS.

NOTES:
FOR ELEVATIONS AND OFFSETS ON DECK, SEE D. 5086-B
FOR REINFORCEMENT IN DECK, SEE D. 5086-10.

| PRINT RECORD | | |
|--------------|-----|------|
| No. | FOR | DATE |
| 3 | 20 | 1962 |

| REVISIONS | | DATE | | BY | | DESCRIPTION | |
|-----------|---|------|--|----|--|-------------|--|
| 1 | REVISED - AS CONSTRUCTED | | | | | | |
| 2 | REV. NOTES - (DETAIL VII-VIII-IX-SECT. C-C) | | | | | | |
| 3 | GUTTER DETAIL AT MEDIAN ADDED - DIM. REV. | | | | | | |

TWP # 1337-175-

DEPARTMENT OF HIGHWAYS ONTARIO
BRIDGE DIVISION

C.N.R. OVERHEAD
2.5 MI. WEST OF E. JCT. OF HIGHWAY #25
KING'S HIGHWAY No. 5 DIST. No. 4
CO. HALTON
TWP. TOWN OF BURLINGTON LOT 4.E.5 CON. INDS.

LAYOUT OF SUPERSTRUCTURE

| | | | | | | | |
|---------|-----------|---------|---------|-------------|-----------|-----------|-------|
| DESIGN | S.K. | CHECK | D.S. | CONTRACT | No. | 63-13 | 63-18 |
| DRAWING | D.SCH | CHECK | D.S. | LOADING | 120-516 | D. 5086-5 | |
| DATE | NOV. 1962 | LOADING | 120-516 | DRAWING No. | D. 5086-5 | | |

TWP # 1337-175-9-1

APPENDIX B
SITE PHOTOGRAPHS



DECK LAYOUT



ELEVATION VIEW



UNDERSIDE VIEW



LONGITUDINAL EXPANSION JOINT

APPENDIX C
ANALYSIS RESULTS



RUN #1: END SPAN, INTERIOR GIRDER, 3 LANES LOADED

| ULS1 Results, calculated using Section 3 design load factors. | | | | | | | | | | |
|---|--------------------|--------------------|--------------------|--------------------|-------|--------------------|--------------------|--------------------|--------------------|-------|
| x/L | M _{max,f} | M _{min,f} | M _{max,R} | M _{min,R} | Mr/Mf | V _{max,f} | V _{min,f} | V _{max,R} | V _{min,R} | Vr/Vf |
| | kNm | kNm | kNm | kNm | | kN | kN | kN | kN | |
| 0.0 | | | | | | 784 | 162 | 1206 | 1206 | 1.54 |
| 0.1 | | | | | | 661 | 103 | 842 | 842 | 1.27 |
| 0.2 | | | | | | 538 | 28 | 713 | 713 | 1.33 |
| 1.0 | | | | | | 784 | 157 | 1057 | 1206 | 1.35 |
| 0.5 | 2071 | 446 | 3368 | 3368 | 1.63 | | | | | |

RUN #2: END SPAN, EXTERIOR GIRDER, 3 LANES LOADED

| ULS1 Results, calculated using Section 3 design load factors. | | | | | | | | | | |
|---|--------------------|--------------------|--------------------|--------------------|-------|--------------------|--------------------|--------------------|--------------------|-------|
| x/L | M _{max,f} | M _{min,f} | M _{max,R} | M _{min,R} | Mr/Mf | V _{max,f} | V _{min,f} | V _{max,R} | V _{min,R} | Vr/Vf |
| | kNm | kNm | kNm | kNm | | kN | kN | kN | kN | |
| 0.0 | | | | | | 779 | 159 | 1206 | 1206 | 1.55 |
| 0.1 | | | | | | 658 | 100 | 842 | 842 | 1.28 |
| 0.2 | | | | | | 536 | 26 | 713 | 713 | 1.33 |
| 1.0 | | | | | | 779 | 154 | 1059 | 1206 | 1.36 |
| 0.5 | 2057 | 436 | 3358 | 3358 | 1.63 | | | | | |

RUN #3: MAIN SPAN, INTERIOR GIRDER, 3 LANES LOADED

| ULS1 Results, calculated using Section 3 design load factors. | | | | | | | | | | |
|---|--------------------|--------------------|--------------------|--------------------|-------|--------------------|--------------------|--------------------|--------------------|-------|
| x/L | M _{max,f} | M _{min,f} | M _{max,R} | M _{min,R} | Mr/Mf | V _{max,f} | V _{min,f} | V _{max,R} | V _{min,R} | Vr/Vf |
| | kNm | kNm | kNm | kNm | | kN | kN | kN | kN | |
| 0.0 | | | | | | 977 | 223 | 1209 | 1209 | 1.24 |
| 0.1 | | | | | | 827 | 162 | 919 | 919 | 1.11 |
| 0.2 | | | | | | 669 | 66 | 773 | 773 | 1.16 |
| 0.3 | | | | | | | | | | |
| 0.4 | | | | | | | | | | |
| 0.5 | 3868 | 1031 | 5308 | 5308 | 1.37 | | | | | |

RUN #4: MAIN SPAN, EXTERIOR GIRDER, 3 LANES LOADED

| ULS1 Results, calculated using Section 3 design load factors. | | | | | | | | | | |
|---|--------------------|--------------------|--------------------|--------------------|-------|--------------------|--------------------|--------------------|--------------------|-------|
| x/L | M _{max,f} | M _{min,f} | M _{max,R} | M _{min,R} | Mr/Mf | V _{max,f} | V _{min,f} | V _{max,R} | V _{min,R} | Vr/Vf |
| | kNm | kNm | kNm | kNm | | kN | kN | kN | kN | |
| 0.0 | -75 | -127 | -1843 | -1843 | 14.50 | 994 | 236 | 1209 | 1209 | 1.22 |
| 0.1 | 1497 | 334 | 4559 | 4559 | 3.05 | 822 | 158 | 919 | 919 | 1.12 |
| 0.2 | 2552 | 628 | 4833 | 4833 | 1.89 | 665 | 63 | 773 | 773 | 1.16 |
| 0.3 | 3349 | 838 | 5105 | 5105 | 1.52 | 522 | -34 | 728 | -661 | 1.39 |
| 0.4 | 3763 | 966 | 5293 | 5293 | 1.41 | 380 | -138 | 503 | -624 | 1.32 |
| 0.5 | 3843 | 1012 | 5293 | 5293 | 1.38 | 241 | -241 | 569 | -624 | 2.36 |



CNR OVERHEAD STRUCTURE: CANBAS IKODES

CANBAS IKODE 35: Shear @ x/L=1.0 for End Span Girder (Run 9)

CL.8.9.3.11 Longitudinal reinforcement on the flexural tension side

Longitudinal reinforcement on the flexural tension side shall be proportioned so that at all sections the factored resistance of the reinforcement, taking account of the stress that can be developed in this reinforcement, is greater than or equal to F_{tt} , calculated as follows:

$$F_{tt} = \frac{M_f}{d_v} + 0.5N_f + (V_f - 0.5V_s - V_p) \cot \theta$$

where M_f and V_f are taken as positive quantities and N_f is positive for axial tension and negative for axial compression. In this equation, d_v may be taken as the flexural lever arm at the factored resistance.

CL.8.9.3.12 Longitudinal reinforcement on the flexural compression side

Longitudinal reinforcement on the flexural compression side of the section shall be proportioned so that the factored tensile resistance of this reinforcement, taking account of the stress that can be developed in this reinforcement, shall be greater than or equal to the force F_{tc} , calculated as follows:

$$F_{tc} = 0.5N_f + (V_f - 0.5V_s - V_p) \cot \theta - \frac{M_f}{d_v}$$

where M_f and V_f are taken as positive quantities and N_f is positive for axial tension and negative for axial compression.

Discussion of IKODE 35:

The pre-stressed girders do not have any longitudinal reinforcement on the flexural tension side. Check if the prestressed strands can handle F_{tt} at $x/L=1.0$:

$$\begin{aligned} F_{tt} &= 187.4[T] + 0.5 \cdot 233.1[C] + (814.4 - 0.5 \cdot 885 - 0) \cot 42^\circ \\ F_{tt} &= 70.85[T] + 413.04[T] \\ F_{tt} &= 483.89 \text{ kN [T]} \end{aligned}$$

Working force per girder after all losses including those due to creep and shrinkage of concrete of steel is 370.58 kips = 1648.42 kN. Therefore, longitudinal reinforcement on flexural tension side is not required.

The pre-stressed girders have longitudinal reinforcement on the flexural compression side. Check adequacy of longitudinal reinforcement for F_{tc} at $x/L=1.0$:

$$\begin{aligned} F_{tc} &= 0.5 \cdot 233.1[C] + (814.4 - 0.5 \cdot 885 - 0) \cot 42^\circ - 187.4[T] \\ F_{tc} &= -116.55 + 413.04 - 187.4 \\ F_{tc} &= 109.09 \text{ kN [T]} \end{aligned}$$

$$\begin{aligned} T_r &= 4(0.95)(275 \text{ MPa})(284 \text{ mm}^2) \\ T_r &= 296.78 \text{ kN} \end{aligned}$$

Therefore, longitudinal reinforcement on flexural compression side is adequate.

Lastly, since the span is simply supported, bending moment and shears should be similar at locations $x/L=0.0$ and $x/L=1.0$. Both ends of the girder are also designed to have the same number of prestressing

strands and top girder rebar. However, CANBAS does not report problems with $x/L=0.0$, rather only with $x/L=1.0$. Thus, this violation may not be valid.

CANBAS IKODE 36: Stirrup spacing = 305mm @ various locations

8.14.6 Maximum spacing of reinforcement for shear and torsion

If V_f is less than or equal to $(0.10 \phi_c f_c' b_v d_v + V_p)$ and T_f is less than or equal to $0.25 T_{cr}$, the spacing of the transverse reinforcement, s , measured in the longitudinal direction, shall not exceed the lesser of 600 mm or $0.75 d_v$.

If V_f exceeds $(0.10 \phi_c f_c' b_v d_v + V_p)$, or if T_f exceeds $0.25 T_{cr}$, s shall not exceed the lesser of 300 mm or $0.33 d_v$.

The spacing of the transverse reinforcement, s , measured in the longitudinal direction shall not exceed the lesser of

- (a) 600 mm or $0.75 d_v$ if the nominal shear stress is less than $0.10 \phi_c f_c'$; and
- (b) 300 mm or $0.33 d_v$ if the nominal shear stress equals or exceeds $0.10 \phi_c f_c'$.

The spacing of longitudinal bars for torsion distributed around the perimeter of the stirrups shall not exceed 300 mm. At least one longitudinal bar with a diameter not less than 0.06 times the spacing of the stirrups and not smaller than 15M shall be placed inside each corner of the closed stirrups. The corner bars shall be anchored in accordance with Clause 8.15.2 or 8.15.5.

Discussion of IKODE 36:

Since the girder locations in violation of CAN/CSA-S6-06, Cl. 8.14.6 have a stirrup spacing of 305 mm instead of 300 mm, it is considered a minor discrepancy and not a cause for concern.

CANBAS IKODE 40: @ $x/L=0.10$ & others, End Span, Interior Girder (Run 9)

8.9.5.1 General

A crack shall be assumed to occur along the shear plane and the relative displacement shall be considered to be resisted by cohesion and friction maintained by the shear-friction reinforcement crossing the crack.

In lieu of more detailed calculations, the shear resistance of the plane, v , may be calculated as $\phi_c (c + \mu \sigma)$, but v shall not exceed $0.25 \phi_c f_c'$ or 6.5 MPa. c and μ shall be as specified in Clause 8.9.5.2 and σ shall be as specified in Clause 8.9.5.3.

8.9.5.2 Values of c and μ

8.9.5.2.1

The following values shall be taken for c and μ in Clause 8.9.5.1:

- (a) For concrete placed against hardened concrete, with the surface clean and free of laitance but not intentionally roughened, c shall equal 0.25 MPa and μ shall equal $0.60 \lambda_1$.
- (b) For concrete placed against hardened concrete, with the surface clean and free of laitance and intentionally roughened to a full amplitude of about 5 mm and a spacing of about 15 mm, c shall equal 0.50 MPa and μ shall equal $1.00 \lambda_1$.
- (c) For concrete placed monolithically, c shall equal 1.00 MPa and μ shall equal $1.40 \lambda_1$.

The values of λ_1 shall be as specified in Clause 8.9.5.2.2.

8.9.5.2.2 Values of λ_1

The values of λ_1 shall be as follows:

- (a) normal-density concrete: 1;
- (b) semi-low-density concrete: 0.85; and

8.9.5.3 Value of σ

The value of σ in Clause 8.9.5.1 shall be calculated as follows:

$$\sigma = \rho_v f_y + \frac{N}{A_{cv}}$$

where

$$\rho_v = \frac{A_{vf}}{A_{cv}}$$

Discussion of IKODE 40:

Calculate shear resistance of the plane, v, @ x/L=0.10, End Span, Interior Girder and check for adequacy against shear stress.

$f'_c = 34.5\text{MPa}$ for prestressed girders
 $f'_c = 27.6\text{MPa}$ for deck slab

For surface intentionally roughened, $c = 0.50\text{MPa}$; $\mu = 1.00\lambda_1$
 $\lambda_1 = 1.00$ for normal density concrete

$$v = 0.75(0.50\text{MPa} + \sigma) < \min\{0.25 \cdot 0.75 \cdot 27.6\text{MPa}, 6.5\text{MPa}\} < 5.175\text{MPa}$$

$$\sigma = \rho_v f_y + N/A_{cv}$$

$$\sigma = f_y \cdot A_{vf}/A_{cv} + N/A_{cv}$$

where $f_y = 275\text{MPa}$
 A_{cv} = area of concrete resisting shear transfer = sb
 A_{vf} = area of shear friction rebar = 258 mm^2 at x/L=0.10
 v = shear resistance of shear friction plane
 N = unfactored permanent load normal to the interface area

| | |
|---------------------------------|---|
| $s = 228.6\text{ mm}$ | ω (deck slab) = 13.165 kN/m for $t = 225\text{ mm}$ |
| $b = 406.4\text{ mm}$ | ω (asphalt) = 5.157 kN/m for $t = 90\text{ mm}$ |
| $A_{cv} = 92903.04\text{ mm}^2$ | $\Sigma\omega = 18.322\text{ kN/m}$ |
| | $N = \Sigma\omega(L/2 - x)$ |
| | $N = 18.322\text{ kN/m}(12.192\text{ m}/2 - 1.2192\text{ m})$ |
| | $N = 89.35\text{ kN}$ |

$$\sigma = 275\text{MPa} \cdot 258/92903.04 + 89.35\text{kN}/92903.04\text{mm}^2$$

$$\sigma = 0.764\text{MPa} + 0.962\text{MPa}$$

$v = 0.75(0.50 + 0.764 + 0.962)\text{MPa}$
 $\therefore v = 1669.5\text{ kPa}$ @ x/L=0.10, End Span, Interior Girder, rehab. Scenario
 CANBAS results give $v = 981\text{MPa}$.

Let τ denote interface shear stress.

$$V_f = 563 \text{ kN} \text{ \{from CANBAS Run 9 results\}}$$

$$Q = (225\text{mm})(2422\text{mm})(225/2+184\text{mm}) = 1.6158 \times 10^8 \text{ mm}^3$$

$$I = 171162 \times 10^6 \text{ mm}^4$$

$$\tau = 563 \text{ kN} \times 1.6158 \times 10^8 \text{ mm}^3 / (171162 \times 10^6 \text{ mm}^4 \times 406.4\text{mm})$$

$$\therefore \tau = 1307.8 \text{ kPa}$$

$$\tau = V_f Q / (Ib) = 1276 \text{ kN} \text{ \{from CANBAS Run 9 results\}}$$

Thus, according to hand calculations, $v > \tau$, indicating that reinforcement provided for the interface shear transfer is adequate.

Run # 1, Filename: 7108.1b1
 End Span, Interior Girder, 3 lanes loaded

COMPOSITE PRESTRESSED GIRDER - ULTIMATE LIMIT STATES - FLEXURE

STAGE NUMBER = 2

THE IKODE NUMBER IS GIVEN WHEN A CODE CLAUSE IS VIOLATED.

| IKODE NO. | CODE CLAUSE | SPAN/ SEC | X/L | COMB. TABLE NO. | ULS GROUP | MAX/MIN APPLIED MOMENT (kN-m) | Mf (kN-m) | Mr (kN-m) | Mcr (kN-m) | CRACKING N.A FROM EXT.COMP FIBRE | Mr/Mf | 1.2Mcr/Mr | 1.33Mf/Mr | c/d | IKODE NOS. |
|-----------|-------------------------------|-----------|-------|-----------------|-----------|-------------------------------|-----------|-----------|------------|----------------------------------|-------|-----------|-----------|------|------------|
| 30 | 8.8.4.3 MIN. LONGITUDINAL R/F | LC/ 2 | 0.000 | CHBDC 1 | MIN | -33. | -1629. | -785. | 0.214 | 49.8 | 0.578 | 0.027 | 0.105 | 0.22 | |
| 31 | 8.8.4.5 MAX. LONGITUDINAL R/F | CHBDC 1 | MAX | CHBDC 1 | MAX | -30. | -1629. | -785. | 0.214 | 55.0 | 0.578 | 0.024 | 0.105 | 0.22 | |
| 32 | Mr/Mf < 1.0 | CHBDC 1 | | CHBDC 1 | | -33. | -1629. | -785. | 0.214 | 49.8 | 0.578 | 0.027 | 0.105 | 0.22 | |
| | | CHBDC 1 | | CHBDC 1 | | -30. | -1629. | -785. | 0.214 | 55.0 | 0.578 | 0.024 | 0.105 | 0.22 | |
| | | CHBDC 1 | | CHBDC 1 | | -33. | -1629. | -785. | 0.214 | 49.8 | 0.578 | 0.027 | 0.105 | 0.22 | |
| | | CHBDC 1 | | CHBDC 1 | | -134. | -1706. | -785. | 0.208 | 12.7 | 0.552 | 0.105 | 0.105 | 0.23 | |
| | | CHBDC 1 | | CHBDC 1 | | -30. | -1706. | -785. | 0.208 | 57.1 | 0.552 | 0.023 | 0.105 | 0.23 | |
| | | CHBDC 1 | | CHBDC 1 | | -129. | -1706. | -785. | 0.208 | 13.3 | 0.552 | 0.100 | 0.105 | 0.23 | |
| | | CHBDC 1 | | CHBDC 1 | | -33. | -1706. | -785. | 0.208 | 51.9 | 0.552 | 0.026 | 0.105 | 0.23 | |
| | | CHBDC 1 | | CHBDC 1 | | -30. | -1706. | -785. | 0.208 | 56.1 | 0.552 | 0.024 | 0.105 | 0.23 | |
| | | CHBDC 1 | | CHBDC 1 | | -134. | -1706. | -785. | 0.208 | 12.7 | 0.552 | 0.105 | 0.105 | 0.23 | |
| | | CHBDC 1 | | CHBDC 1 | | -146. | -1723. | -785. | 0.212 | 11.8 | 0.547 | 0.113 | 0.113 | 0.25 | |
| | | CHBDC 1 | | CHBDC 1 | | -40. | -1723. | -785. | 0.212 | 42.6 | 0.547 | 0.031 | 0.113 | 0.25 | |
| | | CHBDC 1 | | CHBDC 1 | | -40. | -1723. | -785. | 0.212 | 42.6 | 0.547 | 0.031 | 0.113 | 0.25 | |
| | | CHBDC 1 | | CHBDC 1 | | -45. | -1723. | -785. | 0.212 | 38.2 | 0.547 | 0.035 | 0.113 | 0.25 | |
| | | CHBDC 1 | | CHBDC 1 | | -41. | -1723. | -785. | 0.212 | 42.0 | 0.547 | 0.032 | 0.113 | 0.25 | |
| | | CHBDC 1 | | CHBDC 1 | | -146. | -1723. | -785. | 0.212 | 11.8 | 0.547 | 0.113 | 0.113 | 0.25 | |
| | | CHBDC 1 | | CHBDC 1 | | 87. | 3368. | 1611. | 0.086 | 38.8 | 0.574 | 0.034 | 0.034 | 0.10 | |
| | | CHBDC 1 | | CHBDC 1 | | 820. | 3368. | 1611. | 0.086 | 4.1 | 0.574 | 0.324 | 0.324 | 0.10 | |
| | | CHBDC 1 | | CHBDC 1 | | 500. | 3368. | 1611. | 0.086 | 6.7 | 0.574 | 0.197 | 0.197 | 0.10 | |
| | | CHBDC 1 | | CHBDC 1 | | 820. | 3368. | 1611. | 0.086 | 4.1 | 0.574 | 0.324 | 0.324 | 0.10 | |
| | | CHBDC 1 | | CHBDC 1 | | 244. | 3368. | 1611. | 0.086 | 13.8 | 0.574 | 0.096 | 0.096 | 0.10 | |

LC = LEFT CANTILEVER SECTION
 RC = RIGHT CANTILEVER SECTION
 |Mr/Mf| = ABSOLUTE VALUE OF Mr/Mf
 c/d = FACTOR DEFINED IN 8.8.4.5 ; A NEGATIVE VALUE OF c/d INDICATES Asc > As

| SPAN/ SEC | X/L | COMB. TABLE GROUP NO. | ULS | MAX/MIN APPLIED MOMENT Mf (kN-m) | (FACTORED) RESISTANCE MOMENT Mr (kN-m) | CRACKING MOMENT Mcr (kN-m) | N.A FROM EXT.COMP FIBRE C (m) | Mr/Mf | 1.2Mcr/Mr | 1.33ME/Mr | c/d | IKODE NOS. |
|--------------|-------|--------------------------------|-------|--|--|-------------------------------------|---|-------|-----------|-----------|------|------------|
| 1/ 5 | 0.200 | CHBDC 1 | 1 MIN | 178. | 3368. | 1611. | 0.086 | 18.9 | 0.574 | 0.070 | 0.10 | |
| | | CHBDC 1 | 1 MAX | 237. | 3368. | 1545. | 0.086 | 14.2 | 0.551 | 0.093 | 0.10 | |
| | | CHBDC 1 | 1 MAX | 1401. | 3368. | 1545. | 0.086 | 2.4 | 0.551 | 0.553 | 0.10 | |
| | | CHBDC 1 | 1 | 1004. | 3368. | 1545. | 0.086 | 3.4 | 0.551 | 0.397 | 0.10 | |
| | | CHBDC 1 | 1 | 1401. | 3368. | 1545. | 0.086 | 2.4 | 0.551 | 0.553 | 0.10 | |
| | | CHBDC 1 | 1 | 435. | 3368. | 1545. | 0.086 | 7.7 | 0.551 | 0.172 | 0.10 | |
| | | CHBDC 1 | 1 | 317. | 3368. | 1545. | 0.086 | 10.6 | 0.551 | 0.125 | 0.10 | |
| 1/ 5 | 0.300 | CHBDC 1 | 1 MIN | 346. | 3368. | 1498. | 0.086 | 9.7 | 0.534 | 0.137 | 0.10 | |
| | | CHBDC 1 | 1 MAX | 1780. | 3368. | 1498. | 0.086 | 1.9 | 0.534 | 0.703 | 0.10 | |
| | | CHBDC 1 | 1 | 1418. | 3368. | 1498. | 0.086 | 2.4 | 0.534 | 0.560 | 0.10 | |
| | | CHBDC 1 | 1 | 1780. | 3368. | 1498. | 0.086 | 1.9 | 0.534 | 0.703 | 0.10 | |
| | | CHBDC 1 | 1 | 572. | 3368. | 1498. | 0.086 | 5.9 | 0.534 | 0.226 | 0.10 | |
| | | CHBDC 1 | 1 | 417. | 3368. | 1498. | 0.086 | 8.1 | 0.534 | 0.165 | 0.10 | |
| 1/ 6 | 0.400 | CHBDC 1 | 1 MIN | 416. | 3368. | 1470. | 0.086 | 8.1 | 0.524 | 0.164 | 0.10 | |
| | | CHBDC 1 | 1 MAX | 1995. | 3368. | 1470. | 0.086 | 1.7 | 0.524 | 0.788 | 0.10 | |
| | | CHBDC 1 | 1 | 1679. | 3368. | 1470. | 0.086 | 2.0 | 0.524 | 0.663 | 0.10 | |
| | | CHBDC 1 | 1 | 1995. | 3368. | 1470. | 0.086 | 1.7 | 0.524 | 0.788 | 0.10 | |
| | | CHBDC 1 | 1 | 654. | 3368. | 1470. | 0.086 | 5.1 | 0.524 | 0.258 | 0.10 | |
| | | CHBDC 1 | 1 | 477. | 3368. | 1470. | 0.086 | 7.1 | 0.524 | 0.188 | 0.10 | |
| 1/ 6 | 0.500 | CHBDC 1 | 1 MIN | 446. | 3368. | 1461. | 0.086 | 7.5 | 0.520 | 0.176 | 0.10 | |
| | | CHBDC 1 | 1 MAX | 2071. | 3368. | 1461. | 0.086 | 1.6 | 0.520 | 0.818 | 0.10 | |
| | | CHBDC 1 | 1 | 1836. | 3368. | 1461. | 0.086 | 1.8 | 0.520 | 0.725 | 0.10 | |
| | | CHBDC 1 | 1 | 2020. | 3368. | 1461. | 0.086 | 1.7 | 0.520 | 0.798 | 0.10 | |
| | | CHBDC 1 | 1 | 682. | 3368. | 1461. | 0.086 | 4.9 | 0.520 | 0.269 | 0.10 | |
| | | CHBDC 1 | 1 | 497. | 3368. | 1461. | 0.086 | 6.8 | 0.520 | 0.196 | 0.10 | |
| 1/ 6 | 0.600 | CHBDC 1 | 1 MIN | 437. | 3368. | 1470. | 0.086 | 7.7 | 0.524 | 0.172 | 0.10 | |
| | | CHBDC 1 | 1 MAX | 1995. | 3368. | 1470. | 0.086 | 1.7 | 0.524 | 0.788 | 0.10 | |
| | | CHBDC 1 | 1 | 1679. | 3368. | 1470. | 0.086 | 1.7 | 0.524 | 0.788 | 0.10 | |
| | | CHBDC 1 | 1 | 655. | 3368. | 1470. | 0.086 | 2.0 | 0.524 | 0.663 | 0.10 | |
| | | CHBDC 1 | 1 | 477. | 3368. | 1470. | 0.086 | 5.1 | 0.524 | 0.258 | 0.10 | |
| 1/ 7 | 0.700 | CHBDC 1 | 1 MIN | 386. | 3368. | 1498. | 0.086 | 8.7 | 0.534 | 0.152 | 0.10 | |
| | | CHBDC 1 | 1 MAX | 1780. | 3368. | 1498. | 0.086 | 1.9 | 0.534 | 0.703 | 0.10 | |
| | | CHBDC 1 | 1 | 1419. | 3368. | 1498. | 0.086 | 1.9 | 0.534 | 0.703 | 0.10 | |
| | | CHBDC 1 | 1 | 573. | 3368. | 1498. | 0.086 | 2.4 | 0.534 | 0.560 | 0.10 | |
| | | CHBDC 1 | 1 | 418. | 3368. | 1498. | 0.086 | 5.9 | 0.534 | 0.226 | 0.10 | |
| 1/ 7 | 0.800 | CHBDC 1 | 1 MIN | 282. | 3368. | 1545. | 0.086 | 12.0 | 0.550 | 0.111 | 0.10 | |
| | | CHBDC 1 | 1 MAX | 1402. | 3368. | 1545. | 0.086 | 2.4 | 0.550 | 0.554 | 0.10 | |
| | | CHBDC 1 | 1 | 1402. | 3368. | 1545. | 0.086 | 2.4 | 0.550 | 0.554 | 0.10 | |
| | | CHBDC 1 | 1 | 1005. | 3368. | 1545. | 0.086 | 3.4 | 0.550 | 0.397 | 0.10 | |

| SPAN/ SEC | X/L | COMB. TABLE GROUP NO. | ULS GROUP NO. | MAX/MIN APPLIED MOMENT Mf (kN-m) | (FACTORED) RESISTANCE MOMENT Mr (kN-m) | CRACKING MOMENT Mcr (kN-m) | N.A FROM EXT.COMP FIBRE C (m) | 1.2Mcr/Mf | 1.33Mf/Mr | c/d | IKODE NOS. |
|--------------|-------|--------------------------------|---------------------|--|--|-------------------------------------|---|-----------|-----------|-------|------------|
| 1/ 8 | 0.900 | CHBDC | 1 | 436. | 3368. | 1545. | 0.086 | 7.7 | 0.550 | 0.172 | 0.10 |
| | | | | 318. | 3368. | 1545. | 0.086 | 10.6 | 0.550 | 0.126 | 0.10 |
| 1/ 8 | 0.900 | CHBDC | 1 | 138. | 3368. | 1610. | 0.086 | 24.5 | 0.574 | 0.054 | 0.10 |
| | | | | 821. | 3368. | 1610. | 0.086 | 4.1 | 0.574 | 0.324 | 0.10 |
| | | | | 821. | 3368. | 1610. | 0.086 | 4.1 | 0.574 | 0.324 | 0.10 |
| | | | | 501. | 3368. | 1610. | 0.086 | 6.7 | 0.574 | 0.198 | 0.10 |
| | | | | 245. | 3368. | 1610. | 0.086 | 13.7 | 0.574 | 0.097 | 0.10 |
| | | | | 179. | 3368. | 1610. | 0.086 | 18.8 | 0.574 | 0.071 | 0.10 |
| 1/ 9 | 1.000 | CHBDC | 1 | -89. | -1690. | -785. | 0.205 | 19.0 | 0.557 | 0.070 | 0.22 |
| | | | | -39. | -1690. | -785. | 0.205 | 43.0 | 0.557 | 0.031 | 0.22 |
| | | | | -43. | -1690. | -785. | 0.205 | 38.9 | 0.557 | 0.034 | 0.22 |
| | | | | -39. | -1690. | -785. | 0.205 | 43.0 | 0.557 | 0.031 | 0.22 |
| | | | | -39. | -1690. | -785. | 0.205 | 42.9 | 0.557 | 0.031 | 0.22 |
| | | | | -89. | -1690. | -785. | 0.205 | 19.0 | 0.557 | 0.070 | 0.22 |
| RC/ 9 | 0.000 | CHBDC | 1 | -8. | -1690. | -785. | 0.205 | **** | 0.557 | 0.006 | 0.22 |
| | | | | 42. | 3361. | 747. | 0.085 | 79.5 | 0.267 | 0.017 | 0.10 |
| | | | | 42. | 3361. | 747. | 0.085 | 79.5 | 0.267 | 0.017 | 0.10 |
| | | | | 38. | 3361. | 747. | 0.085 | 88.2 | 0.267 | 0.015 | 0.10 |
| | | | | 42. | 3361. | 747. | 0.085 | 79.7 | 0.267 | 0.017 | 0.10 |
| | | | | -8. | -1690. | -785. | 0.205 | **** | 0.557 | 0.006 | 0.22 |
| RC/ 9 | 1.000 | CHBDC | 1 | -43. | -1629. | -785. | 0.214 | 38.3 | 0.578 | 0.035 | 0.22 |
| | | | | -39. | -1629. | -785. | 0.214 | 42.3 | 0.578 | 0.031 | 0.22 |
| | | | | -39. | -1629. | -785. | 0.214 | 42.3 | 0.578 | 0.031 | 0.22 |
| | | | | -43. | -1629. | -785. | 0.214 | 38.3 | 0.578 | 0.035 | 0.22 |
| | | | | -39. | -1629. | -785. | 0.214 | 42.3 | 0.578 | 0.031 | 0.22 |
| | | | | -43. | -1629. | -785. | 0.214 | 38.3 | 0.578 | 0.035 | 0.22 |

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COMPOSITE PRESTRESSED GIRDER - ULTIMATE LIMIT STATES - SHEAR

STAGE NUMBER = 2

THE IKODE NUMBER IS GIVEN WHEN A CODE CLAUSE IS VIOLATED.
 VIOLATION OF CL 8.9.3.11/12 MAY NOT BE CRITICAL IF USER ENSURES THAT CL 8.9.3.10 IS SATISFIED BY PROPER REBAR DETAILING.
 N/C ---> NOT CALCULATED, STIRRUPS NOT REQUIRED AS PER CHBDC CLAUSE 8.9.1.2 FOR Vf
 CODE CLAUSE
 8.9.3.2

8.9.3.11/12
 8.14.6 NOTE: THE APPLICABILITY OF IKODES 36 & 37 FOR SOLID SLAB SECTIONS MUST BE ASCERTAINED BY THE USER.
 8.9.1.3

LC = LEFT CANTILEVER SECTION
 RC = RIGHT CANTILEVER SECTION

| SPAN/ SEC | X/L | COMB. TABLE | ULS GRP | MAX/MIN APPLIED SHEAR Vf (kN) | FACTORED SHEAR RESISTANCE Vr (kN) | STIRUP CAPACITY Vs (kN) | CONCRETE CAPACITY Vc (kN) | PRESTRESS NOMINAL COMPONENT FOR SHEAR Vp (kN) | MIN TOTAL SPACING AREA REQD Av (mm) | MAX SPACING REQD Av (mm) | IKODE NOS. |
|--------------|-------|----------------|------------|---|---|----------------------------------|------------------------------------|---|---|--------------------------------------|------------|
| LC/ 2 | 0.000 | | | | | | | | | | |
| LC/ 3 | 1.000 | | | -310. | -1206. | 1204. | 320. | 0. | 398. | 152. | 35. 600. |
| | | | | -9. | -1206. | 1208. | 326. | 0. | 398. | 152. | N/C N/C |
| | | | 1 MIN | -310. | -1206. | 1202. | 318. | 0. | 1687. | 152. | 35. 600. |
| | | | 1 MAX | -9. | -1206. | 1208. | 326. | 0. | 398. | 152. | N/C N/C |
| | | | 1 | -12. | -1206. | 1208. | 326. | 0. | 68. | 152. | N/C N/C |
| | | | 1 | -310. | -1206. | 1204. | 320. | 0. | 1685. | 152. | 35. 600. |
| 1/ 3 | | | | 236. | 1206. | 1208. | 326. | 0. | 1282. | 152. | 35. 600. |
| | | | | 166. | 1206. | 1208. | 326. | 0. | 902. | 152. | 35. 600. |
| | | | 1 MIN | 1206. | 1206. | 1208. | 326. | 0. | 882. | 152. | 35. 600. |
| | | | 1 MAX | 1206. | 1206. | 1032. | 176. | 0. | 4267. | 152. | 35. 300. |
| | | | 1 | 227. | 1206. | 1208. | 326. | 0. | 1238. | 152. | 35. 600. |
| | | | 1 | 236. | 1206. | 1208. | 326. | 0. | 1282. | 152. | 35. 600. |
| 1/ 4 | 0.100 | | | 141. | 842. | 517. | 325. | 0. | 770. | 229. | 53. 600. |
| | | | | 423. | 842. | 517. | 325. | 0. | 2315. | 229. | 53. 600. |
| | | | 1 MIN | 1206. | 1206. | 517. | 325. | 0. | 563. | 229. | 53. 600. |
| | | | 1 MAX | 1206. | 1206. | 517. | 325. | 0. | 3617. | 229. | 53. 300. |
| | | | 1 | 182. | 842. | 517. | 325. | 0. | 995. | 229. | 53. 600. |
| | | | 1 | 133. | 842. | 517. | 325. | 0. | 726. | 229. | 53. 600. |
| 1/ 5 | 0.200 | | | 108. | 713. | 388. | 325. | 0. | 589. | 305. | 70. 600. |
| | | | | 300. | 713. | 388. | 325. | 0. | 1643. | 305. | 70. 600. |
| | | | 1 MIN | 1206. | 1206. | 388. | 325. | 0. | 154. | 305. | N/C N/C |
| | | | 1 MAX | 1206. | 1206. | 388. | 325. | 0. | 2945. | 305. | 70. 300. |

**** OPTIMIZED SHEAR = 0.0 - RESISTANCE NOT DONE ****

SPAN/ X/L COMB. ULS MAX/MIN PRESTRESS NOMINAL <- STIRRUPS-> MIN MAX IKODE NOS.
 SEC TABLE GRP ULS APPLIED SHEAR RESISTANCE

| SPAN/ SEC | X/L | COMB. TABLE | ULS GRP | MAX/MIN APPLIED SHEAR V _f (kN) | FACTORED SHEAR RESISTANCE V _r (kN) | STIRRUP CAPACITY V _s (kN) | CONCRETE CAPACITY V _c (kN) | PRESTRESS COMPONENT FOR SHEAR V _p (kN) | NOMINAL SHEAR STRESS (v) (v) | AV ² (mm) | REQD AREA (mm) | MIN SPACING (mm) | MAX SPACING (mm) |
|-----------|-------|-------------|---------|---|---|--------------------------------------|---------------------------------------|---|------------------------------|----------------------|----------------|------------------|------------------|
| | | | | | | | | | | | | | |
| | | CHBDC | 1 | 137. | 713. | 388. | 325. | 0. | 747. | 258. | 305. | 70. | 600. |
| | | CHBDC | 1 | 100. | 713. | 388. | 325. | 0. | 544. | 258. | 305. | 70. | 600. |
| 1/ 5 | 0.300 | CHBDC | 1 | 75. | 713. | 388. | 325. | 0. | 408. | 258. | 305. | 70. | 600. |
| | | CHBDC | 1 | 188. | 713. | 388. | 325. | 0. | 1028. | 258. | 305. | 70. | 600. |
| | | CHBDC | 1 | MIN | -713. | 388. | 325. | 0. | 288. | 258. | 305. | N/C | N/C |
| | | CHBDC | 1 | MAX | 426. | 636. | 264. | 0. | 2330. | 258. | 305. | 70. | 600. |
| | | CHBDC | 1 | 91. | 713. | 388. | 325. | 0. | 498. | 258. | 305. | 70. | 600. |
| | | CHBDC | 1 | 66. | 713. | 388. | 325. | 0. | 363. | 258. | 305. | 70. | 600. |
| 1/ 6 | 0.400 | CHBDC | 1 | 41. | 584. | 259. | 325. | 0. | 226. | 258. | 457. | N/C | N/C |
| | | CHBDC | 1 | 86. | 584. | 259. | 325. | 0. | 473. | 258. | 457. | 105. | 600. |
| | | CHBDC | 1 | MIN | -133. | 259. | 325. | 0. | 730. | 258. | 457. | 105. | 600. |
| | | CHBDC | 1 | MAX | 324. | 457. | 220. | 0. | 1775. | 258. | 457. | 105. | 600. |
| | | CHBDC | 1 | 46. | 584. | 259. | 325. | 0. | 249. | 258. | 457. | N/C | N/C |
| | | CHBDC | 1 | 33. | 584. | 259. | 325. | 0. | 182. | 258. | 457. | N/C | N/C |
| 1/ 6 | 0.500 | CHBDC | 1 | 8. | 584. | 259. | 325. | 0. | 45. | 258. | 457. | N/C | N/C |
| | | CHBDC | 1 | -41. | -584. | 259. | 325. | 0. | 222. | 258. | 457. | N/C | N/C |
| | | CHBDC | 1 | MIN | -223. | 259. | 325. | 0. | 1218. | 258. | 457. | 105. | 600. |
| | | CHBDC | 1 | MAX | 223. | 495. | 250. | 0. | 1219. | 258. | 457. | 105. | 600. |
| | | CHBDC | 1 | 0. | 584. | 259. | 325. | 0. | 1. | 258. | 457. | N/C | N/C |
| 1/ 6 | 0.600 | CHBDC | 1 | -25. | -584. | 259. | 325. | 0. | 136. | 258. | 457. | N/C | N/C |
| | | CHBDC | 1 | -86. | -584. | 259. | 325. | 0. | 471. | 258. | 457. | 105. | 600. |
| | | CHBDC | 1 | MIN | -324. | 237. | 220. | 0. | 1773. | 258. | 457. | 105. | 600. |
| | | CHBDC | 1 | MAX | 134. | 259. | 325. | 0. | 731. | 258. | 457. | 105. | 600. |
| | | CHBDC | 1 | -45. | -584. | 259. | 325. | 0. | 248. | 258. | 457. | N/C | N/C |
| | | CHBDC | 1 | -33. | -584. | 259. | 325. | 0. | 181. | 258. | 457. | N/C | N/C |
| 1/ 7 | 0.700 | CHBDC | 1 | -70. | -713. | 388. | 325. | 0. | 382. | 258. | 305. | 70. | 600. |
| | | CHBDC | 1 | -188. | -713. | 388. | 325. | 0. | 1027. | 258. | 305. | 70. | 600. |
| | | CHBDC | 1 | MIN | -426. | 372. | 264. | 0. | 2329. | 258. | 305. | 70. | 600. |
| | | CHBDC | 1 | MAX | 53. | 388. | 325. | 0. | 289. | 258. | 305. | N/C | N/C |
| | | CHBDC | 1 | -91. | -713. | 388. | 325. | 0. | 497. | 258. | 305. | 70. | 600. |
| | | CHBDC | 1 | -66. | -713. | 388. | 325. | 0. | 362. | 258. | 305. | 70. | 600. |
| 1/ 7 | 0.800 | CHBDC | 1 | -103. | -713. | 388. | 325. | 0. | 563. | 258. | 305. | 70. | 600. |
| | | CHBDC | 1 | -300. | -713. | 388. | 325. | 0. | 1642. | 258. | 305. | 70. | 600. |
| | | CHBDC | 1 | MIN | -538. | 388. | 325. | 0. | 2943. | 258. | 305. | 70. | 300. |
| | | CHBDC | 1 | MAX | -28. | 388. | 325. | 0. | 153. | 258. | 305. | N/C | N/C |
| | | CHBDC | 1 | -136. | -713. | 388. | 325. | 0. | 745. | 258. | 305. | 70. | 600. |
| | | CHBDC | 1 | -99. | -713. | 388. | 325. | 0. | 543. | 258. | 305. | 70. | 600. |
| 1/ 8 | 0.900 | CHBDC | 1 | -136. | -842. | 517. | 325. | 0. | 745. | 258. | 229. | 53. | 600. |
| | | CHBDC | 1 | -423. | -842. | 517. | 325. | 0. | 2313. | 258. | 229. | 53. | 600. |

SPAN/ X/L COMB. ULS MAX/MIN FACTORED STIRRUP CONCRETE PRESTRESS NOMINAL <- STIRRUPS-> MIN MAX IKODE NOS.
 SEC TABLE GRP APPLIED SHEAR RESISTANCE V_f (kN) (kN) (kN) (kN) (kN) (kPa) (mm) (mm) (mm) (mm) (mm) (mm)

| SPAN/ SEC | X/L | COMB. TABLE | ULS GRP | MAX/MIN APPLIED SHEAR | FACTORED SHEAR RESISTANCE | V _f (kN) | V _s (kN) | V _c (kN) | V _p (kN) | FOR SHEAR STRESS AREA | COMPONENT SHEAR FOR SHEAR STRESS AREA | AV ² (mm) | REOD ² (mm) | MIN TOTAL SPACING AREA | MAX SPACING | IKODE NOS. |
|-----------|-------|-------------|---------|-----------------------|---------------------------|---------------------|---------------------|---------------------|---------------------|-----------------------|---------------------------------------|----------------------|------------------------|------------------------|-------------|------------|
| | | CHBDC | 1 | MIN | -661. | -842. | 517. | 325. | 0. | 3615. | 258. | 229. | 53. | 53. | 300. | |
| | | CHBDC | 1 | MAX | -103. | -842. | 517. | 325. | 0. | 562. | 258. | 229. | 53. | 53. | 600. | |
| | | CHBDC | 1 | | -182. | -842. | 517. | 325. | 0. | 994. | 258. | 229. | 53. | 53. | 600. | |
| | | CHBDC | 1 | | -132. | -842. | 517. | 325. | 0. | 724. | 258. | 229. | 53. | 53. | 600. | |
| 1/ 9 | 1.000 | CHBDC | 1 | | -231. | -1206. | 1032. | 326. | 0. | 1256. | 398. | 178. | 41. | 41. | 600. | |
| | | CHBDC | 1 | | -166. | -1206. | 1032. | 326. | 0. | 901. | 398. | 178. | 41. | 41. | 600. | |
| | | CHBDC | 1 | MIN | -157. | -1057. | 881. | 176. | 0. | 4266. | 398. | 178. | 41. | 41. | 300. | |
| | | CHBDC | 1 | MAX | -157. | -1206. | 1032. | 326. | 0. | 857. | 398. | 178. | 41. | 41. | 600. | |
| | | CHBDC | 1 | | -227. | -1206. | 1032. | 326. | 0. | 1236. | 398. | 178. | 41. | 41. | 600. | |
| | | CHBDC | 1 | | -231. | -1206. | 1032. | 326. | 0. | 1256. | 398. | 178. | 41. | 41. | 600. | |
| RC/ 9 | 0.000 | CHBDC | 1 | | 303. | 1206. | 997. | 277. | 0. | 1648. | 398. | 178. | 41. | 41. | 600. | |
| | | CHBDC | 1 | | 4. | 1200. | 1027. | 325. | 0. | 22. | 398. | 178. | N/C | N/C | N/C | |
| | | CHBDC | 1 | MIN | 4. | 1200. | 1027. | 325. | 0. | 22. | 398. | 178. | N/C | N/C | N/C | |
| | | CHBDC | 1 | MAX | 303. | 1200. | 1027. | 325. | 0. | 1658. | 398. | 178. | 41. | 41. | 600. | |
| | | CHBDC | 1 | | 6. | 1200. | 1027. | 325. | 0. | 31. | 398. | 178. | N/C | N/C | N/C | |
| | | CHBDC | 1 | | 303. | 1206. | 997. | 277. | 0. | 1648. | 398. | 178. | 41. | 41. | 600. | |
| RC/ 9 | 1.000 | CHBDC | 1 | MAX | 298. | 1206. | 1032. | 326. | 0. | 1619. | 398. | 178. | 41. | 41. | 600. | |



Run # 2, Filename: 7108.2b1
 End Span, Exterior Girder, 3 lanes loaded

STAGE NUMBER = 2

THE IKODE NUMBER IS GIVEN WHEN A CODE CLAUSE IS VIOLATED.

| IKODE NO. | CODE CLAUSE |
|-----------|-------------------------------|
| 30 | 8.8.4.3 MIN. LONGITUDINAL R/F |
| 31 | 8.8.4.5 MAX. LONGITUDINAL R/F |
| 32 | $ Mr/Mf < 1.0$ |

LC = LEFT CANTILEVER SECTION
 RC = RIGHT CANTILEVER SECTION
 $|Mr/Mf|$ = ABSOLUTE VALUE OF M_r/M_f
 c/d = FACTOR DEFINED IN 8.8.4.5 ; A NEGATIVE VALUE OF c/d INDICATES Asc > As

| SPAN/ SEC | X/L | COMB. TABLE | ULS GROUP NO. | MAX/MIN APPLIED MOMENT MF (kN-m) | (FACTORED) RESISTANCE MOMENT MR (kN-m) | CRACKING MOMENT Mcr (kN-m) | N.A FROM EXT.COMP FIBRE C (m) | $ Mr/Mf $ | 1.2Mcr/Mr | 1.33ME/Mr | c/d | IKODE NOS. |
|--------------|-------|----------------|---------------------|--|--|-------------------------------------|---|-----------|-----------|-----------|------|------------|
| LC/ 2 | 0.000 | CHBDC | 1 MIN | -33. | -1629. | -749. | 0.214 | 49.8 | 0.552 | 0.027 | 0.22 | |
| | | | 1 MAX | -30. | -1629. | -749. | 0.214 | 55.0 | 0.552 | 0.024 | 0.22 | |
| | | | 1 | -30. | -1629. | -749. | 0.214 | 55.0 | 0.552 | 0.024 | 0.22 | |
| | | | 1 | -30. | -1629. | -749. | 0.214 | 55.0 | 0.552 | 0.024 | 0.22 | |
| | | | 1 | -30. | -1629. | -749. | 0.214 | 55.0 | 0.552 | 0.024 | 0.22 | |
| | | | 1 | -33. | -1629. | -749. | 0.214 | 49.8 | 0.552 | 0.027 | 0.22 | |
| LC/ 3 | 1.000 | CHBDC | 1 MIN | -134. | -1706. | -749. | 0.208 | 12.7 | 0.527 | 0.105 | 0.23 | |
| | | | 1 MAX | -30. | -1706. | -749. | 0.208 | 57.2 | 0.527 | 0.023 | 0.23 | |
| | | | 1 | -129. | -1706. | -749. | 0.208 | 13.3 | 0.527 | 0.100 | 0.23 | |
| | | | 1 | -33. | -1706. | -749. | 0.208 | 52.0 | 0.527 | 0.026 | 0.23 | |
| | | | 1 | -30. | -1706. | -749. | 0.208 | 56.2 | 0.527 | 0.024 | 0.23 | |
| | | | 1 | -134. | -1706. | -749. | 0.208 | 12.7 | 0.527 | 0.105 | 0.23 | |
| 1/ 3 | 0.000 | CHBDC | 1 MIN | -146. | -1723. | -749. | 0.212 | 11.8 | 0.522 | 0.113 | 0.25 | |
| | | | 1 MAX | -40. | -1723. | -749. | 0.212 | 42.6 | 0.522 | 0.031 | 0.25 | |
| | | | 1 | -40. | -1723. | -749. | 0.212 | 42.6 | 0.522 | 0.031 | 0.25 | |
| | | | 1 | -45. | -1723. | -749. | 0.212 | 38.2 | 0.522 | 0.035 | 0.25 | |
| | | | 1 | -41. | -1723. | -749. | 0.212 | 42.0 | 0.522 | 0.032 | 0.25 | |
| | | | 1 | -146. | -1723. | -749. | 0.212 | 11.8 | 0.522 | 0.113 | 0.25 | |
| 1/ 4 | 0.100 | CHBDC | 1 MIN | 83. | 3358. | 1603. | 0.092 | 40.4 | 0.573 | 0.033 | 0.10 | |
| | | | 1 MAX | 815. | 3358. | 1603. | 0.092 | 4.1 | 0.573 | 0.323 | 0.10 | |
| | | | 1 | 496. | 3358. | 1603. | 0.092 | 6.8 | 0.573 | 0.196 | 0.10 | |
| | | | 1 | 815. | 3358. | 1603. | 0.092 | 4.1 | 0.573 | 0.323 | 0.10 | |
| | | | 1 | 239. | 3358. | 1603. | 0.092 | 14.1 | 0.573 | 0.095 | 0.10 | |
| | | | 1 | 83. | 3358. | 1603. | 0.092 | 40.4 | 0.573 | 0.033 | 0.10 | |

| SPAN/ SEC | X/L | COMB. TABLE | ULS GROUP NO. | MAX/MIN APPLIED MOMENT Mf (kN-m) | (FACTORED) RESISTANCE MOMENT Mr (kN-m) | CRACKING MOMENT Mcr (kN-m) | N.A FROM EXT.COMP FIBRE C (m) | Mr/Mf | 1.2Mcr/Mr | 1.33ME/Mr | c/d | IKODE NOS. |
|--------------|-------|----------------|---------------------|--|--|-------------------------------------|---|-------|-----------|-----------|------|------------|
| | | | | 174. | 3358. | 1603. | 0.092 | 19.3 | 0.573 | 0.069 | 0.10 | |
| | | | | 230. | 3358. | 1541. | 0.092 | 14.6 | 0.550 | 0.091 | 0.10 | |
| 1/ 5 | 0.200 | | 1 MIN | 1392. | 3358. | 1541. | 0.092 | 2.4 | 0.550 | 0.551 | 0.10 | |
| | | | 1 MAX | 997. | 3358. | 1541. | 0.092 | 3.4 | 0.550 | 0.395 | 0.10 | |
| | | | | 1392. | 3358. | 1541. | 0.092 | 2.4 | 0.550 | 0.551 | 0.10 | |
| | | | | 426. | 3358. | 1541. | 0.092 | 7.9 | 0.550 | 0.169 | 0.10 | |
| | | | | 311. | 3358. | 1541. | 0.092 | 10.8 | 0.550 | 0.123 | 0.10 | |
| | | | | 337. | 3358. | 1496. | 0.092 | 10.0 | 0.535 | 0.134 | 0.10 | |
| 1/ 5 | 0.300 | | 1 MIN | 1768. | 3358. | 1496. | 0.092 | 1.9 | 0.535 | 0.700 | 0.10 | |
| | | | 1 MAX | 1410. | 3358. | 1496. | 0.092 | 2.4 | 0.535 | 0.558 | 0.10 | |
| | | | | 1768. | 3358. | 1496. | 0.092 | 1.9 | 0.535 | 0.700 | 0.10 | |
| | | | | 560. | 3358. | 1496. | 0.092 | 6.0 | 0.535 | 0.222 | 0.10 | |
| | | | | 408. | 3358. | 1496. | 0.092 | 8.2 | 0.535 | 0.162 | 0.10 | |
| | | | | 406. | 3358. | 1469. | 0.092 | 8.3 | 0.525 | 0.161 | 0.10 | |
| 1/ 6 | 0.400 | | 1 MIN | 1981. | 3358. | 1469. | 0.092 | 1.7 | 0.525 | 0.785 | 0.10 | |
| | | | 1 MAX | 1669. | 3358. | 1469. | 0.092 | 2.0 | 0.525 | 0.661 | 0.10 | |
| | | | | 1981. | 3358. | 1469. | 0.092 | 1.7 | 0.525 | 0.785 | 0.10 | |
| | | | | 641. | 3358. | 1469. | 0.092 | 5.2 | 0.525 | 0.254 | 0.10 | |
| | | | | 467. | 3358. | 1469. | 0.092 | 7.2 | 0.525 | 0.185 | 0.10 | |
| | | | | 436. | 3358. | 1460. | 0.092 | 7.7 | 0.522 | 0.173 | 0.10 | |
| 1/ 6 | 0.500 | | 1 MIN | 2057. | 3358. | 1460. | 0.092 | 1.6 | 0.522 | 0.815 | 0.10 | |
| | | | 1 MAX | 1825. | 3358. | 1460. | 0.092 | 1.8 | 0.522 | 0.723 | 0.10 | |
| | | | | 2006. | 3358. | 1460. | 0.092 | 1.7 | 0.522 | 0.795 | 0.10 | |
| | | | | 668. | 3358. | 1460. | 0.092 | 5.0 | 0.522 | 0.264 | 0.10 | |
| | | | | 486. | 3358. | 1460. | 0.092 | 6.9 | 0.522 | 0.193 | 0.10 | |
| | | | | 427. | 3358. | 1469. | 0.092 | 7.9 | 0.525 | 0.169 | 0.10 | |
| 1/ 6 | 0.600 | | 1 MIN | 1982. | 3358. | 1469. | 0.092 | 1.7 | 0.525 | 0.785 | 0.10 | |
| | | | 1 MAX | 1982. | 3358. | 1469. | 0.092 | 1.7 | 0.525 | 0.785 | 0.10 | |
| | | | | 1669. | 3358. | 1469. | 0.092 | 2.0 | 0.525 | 0.661 | 0.10 | |
| | | | | 641. | 3358. | 1469. | 0.092 | 5.2 | 0.525 | 0.254 | 0.10 | |
| | | | | 467. | 3358. | 1469. | 0.092 | 7.2 | 0.525 | 0.185 | 0.10 | |
| | | | | 377. | 3358. | 1496. | 0.092 | 8.9 | 0.535 | 0.149 | 0.10 | |
| 1/ 7 | 0.700 | | 1 MIN | 1769. | 3358. | 1496. | 0.092 | 1.9 | 0.535 | 0.700 | 0.10 | |
| | | | 1 MAX | 1769. | 3358. | 1496. | 0.092 | 1.9 | 0.535 | 0.700 | 0.10 | |
| | | | | 1410. | 3358. | 1496. | 0.092 | 2.4 | 0.535 | 0.558 | 0.10 | |
| | | | | 561. | 3358. | 1496. | 0.092 | 6.0 | 0.535 | 0.222 | 0.10 | |
| | | | | 409. | 3358. | 1496. | 0.092 | 8.2 | 0.535 | 0.162 | 0.10 | |
| | | | | 275. | 3358. | 1540. | 0.092 | 12.2 | 0.550 | 0.109 | 0.10 | |
| 1/ 7 | 0.800 | | 1 MIN | 1393. | 3358. | 1540. | 0.092 | 2.4 | 0.550 | 0.552 | 0.10 | |
| | | | 1 MAX | 1393. | 3358. | 1540. | 0.092 | 2.4 | 0.550 | 0.552 | 0.10 | |
| | | | | 998. | 3358. | 1540. | 0.092 | 3.4 | 0.550 | 0.395 | 0.10 | |

| SPAN/ SEC | X/L | COMB. TABLE | ULS GROUP NO. | MAX/MIN APPLIED MOMENT Mf (kN-m) | (FACTORED) RESISTANCE MOMENT Mr (kN-m) | CRACKING MOMENT Mcr (kN-m) | N.A FROM EXT.COMP FIBRE C (m) | 1.2Mcr/Mr | 1.33Mf/Mr | c/d | IKODE NOS. |
|--------------|-------|----------------|---------------------|--|--|-------------------------------------|---|-----------|-----------|-------|------------|
| 1/ 8 | 0.900 | CHBDC | 1 | 427. | 3358. | 1540. | 0.092 | 7.9 | 0.550 | 0.169 | 0.10 |
| | | | 1 | 311. | 3358. | 1540. | 0.092 | 10.8 | 0.550 | 0.123 | 0.10 |
| 1/ 8 | 0.900 | CHBDC | 1 | 134. | 3358. | 1602. | 0.092 | 25.1 | 0.573 | 0.053 | 0.10 |
| | | | 1 | 816. | 3358. | 1602. | 0.092 | 4.1 | 0.573 | 0.323 | 0.10 |
| | | | 1 | 816. | 3358. | 1602. | 0.092 | 4.1 | 0.573 | 0.323 | 0.10 |
| | | | 1 | 497. | 3358. | 1602. | 0.092 | 6.8 | 0.573 | 0.197 | 0.10 |
| | | | 1 | 240. | 3358. | 1602. | 0.092 | 14.0 | 0.573 | 0.095 | 0.10 |
| | | | 1 | 175. | 3358. | 1602. | 0.092 | 19.2 | 0.573 | 0.069 | 0.10 |
| 1/ 9 | 1.000 | CHBDC | 1 | -89. | -1690. | -749. | 0.205 | 19.0 | 0.532 | 0.070 | 0.22 |
| | | | 1 | -39. | -1690. | -749. | 0.205 | 43.0 | 0.532 | 0.031 | 0.22 |
| | | | 1 | -43. | -1690. | -749. | 0.205 | 38.9 | 0.532 | 0.034 | 0.22 |
| | | | 1 | -39. | -1690. | -749. | 0.205 | 43.0 | 0.532 | 0.031 | 0.22 |
| | | | 1 | -39. | -1690. | -749. | 0.205 | 42.9 | 0.532 | 0.031 | 0.22 |
| | | | 1 | -89. | -1690. | -749. | 0.205 | 19.0 | 0.532 | 0.070 | 0.22 |
| RC/ 9 | 0.000 | CHBDC | 1 | -8. | -1690. | -749. | 0.205 | *** | 0.532 | 0.006 | 0.22 |
| | | | 1 | 42. | 3350. | 741. | 0.091 | 79.3 | 0.265 | 0.017 | 0.10 |
| | | | 1 | 42. | 3350. | 741. | 0.091 | 79.3 | 0.265 | 0.017 | 0.10 |
| | | | 1 | 38. | 3350. | 741. | 0.091 | 87.9 | 0.265 | 0.015 | 0.10 |
| | | | 1 | 42. | 3350. | 741. | 0.091 | 79.5 | 0.265 | 0.017 | 0.10 |
| | | | 1 | -8. | -1690. | -749. | 0.205 | *** | 0.532 | 0.006 | 0.22 |
| RC/ 9 | 1.000 | CHBDC | 1 | -43. | -1629. | -749. | 0.214 | 38.3 | 0.552 | 0.035 | 0.22 |
| | | | 1 | -39. | -1629. | -749. | 0.214 | 42.3 | 0.552 | 0.031 | 0.22 |
| | | | 1 | -39. | -1629. | -749. | 0.214 | 42.3 | 0.552 | 0.031 | 0.22 |
| | | | 1 | -43. | -1629. | -749. | 0.214 | 38.3 | 0.552 | 0.035 | 0.22 |
| | | | 1 | -39. | -1629. | -749. | 0.214 | 42.3 | 0.552 | 0.031 | 0.22 |
| | | | 1 | -43. | -1629. | -749. | 0.214 | 38.3 | 0.552 | 0.035 | 0.22 |



| SPAN/ SEC | X/L | COMB. TABLE | ULS GRP | MAX/MIN APPLIED SHEAR Vf | FACTORED SHEAR RESISTANCE Vr | STIRRUP CAPACITY Vs | CONCRETE CAPACITY Vc | PRESTRESS COMPONENT FOR SHEAR Vp | NOMINAL SHEAR STRESS (v) | AV | MIN TOTAL SPACING AREA REQD (mm) | MAX TOTAL SPACING AREA REQD (mm) | IKODE NOS. |
|--------------|-------|----------------|------------|-----------------------------------|---------------------------------------|---------------------------|----------------------------|--|-----------------------------------|------|---|---|------------|
| | | CHBDC | 1 | 134. | 713. | 388. | 325. | 0. | 731. | 258. | 305. | 70. | 600. |
| | | CHBDC | 1 | 97. | 713. | 388. | 325. | 0. | 533. | 258. | 305. | 70. | 600. |
| 1/ 5 | 0.300 | CHBDC | 1 | 73. | 713. | 388. | 325. | 0. | 400. | 258. | 305. | 70. | 600. |
| | | CHBDC | 1 | 186. | 713. | 388. | 325. | 0. | 1018. | 258. | 305. | 70. | 600. |
| | | CHBDC | 1 | -54. | -713. | 388. | 325. | 0. | 296. | 258. | 305. | N/C | N/C |
| | | CHBDC | 1 | 424. | 645. | 374. | 325. | 0. | 2320. | 258. | 305. | 70. | 600. |
| | | CHBDC | 1 | 89. | 713. | 388. | 325. | 0. | 488. | 258. | 305. | 70. | 600. |
| | | CHBDC | 1 | 65. | 713. | 388. | 325. | 0. | 395. | 258. | 305. | 70. | 600. |
| 1/ 6 | 0.400 | CHBDC | 1 | 41. | 584. | 259. | 325. | 0. | 223. | 258. | 457. | N/C | N/C |
| | | CHBDC | 1 | 86. | 584. | 259. | 325. | 0. | 468. | 258. | 457. | 105. | 600. |
| | | CHBDC | 1 | -134. | -584. | 259. | 325. | 0. | 734. | 258. | 457. | 105. | 600. |
| | | CHBDC | 1 | 324. | 464. | 239. | 225. | 0. | 1769. | 258. | 457. | 105. | 600. |
| | | CHBDC | 1 | 45. | 584. | 259. | 325. | 0. | 244. | 258. | 457. | N/C | N/C |
| | | CHBDC | 1 | 33. | 584. | 259. | 325. | 0. | 178. | 258. | 457. | N/C | N/C |
| 1/ 6 | 0.500 | CHBDC | 1 | 8. | 584. | 259. | 325. | 0. | 45. | 258. | 457. | N/C | N/C |
| | | CHBDC | 1 | 41. | 584. | 259. | 325. | 0. | 224. | 258. | 457. | N/C | N/C |
| | | CHBDC | 1 | -223. | -584. | 259. | 325. | 0. | 1218. | 258. | 457. | 105. | 600. |
| | | CHBDC | 1 | 223. | 502. | 246. | 256. | 0. | 1219. | 258. | 457. | 105. | 600. |
| | | CHBDC | 1 | 0. | 584. | 259. | 325. | 0. | 1. | 258. | 457. | N/C | N/C |
| 1/ 6 | 0.600 | CHBDC | 1 | -24. | -584. | 259. | 325. | 0. | 132. | 258. | 457. | N/C | N/C |
| | | CHBDC | 1 | -85. | -584. | 259. | 325. | 0. | 466. | 258. | 457. | 105. | 600. |
| | | CHBDC | 1 | -323. | -464. | 239. | 225. | 0. | 1768. | 258. | 457. | 105. | 600. |
| | | CHBDC | 1 | 134. | 584. | 259. | 325. | 0. | 735. | 258. | 457. | 105. | 600. |
| | | CHBDC | 1 | -44. | -584. | 259. | 325. | 0. | 243. | 258. | 457. | N/C | N/C |
| | | CHBDC | 1 | -32. | -584. | 259. | 325. | 0. | 177. | 258. | 457. | N/C | N/C |
| 1/ 7 | 0.700 | CHBDC | 1 | -68. | -713. | 388. | 325. | 0. | 374. | 258. | 305. | 70. | 600. |
| | | CHBDC | 1 | -186. | -713. | 388. | 325. | 0. | 1017. | 258. | 305. | 70. | 600. |
| | | CHBDC | 1 | -424. | -645. | 374. | 271. | 0. | 2318. | 258. | 305. | 70. | 600. |
| | | CHBDC | 1 | 54. | 713. | 388. | 325. | 0. | 297. | 258. | 305. | N/C | N/C |
| | | CHBDC | 1 | -89. | -713. | 388. | 325. | 0. | 486. | 258. | 305. | 70. | 600. |
| | | CHBDC | 1 | -65. | -713. | 388. | 325. | 0. | 354. | 258. | 305. | N/C | N/C |
| 1/ 7 | 0.800 | CHBDC | 1 | -101. | -713. | 388. | 325. | 0. | 552. | 258. | 305. | 70. | 600. |
| | | CHBDC | 1 | -297. | -713. | 388. | 325. | 0. | 1626. | 258. | 305. | 70. | 600. |
| | | CHBDC | 1 | -535. | -713. | 388. | 325. | 0. | 2928. | 258. | 305. | 70. | 300. |
| | | CHBDC | 1 | -26. | -713. | 388. | 325. | 0. | 141. | 258. | 305. | N/C | N/C |
| | | CHBDC | 1 | -133. | -713. | 388. | 325. | 0. | 730. | 258. | 305. | 70. | 600. |
| | | CHBDC | 1 | -97. | -713. | 388. | 325. | 0. | 532. | 258. | 305. | 70. | 600. |
| 1/ 8 | 0.900 | CHBDC | 1 | -133. | -842. | 517. | 325. | 0. | 729. | 258. | 229. | 53. | 600. |
| | | CHBDC | 1 | -419. | -842. | 517. | 325. | 0. | 2293. | 258. | 229. | 53. | 600. |

| SPAN/ SEC | X/L | COMB. TABLE | ULS GRP | MAX/MIN APPLIED SHEAR VF | FACTORED SHEAR RESISTANCE VF | STIRRUP CAPACITY VS | CONCRETE CAPACITY VC | PRESTRESS COMPONENT FOR SHEAR VP | NOMINAL SHEAR STRESS AV | STIRRUPS-> | | MAX IKODE NOS. |
|--------------|-------|----------------|------------|-----------------------------------|---------------------------------------|---------------------------|----------------------------|---|----------------------------------|------------------------------|------------------------------|-------------------|
| | | | | | | | | | | MIN TOTAL SPACING REQD | MAX TOTAL SPACING AREA | |
| | | | | (kN) | (kN) | (kN) | (kN) | (kN) | (kPa) | (mm) | (mm) | (mm) |
| | | | | | | | | | | | | |
| 1/ 9 | 0.000 | CHBDC | 1 | -657. | -842. | 517. | 325. | 0. | 3595. | 258. | 229. | 53. |
| | | CHBDC | 1 | -100. | -842. | 517. | 325. | 0. | 546. | 258. | 229. | 53. |
| | | CHBDC | 1 | -178. | -842. | 517. | 325. | 0. | 973. | 258. | 229. | 53. |
| | | CHBDC | 1 | -130. | -842. | 517. | 325. | 0. | 709. | 258. | 229. | 53. |
| | | CHBDC | 1 | -226. | -1206. | 1032. | 326. | 0. | 1231. | 398. | 178. | 41. |
| | | CHBDC | 1 | -162. | -1206. | 1032. | 326. | 0. | 882. | 398. | 178. | 41. |
| | | CHBDC | 1 | | | 883. | 177. | 0. | 4240. | 398. | 178. | 41. |
| | | CHBDC | 1 | | | 1032. | 326. | 0. | 838. | 398. | 178. | 41. |
| | | CHBDC | 1 | -222. | -1206. | 1032. | 326. | 0. | 1211. | 398. | 178. | 41. |
| | | CHBDC | 1 | -226. | -1206. | 1032. | 326. | 0. | 1231. | 398. | 178. | 41. |
| RC/ 9 | 0.000 | CHBDC | 1 | 303. | 1206. | 997. | 277. | 0. | 1647. | 398. | 178. | 41. |
| | | CHBDC | 1 | 4. | 1200. | 1027. | 325. | 0. | 22. | 398. | 178. | N/C |
| | | CHBDC | 1 | 4. | 1200. | 1027. | 325. | 0. | 22. | 398. | 178. | N/C |
| | | CHBDC | 1 | 303. | 1200. | 1027. | 325. | 0. | 1657. | 398. | 178. | 41. |
| | | CHBDC | 1 | 6. | 1200. | 1027. | 325. | 0. | 30. | 398. | 178. | N/C |
| | | CHBDC | 1 | 303. | 1206. | 997. | 277. | 0. | 1647. | 398. | 178. | 41. |
| RC/ 9 | 1.000 | CHBDC | 1 | 297. | 1206. | 1032. | 326. | 0. | 1619. | 398. | 178. | 41. |



COMPOSITE PRESTRESSED GIRDER - ULTIMATE LIMIT STATES - FLEXURE

STAGE NUMBER = 2

THE IKODE NUMBER IS GIVEN WHEN A CODE CLAUSE IS VIOLATED.

IKODE NO. CODE CLAUSE

- 30 8.8.4.3 MIN. LONGITUDINAL R/F
- 31 8.8.4.5 MAX. LONGITUDINAL R/F
- 32 $|M_r/M_f| < 1.0$

LC = LEFT CANTILEVER SECTION
RC = RIGHT CANTILEVER SECTION

$|M_r/M_f|$ = ABSOLUTE VALUE OF M_r/M_f

c/d = FACTOR DEFINED IN 8.8.4.5 ; A NEGATIVE VALUE OF c/d INDICATES Asc > As

SPAN/ X/L COMB. ULS (FACTORED) CRACKING N.A FROM 1.2Mcr/Mr 1.33Mf/Mr c/d IKODE NOS.

SEC TABLE GROUP NO. APPLIED RESISTANCE MOMENT EXT. COMP FIBRE

(kN-m) (kN-m) (kN-m) (kN-m) (m)

| LC/ 2 | 0.000 | CHBDC | 1 | MIN | -55. | -1748. | -785. | 0.250 | 31.7 | 0.539 | 0.042 | 0.25 |
|-------|-------|-------|---|-----|-------|--------|-------|-------|------|-------|-------|-------|
| | | CHBDC | 1 | MAX | -50. | -1748. | -785. | 0.250 | 35.0 | 0.539 | 0.038 | 0.25 |
| | | CHBDC | 1 | | -55. | -1748. | -785. | 0.250 | 31.7 | 0.539 | 0.042 | 0.25 |
| | | CHBDC | 1 | | -50. | -1748. | -785. | 0.250 | 35.0 | 0.539 | 0.038 | 0.25 |
| | | CHBDC | 1 | | -50. | -1748. | -785. | 0.250 | 35.0 | 0.539 | 0.038 | 0.25 |
| | | CHBDC | 1 | | -55. | -1748. | -785. | 0.250 | 31.7 | 0.539 | 0.042 | 0.25 |
| LC/ 2 | 1.000 | CHBDC | 1 | MIN | -100. | -1728. | -785. | 0.248 | 17.2 | 0.545 | 0.077 | 0.25 |
| | | CHBDC | 1 | MAX | -51. | -1728. | -785. | 0.248 | 34.1 | 0.545 | 0.039 | 0.25 |
| | | CHBDC | 1 | | -100. | -1728. | -785. | 0.248 | 17.2 | 0.545 | 0.077 | 0.25 |
| | | CHBDC | 1 | | -51. | -1728. | -785. | 0.248 | 34.1 | 0.545 | 0.039 | 0.25 |
| | | CHBDC | 1 | | -51. | -1728. | -785. | 0.248 | 34.0 | 0.545 | 0.039 | 0.25 |
| | | CHBDC | 1 | | -100. | -1728. | -785. | 0.248 | 17.2 | 0.545 | 0.077 | 0.25 |
| 1/ 2 | 0.000 | CHBDC | 1 | MIN | -127. | -1843. | -785. | 0.226 | 14.5 | 0.511 | 0.092 | 0.24 |
| | | CHBDC | 1 | MAX | -75. | -1843. | -785. | 0.226 | 24.6 | 0.511 | 0.054 | 0.24 |
| | | CHBDC | 1 | | -83. | -1843. | -785. | 0.226 | 22.3 | 0.511 | 0.060 | 0.24 |
| | | CHBDC | 1 | | -75. | -1843. | -785. | 0.226 | 24.6 | 0.511 | 0.054 | 0.24 |
| | | CHBDC | 1 | | -75. | -1843. | -785. | 0.226 | 24.6 | 0.511 | 0.054 | 0.24 |
| | | CHBDC | 1 | | -127. | -1843. | -785. | 0.226 | 14.5 | 0.511 | 0.092 | 0.24 |
| 1/ 3 | 0.100 | CHBDC | 1 | MIN | 339. | 4576. | 2227. | 0.107 | 13.5 | 0.584 | 0.099 | 0.11 |
| | | CHBDC | 1 | MAX | 1504. | 4576. | 2227. | 0.107 | 3.0 | 0.584 | 0.11 | 0.437 |
| | | CHBDC | 1 | | 871. | 4576. | 2227. | 0.107 | 5.3 | 0.584 | 0.253 | 0.11 |
| | | CHBDC | 1 | | 1504. | 4576. | 2227. | 0.107 | 3.0 | 0.584 | 0.437 | 0.11 |
| | | CHBDC | 1 | | 520. | 4576. | 2227. | 0.107 | 8.8 | 0.584 | 0.151 | 0.11 |

| SPAN/ SEC | X/L | COMB. TABLE GROUP NO. | ULS GROUP NO. | MAX/MIN APPLIED MOMENT (kN-m) | (FACTORED) RESISTANCE MOMENT (kN-m) | Mcr (kN-m) | N.A FROM EXT.COMP FIBRE C (m) | Mr/Mf | 1.2Mcr/Mr | 1.33Mf/Mr | c/d | IKODE NOS. |
|--------------|-------|--------------------------------|---------------------|--|--|---------------|---|-------|-----------|-----------|------|------------|
| | | CHBDC | 1 | 379. | 4576. | 2227. | 0.107 | 12.1 | 0.584 | 0.110 | 0.11 | |
| 1/ 4 | 0.200 | CHBDC | 1 MIN | 639. | 4849. | 2318. | 0.107 | 7.6 | 0.574 | 0.175 | 0.10 | |
| | | CHBDC | 1 MAX | 1777. | 4849. | 2318. | 0.107 | 1.9 | 0.574 | 0.704 | 0.10 | |
| | | CHBDC | 1 | 2560. | 4849. | 2318. | 0.107 | 2.7 | 0.574 | 0.487 | 0.10 | |
| | | CHBDC | 1 | 925. | 4849. | 2318. | 0.107 | 1.9 | 0.574 | 0.702 | 0.10 | |
| | | CHBDC | 1 | 674. | 4849. | 2318. | 0.107 | 5.2 | 0.574 | 0.254 | 0.10 | |
| | | CHBDC | 1 | 854. | 5121. | 2449. | 0.107 | 7.2 | 0.574 | 0.185 | 0.10 | |
| 1/ 4 | 0.300 | CHBDC | 1 MIN | 3369. | 5121. | 2449. | 0.107 | 6.0 | 0.574 | 0.222 | 0.10 | |
| | | CHBDC | 1 MAX | 2459. | 5121. | 2449. | 0.107 | 1.5 | 0.574 | 0.875 | 0.10 | |
| | | CHBDC | 1 | 3271. | 5121. | 2449. | 0.107 | 2.1 | 0.574 | 0.639 | 0.10 | |
| | | CHBDC | 1 | 1214. | 5121. | 2449. | 0.107 | 1.6 | 0.574 | 0.850 | 0.10 | |
| | | CHBDC | 1 | 885. | 5121. | 2449. | 0.107 | 4.2 | 0.574 | 0.315 | 0.10 | |
| | | CHBDC | 1 | 984. | 5308. | 2552. | 0.107 | 5.8 | 0.574 | 0.230 | 0.10 | |
| 1/ 5 | 0.400 | CHBDC | 1 MIN | 3787. | 5308. | 2552. | 0.107 | 5.4 | 0.577 | 0.247 | 0.09 | |
| | | CHBDC | 1 MAX | 2948. | 5308. | 2552. | 0.107 | 1.4 | 0.577 | 0.949 | 0.09 | |
| | | CHBDC | 1 | 3590. | 5308. | 2552. | 0.107 | 1.8 | 0.577 | 0.739 | 0.09 | |
| | | CHBDC | 1 | 1387. | 5308. | 2552. | 0.107 | 1.5 | 0.577 | 0.899 | 0.09 | |
| | | CHBDC | 1 | 1011. | 5308. | 2552. | 0.107 | 3.8 | 0.577 | 0.347 | 0.09 | |
| | | CHBDC | 1 | 1031. | 5308. | 2532. | 0.107 | 5.3 | 0.577 | 0.253 | 0.09 | |
| 1/ 5 | 0.500 | CHBDC | 1 MIN | 3868. | 5308. | 2532. | 0.107 | 5.4 | 0.572 | 0.258 | 0.09 | |
| | | CHBDC | 1 MAX | 3158. | 5308. | 2532. | 0.107 | 1.4 | 0.572 | 0.969 | 0.09 | |
| | | CHBDC | 1 | 3550. | 5308. | 2532. | 0.107 | 1.7 | 0.572 | 0.791 | 0.09 | |
| | | CHBDC | 1 | 1445. | 5308. | 2532. | 0.107 | 1.5 | 0.572 | 0.889 | 0.09 | |
| | | CHBDC | 1 | 1053. | 5308. | 2532. | 0.107 | 3.7 | 0.572 | 0.362 | 0.09 | |
| | | CHBDC | 1 | | 5308. | 2532. | 0.107 | 5.0 | 0.572 | 0.264 | 0.09 | |

COMPOSITE PRESTRESSED GIRDER - ULTIMATE LIMIT STATES - SHEAR

STAGE NUMBER = 2

THE IKODE NUMBER IS GIVEN WHEN A CODE CLAUSE IS VIOLATED.
 VIOLATION OF CL 8.9.3.11/12 MAY NOT BE CRITICAL IF USER ENSURES THAT CL 8.9.3.10 IS SATISFIED BY PROPER REBAR DETAILING.
 IKODE NO. N/C ---> NOT CALCULATED, STIRRUPS NOT REQUIRED AS PER CHBDC CLAUSE 8.9.1.2 FOR Vf

33 8.9.3.2
 35 8.9.3.11/12
 36 8.9.1.3
 37 8.9.1.3

LC = LEFT CANTILEVER SECTION
 RC = RIGHT CANTILEVER SECTION

NOTE: THE APPLICABILITY OF IKODES 36 & 37 FOR SOLID SLAB SECTIONS MUST BE ASCERTAINED BY THE USER.

| SPAN/ SEC | X/L | COMP. TABLE | ULS GRP | MAX/MIN SHEAR Vf | FACTORED SHEAR RESISTANCE Vr | STIRRUP CAPACITY Vs | CONCRETE CAPACITY Vc | PRESTRESS NOMINAL COMPONENT FOR SHEAR Vp | STIRRUPS-> TOTAL SPACING AREA AV | MIN REQD | MAX IKODE NOS. |
|--------------|-------|----------------|------------|------------------------|---------------------------------------|---------------------------|----------------------------|---|---|-------------|-------------------|
| | | | | (kN) | (kN) | (kN) | (kN) | (kPa) | (mm) | (mm) | (mm) |
| LC/ 2 | 0.000 | CHBDC | 1 | -11. | -1192. | 1430. | 322. | 0. | 398. | 127. | N/C |
| | | CHBDC | 1 | -10. | -1192. | 1430. | 322. | 0. | 398. | 127. | N/C |
| | | CHBDC | 1 | -11. | -1192. | 1430. | 322. | 0. | 398. | 127. | N/C |
| | | CHBDC | 1 | -10. | -1192. | 1430. | 322. | 0. | 398. | 127. | N/C |
| | | CHBDC | 1 | -10. | -1192. | 1430. | 322. | 0. | 398. | 127. | N/C |
| | | CHBDC | 1 | -11. | -1192. | 1430. | 322. | 0. | 398. | 127. | N/C |
| LC/ 2 | 1.000 | CHBDC | 1 | -314. | -1190. | 1427. | 322. | 0. | 398. | 127. | 29. |
| | | CHBDC | 1 | -14. | -1190. | 1427. | 322. | 0. | 398. | 127. | N/C |
| | | CHBDC | 1 | -314. | -1190. | 1427. | 322. | 0. | 398. | 127. | 29. |
| | | CHBDC | 1 | -14. | -1190. | 1427. | 322. | 0. | 398. | 127. | N/C |
| | | CHBDC | 1 | -15. | -1190. | 1427. | 322. | 0. | 398. | 127. | N/C |
| | | CHBDC | 1 | -314. | -1190. | 1427. | 322. | 0. | 398. | 127. | 29. |
| 1/ 2 | 0.000 | CHBDC | 1 | 318. | 1209. | 1427. | 322. | -19. | 398. | 127. | 29. |
| | | CHBDC | 1 | 227. | 1209. | 1427. | 322. | -19. | 398. | 127. | 29. |
| | | CHBDC | 1 | 227. | 1209. | 1427. | 322. | -19. | 398. | 127. | 29. |
| | | CHBDC | 1 | 317. | 1209. | 1427. | 322. | -19. | 398. | 127. | 29. |
| | | CHBDC | 1 | 318. | 1209. | 1427. | 322. | -19. | 398. | 127. | 29. |
| 1/ 3 | 0.000 | CHBDC | 1 | 195. | 919. | 519. | 326. | -75. | 258. | 229. | 53. |
| | | CHBDC | 1 | 589. | 919. | 519. | 326. | -75. | 258. | 229. | 53. |
| | | CHBDC | 1 | 264. | 919. | 519. | 326. | -75. | 258. | 229. | 53. |
| | | CHBDC | 1 | 193. | 919. | 519. | 326. | -75. | 258. | 229. | 53. |

| SPAN/ SEC | X/L | COMB. TABLE | ULS GRP | MAX/MIN APPLIED SHEAR V _f (kN) | FACTORED SHEAR RESISTANCE V _r (kN) | STIRRUP CAPACITY V _s (kN) | CONCRETE CAPACITY V _c (kN) | PRESTRESS COMPONENT FOR SHEAR V _p (kN) | NOMINAL SHEAR STRESS (v) (kPa) | AV ² (mm) | MIN TOTAL SPACING REQD (mm) | MAX AREA SPACING (mm) | IKODE NOS. |
|--------------|-------|----------------|------------|---|---|---|--|---|--|-------------------------|--------------------------------------|-----------------------------|------------|
| 1/ 4 | 0.200 | CHBDC | 1 | 147. | 773. | 381. | 318. | -75. | 405. | 258. | 305. | 70. | 600. |
| | | CHBDC | 1 | 430. | 773. | 381. | 318. | -75. | 1984. | 258. | 305. | 70. | 600. |
| | | CHBDC | 1 | 66. | 773. | 381. | 318. | -75. | 49. | 258. | 305. | 70. | 600. |
| | | CHBDC | 1 | 669. | 773. | 381. | 318. | -75. | 3314. | 258. | 305. | 70. | 600. |
| | | CHBDC | 1 | 198. | 773. | 381. | 318. | -75. | 691. | 258. | 305. | 70. | 600. |
| | | CHBDC | 1 | 145. | 773. | 381. | 318. | -75. | 391. | 258. | 305. | 70. | 600. |
| 1/ 4 | 0.300 | CHBDC | 1 | 99. | 811. | 401. | 335. | -75. | 129. | 258. | 305. | 70. | 600. |
| | | CHBDC | 1 | 279. | 790. | 397. | 318. | -75. | 1081. | 258. | 305. | 70. | 600. |
| | | CHBDC | 1 | -32. | -661. | 401. | 335. | -75. | 566. | 258. | 305. | 70. | 600. |
| | | CHBDC | 1 | 525. | 719. | 381. | 264. | -75. | 2384. | 258. | 305. | 70. | 600. |
| | | CHBDC | 1 | 132. | 811. | 401. | 335. | -75. | 306. | 258. | 305. | 70. | 600. |
| | | CHBDC | 1 | 96. | 811. | 401. | 335. | -75. | 116. | 258. | 305. | 70. | 600. |
| 1/ 5 | 0.400 | CHBDC | 1 | 51. | 624. | 277. | 347. | 0. | 260. | 258. | 457. | N/C | N/C |
| | | CHBDC | 1 | -52. | -548. | 265. | 283. | 0. | 268. | 258. | 457. | N/C | N/C |
| | | CHBDC | 1 | -137. | -624. | 277. | 347. | 0. | 699. | 258. | 457. | 105. | 600. |
| | | CHBDC | 1 | 381. | 496. | 255. | 241. | 0. | 1951. | 258. | 457. | 105. | 600. |
| | | CHBDC | 1 | 66. | 624. | 277. | 347. | 0. | 339. | 258. | 457. | N/C | N/C |
| | | CHBDC | 1 | 48. | 624. | 277. | 347. | 0. | 247. | 258. | 457. | N/C | N/C |
| 1/ 5 | 0.500 | CHBDC | 1 | -3. | -624. | 277. | 347. | 0. | 13. | 258. | 457. | N/C | N/C |
| | | CHBDC | 1 | 34. | 527. | 261. | 266. | 0. | 172. | 258. | 457. | N/C | N/C |
| | | CHBDC | 1 | -241. | -624. | 277. | 347. | 0. | 1233. | 258. | 457. | 105. | 600. |
| | | CHBDC | 1 | 241. | 559. | 267. | 292. | 0. | 1233. | 258. | 457. | 105. | 600. |

36

Run # 4, Filename: 7108.4b1
Main Span, Exterior Girder, 3 lanes loaded

COMPOSITE PRESTRESSED GIRDER - ULTIMATE LIMIT STATES - FLEXURE

STAGE NUMBER = 2

THE IKODE NUMBER IS GIVEN WHEN A CODE CLAUSE IS VIOLATED.

| IKODE NO. | CODE CLAUSE | SPAN/ SEC | X/L | COMB. TABLE NO. | ULS GROUP | MAX/MIN APPLIED MOMENT (kN-m) | Mf | Mcr | (kN-m) | (kN-m) | CRACKING N.A FROM EXT.COMP FIBRE | Mz/Mf | 1.2Mcr/Mf | 1.33Mf/Mz | c/d | IKODE NOS. |
|-----------|-------------------------------|-----------|-------|-----------------|-----------|-------------------------------|--------|--------|--------|--------|----------------------------------|-------|-----------|-----------|------|------------|
| 30 | 8.8.4.3 MIN. LONGITUDINAL R/F | LC/ 2 | 0.000 | CHBDC | 1 | MIN | -55. | -1748. | -749. | 0.250 | 31.7 | 0.514 | 0.042 | 0.038 | 0.25 | |
| 31 | 8.8.4.5 MAX. LONGITUDINAL R/F | CHBDC | | 1 | MAX | -50. | -1748. | -749. | 0.250 | 35.0 | 0.514 | 0.042 | 0.038 | 0.25 | | |
| 32 | Mf/Mf < 1.0 | CHBDC | | 1 | | -55. | -1748. | -749. | 0.250 | 31.7 | 0.514 | 0.042 | 0.038 | 0.25 | | |
| | | CHBDC | | 1 | | -50. | -1748. | -749. | 0.250 | 35.0 | 0.514 | 0.038 | 0.038 | 0.25 | | |
| | | CHBDC | | 1 | | -55. | -1748. | -749. | 0.250 | 31.7 | 0.514 | 0.042 | 0.042 | 0.25 | | |
| | | CHBDC | | 1 | | -100. | -1728. | -749. | 0.248 | 17.2 | 0.520 | 0.077 | 0.077 | 0.25 | | |
| | | CHBDC | | 1 | | -51. | -1728. | -749. | 0.248 | 34.1 | 0.520 | 0.039 | 0.039 | 0.25 | | |
| | | CHBDC | | 1 | | -100. | -1728. | -749. | 0.248 | 17.2 | 0.520 | 0.077 | 0.077 | 0.25 | | |
| | | CHBDC | | 1 | | -51. | -1728. | -749. | 0.248 | 34.1 | 0.520 | 0.039 | 0.039 | 0.25 | | |
| | | CHBDC | | 1 | | -51. | -1728. | -749. | 0.248 | 34.0 | 0.520 | 0.039 | 0.039 | 0.25 | | |
| | | CHBDC | | 1 | | -100. | -1728. | -749. | 0.248 | 17.2 | 0.520 | 0.077 | 0.077 | 0.25 | | |
| | | CHBDC | | 1 | | -127. | -1843. | -749. | 0.226 | 14.5 | 0.488 | 0.092 | 0.092 | 0.24 | | |
| | | CHBDC | | 1 | | -75. | -1843. | -749. | 0.226 | 24.6 | 0.488 | 0.054 | 0.054 | 0.24 | | |
| | | CHBDC | | 1 | | -83. | -1843. | -749. | 0.226 | 22.3 | 0.488 | 0.060 | 0.060 | 0.24 | | |
| | | CHBDC | | 1 | | -75. | -1843. | -749. | 0.226 | 24.6 | 0.488 | 0.054 | 0.054 | 0.24 | | |
| | | CHBDC | | 1 | | -75. | -1843. | -749. | 0.226 | 24.6 | 0.488 | 0.054 | 0.054 | 0.24 | | |
| | | CHBDC | | 1 | | -127. | -1843. | -749. | 0.226 | 14.5 | 0.488 | 0.092 | 0.092 | 0.24 | | |
| | | CHBDC | | 1 | | 334. | 4559. | 2216. | 0.113 | 13.6 | 0.583 | 0.098 | 0.098 | 0.11 | | |
| | | CHBDC | | 1 | | 1497. | 4559. | 2216. | 0.113 | 3.0 | 0.583 | 0.437 | 0.437 | 0.11 | | |
| | | CHBDC | | 1 | | 866. | 4559. | 2216. | 0.113 | 5.3 | 0.583 | 0.253 | 0.253 | 0.11 | | |
| | | CHBDC | | 1 | | 1497. | 4559. | 2216. | 0.113 | 3.0 | 0.583 | 0.437 | 0.437 | 0.11 | | |
| | | CHBDC | | 1 | | 514. | 4559. | 2216. | 0.113 | 8.9 | 0.583 | 0.150 | 0.150 | 0.11 | | |

LC = LEFT CANTILEVER SECTION
RC = RIGHT CANTILEVER SECTION

|Mr/Mf| = ABSOLUTE VALUE OF Mr/Mf
c/d = FACTOR DEFINED IN 8.8.4.5 ; A NEGATIVE VALUE OF c/d INDICATES Asc > As

SPAN/ X/L COMB. ULS MAX/MIN (FACTORED) CRACKING N.A FROM |Mr/Mf| 1.2Mcr/Mr 1.33ME/Mr c/d IKODE NOS.

SEC TABLE GROUP ULS NO. APPLIED RESISTANCE MOMENT Mr (kN-m) (kN-m) FIBRE EXT. COMP FIBRE

Mf (kN-m) Mr (kN-m) Mcr (kN-m) c

(kN-m) (kN-m) (kN-m) (m)

| SPAN/ SEC | X/L | COMB. TABLE | GROUP ULS NO. | Mf (kN-m) | Mr (kN-m) | Mcr (kN-m) | c (m) | Mr/Mf | 1.2Mcr/Mr | 1.33ME/Mr | c/d | IKODE NOS. |
|-----------|-------|-------------|---------------|-----------|-----------|------------|-------|-------|-----------|-----------|------|------------|
| | | CHBDC | 1 | 374. | 4559. | 2216. | 0.113 | 12.2 | 0.583 | 0.109 | 0.11 | |
| 1/ 4 | 0.200 | CHBDC | 1 MIN | 628. | 4833. | 2313. | 0.113 | 7.7 | 0.574 | 0.173 | 0.11 | |
| | | CHBDC | 1 MAX | 2552. | 4833. | 2313. | 0.113 | 1.9 | 0.574 | 0.702 | 0.11 | |
| | | CHBDC | 1 | 1766. | 4833. | 2313. | 0.113 | 2.7 | 0.574 | 0.486 | 0.11 | |
| | | CHBDC | 1 | 2545. | 4833. | 2313. | 0.113 | 1.9 | 0.574 | 0.700 | 0.11 | |
| | | CHBDC | 1 | 910. | 4833. | 2313. | 0.113 | 5.3 | 0.574 | 0.250 | 0.11 | |
| | | CHBDC | 1 | 663. | 4833. | 2313. | 0.113 | 7.3 | 0.574 | 0.182 | 0.11 | |
| 1/ 4 | 0.300 | CHBDC | 1 MIN | 838. | 5105. | 2447. | 0.113 | 6.1 | 0.575 | 0.218 | 0.10 | |
| | | CHBDC | 1 MAX | 3349. | 5105. | 2447. | 0.113 | 1.5 | 0.575 | 0.872 | 0.10 | |
| | | CHBDC | 1 | 2443. | 5105. | 2447. | 0.113 | 2.1 | 0.575 | 0.637 | 0.10 | |
| | | CHBDC | 1 | 3251. | 5105. | 2447. | 0.113 | 1.6 | 0.575 | 0.847 | 0.10 | |
| | | CHBDC | 1 | 1193. | 5105. | 2447. | 0.113 | 4.3 | 0.575 | 0.311 | 0.10 | |
| | | CHBDC | 1 | 869. | 5105. | 2447. | 0.113 | 5.9 | 0.575 | 0.226 | 0.10 | |
| 1/ 5 | 0.400 | CHBDC | 1 MIN | 966. | 5293. | 2552. | 0.113 | 5.5 | 0.579 | 0.243 | 0.10 | |
| | | CHBDC | 1 MAX | 3763. | 5293. | 2552. | 0.113 | 1.4 | 0.579 | 0.946 | 0.10 | |
| | | CHBDC | 1 | 2930. | 5293. | 2552. | 0.113 | 1.8 | 0.579 | 0.736 | 0.10 | |
| | | CHBDC | 1 | 3565. | 5293. | 2552. | 0.113 | 1.5 | 0.579 | 0.896 | 0.10 | |
| | | CHBDC | 1 | 1362. | 5293. | 2552. | 0.113 | 3.9 | 0.579 | 0.342 | 0.10 | |
| | | CHBDC | 1 | 993. | 5293. | 2552. | 0.113 | 5.3 | 0.579 | 0.249 | 0.10 | |
| 1/ 5 | 0.500 | CHBDC | 1 MIN | 1012. | 5293. | 2533. | 0.113 | 5.2 | 0.574 | 0.254 | 0.10 | |
| | | CHBDC | 1 MAX | 3843. | 5293. | 2533. | 0.113 | 1.4 | 0.574 | 0.966 | 0.10 | |
| | | CHBDC | 1 | 3139. | 5293. | 2533. | 0.113 | 1.7 | 0.574 | 0.789 | 0.10 | |
| | | CHBDC | 1 | 3524. | 5293. | 2533. | 0.113 | 1.5 | 0.574 | 0.886 | 0.10 | |
| | | CHBDC | 1 | 1419. | 5293. | 2533. | 0.113 | 3.7 | 0.574 | 0.357 | 0.10 | |
| | | CHBDC | 1 | 1034. | 5293. | 2533. | 0.113 | 5.1 | 0.574 | 0.260 | 0.10 | |

COMPOSITE PRESTRESSED GIRDER - ULTIMATE LIMIT STATES - SHEAR

STAGE NUMBER = 2

THE IKODE NUMBER IS GIVEN WHEN A CODE CLAUSE IS VIOLATED.
 VIOLATION OF CL 8.9.3.11/12 MAY NOT BE CRITICAL IF USER ENSURES THAT CL 8.9.3.10 IS SATISFIED BY PROPER REBAR DETAILING.
 IKODE NO. N/C ---> NOT CALCULATED, STIRRUPS NOT REQUIRED AS PER CHBDC CLAUSE 8.9.1.2 FOR Vf

33 8.9.3.2
 35 8.9.3.11/12
 36 8.14.6 NOTE: THE APPLICABILITY OF IKODES 36 & 37 FOR SOLID SLAB SECTIONS MUST BE ASCERTAINED BY THE USER.
 37 8.9.1.3

LC = LEFT CANTILEVER SECTION
 RC = RIGHT CANTILEVER SECTION

| SPAN/ SEC | X/L | COMB. TABLE | ULS GRP | MAX/MIN APPLIED SHEAR Vf (kN) | FACTORED SHEAR RESISTANCE Vr (kN) | STIRRUP CAPACITY Vs (kN) | CONCRETE CAPACITY Vc (kN) | PRESTRESS NOMINAL COMPONENT SHEAR FOR SHEAR STRESS AREA Vp (kN) | PRESTRESS NOMINAL TOTAL SHEAR AREA Av (mm ²) | STIRRUPS-> MIN TOTAL SPACING AREA REQD (mm) | MAX SPACING (mm) | IKODE NOS. |
|--------------|-------|----------------|------------|---|---|-----------------------------------|------------------------------------|---|--|---|------------------------|------------|
| | | | | | | | | | | | | |
| LC/ 2 | 0.000 | CHBDC | 1 | -11. | -1192. | 1430. | 322. | 0. | 398. | 127. | N/C | N/C |
| | | CHBDC | 1 | -10. | -1192. | 1430. | 322. | 0. | 398. | 127. | N/C | N/C |
| | | CHBDC | 1 | MIN | -1192. | 1430. | 322. | 0. | 398. | 127. | N/C | N/C |
| | | CHBDC | 1 | MAX | -1192. | 1430. | 322. | 0. | 398. | 127. | N/C | N/C |
| | | CHBDC | 1 | -10. | -1192. | 1430. | 322. | 0. | 398. | 127. | N/C | N/C |
| | | CHBDC | 1 | -11. | -1192. | 1430. | 322. | 0. | 398. | 127. | N/C | N/C |
| LC/ 2 | 1.000 | CHBDC | 1 | -313. | -1190. | 1427. | 322. | 0. | 398. | 127. | 29. | 600. |
| | | CHBDC | 1 | -13. | -1190. | 1427. | 322. | 0. | 398. | 127. | N/C | N/C |
| | | CHBDC | 1 | MIN | -1190. | 1427. | 322. | 0. | 398. | 127. | 29. | 600. |
| | | CHBDC | 1 | MAX | -1190. | 1427. | 322. | 0. | 398. | 127. | N/C | N/C |
| | | CHBDC | 1 | -13. | -1190. | 1427. | 322. | 0. | 398. | 127. | N/C | N/C |
| | | CHBDC | 1 | -15. | -1190. | 1427. | 322. | 0. | 398. | 127. | N/C | N/C |
| | | CHBDC | 1 | -313. | -1190. | 1427. | 322. | 0. | 398. | 127. | 29. | 600. |
| 1/ 2 | 0.000 | CHBDC | 1 | 335. | 1209. | 1427. | 322. | -19. | 398. | 127. | 29. | 600. |
| | | CHBDC | 1 | 240. | 1209. | 1427. | 322. | -19. | 398. | 127. | 29. | 600. |
| | | CHBDC | 1 | MIN | 1209. | 1427. | 322. | -19. | 398. | 127. | 29. | 600. |
| | | CHBDC | 1 | MAX | 1209. | 1427. | 322. | -19. | 398. | 127. | 29. | 600. |
| | | CHBDC | 1 | 994. | 1209. | 1219. | 174. | -19. | 398. | 127. | 29. | 600. |
| | | CHBDC | 1 | 334. | 1209. | 1427. | 322. | -19. | 398. | 127. | 29. | 600. |
| | | CHBDC | 1 | 335. | 1209. | 1427. | 322. | -19. | 398. | 127. | 29. | 600. |
| 1/ 3 | 0.100 | CHBDC | 1 | 191. | 919. | 519. | 326. | -75. | 258. | 229. | 53. | 600. |
| | | CHBDC | 1 | 584. | 919. | 519. | 326. | -75. | 258. | 229. | 53. | 300. |
| | | CHBDC | 1 | MIN | 919. | 519. | 326. | -75. | 258. | 229. | 53. | 600. |
| | | CHBDC | 1 | MAX | 919. | 519. | 326. | -75. | 258. | 229. | 53. | 300. |
| | | CHBDC | 1 | 822. | 919. | 519. | 326. | -75. | 258. | 229. | 53. | 600. |
| | | CHBDC | 1 | 259. | 919. | 519. | 326. | -75. | 258. | 229. | 53. | 600. |
| | | CHBDC | 1 | 189. | 919. | 519. | 326. | -75. | 258. | 229. | 53. | 600. |

| SPAN/ SEC | X/L | COMB. TABLE | ULS GRP | MAX/MIN APPLIED SHEAR Vf (kN) | FACTORED SHEAR RESISTANCE Vr (kN) | STIRRUP CAPACITY Vs (kN) | CONCRETE CAPACITY Vc (kN) | PRESTRESS COMPONENT FOR SHEAR Vp (kN) | NOMINAL SHEAR STRESS (v) (kPa) | ←- STIRRUPS-→ TOTAL SPACING AREA AV (mm) | MIN AREA REQD (mm) | MAX SPACING (mm) | IKODE NOS. | |
|--------------|-------|----------------|------------|---|---|-----------------------------------|------------------------------------|---|--|--|-----------------------------|------------------------|------------|------|
| | | | | | | | | | | | | | | 144. |
| 1/ 4 | 0.200 | CHBDC | 1 | 144. | 773. | 381. | 318. | -75. | 388. | 258. | 305. | 70. | 600. | |
| | | CHBDC | 1 | 426. | 773. | 381. | 318. | -75. | 1961. | 258. | 305. | 70. | 600. | |
| | | CHBDC | 1 | 63. | 773. | 381. | 318. | -75. | 66. | 258. | 305. | 70. | 600. | |
| | | CHBDC | 1 | 665. | 773. | 381. | 318. | -75. | 3291. | 258. | 305. | 70. | 300. | 36 |
| | | CHBDC | 1 | 194. | 773. | 381. | 318. | -75. | 668. | 258. | 305. | 70. | 600. | |
| | | CHBDC | 1 | 142. | 773. | 381. | 318. | -75. | 374. | 258. | 305. | 70. | 600. | |
| 1/ 4 | 0.300 | CHBDC | 1 | 97. | 811. | 401. | 335. | -75. | 118. | 258. | 305. | 70. | 600. | |
| | | CHBDC | 1 | 276. | 802. | 399. | 328. | -75. | 1067. | 258. | 305. | 70. | 600. | |
| | | CHBDC | 1 | -34. | -661. | 401. | 335. | -75. | 577. | 258. | 305. | 70. | 600. | |
| | | CHBDC | 1 | 522. | 728. | 383. | 270. | -75. | 2370. | 258. | 305. | 70. | 600. | |
| | | CHBDC | 1 | 130. | 811. | 401. | 335. | -75. | 291. | 258. | 305. | 70. | 600. | |
| | | CHBDC | 1 | 94. | 811. | 401. | 335. | -75. | 105. | 258. | 305. | 70. | 600. | |
| 1/ 5 | 0.400 | CHBDC | 1 | 50. | 624. | 277. | 347. | 0. | 255. | 258. | 457. | N/C | N/C | |
| | | CHBDC | 1 | -54. | -556. | 267. | 290. | 0. | 275. | 258. | 457. | N/C | N/C | |
| | | CHBDC | 1 | -138. | -624. | 277. | 347. | 0. | 704. | 258. | 457. | 105. | 600. | |
| | | CHBDC | 1 | 380. | 503. | 257. | 247. | 0. | 1944. | 258. | 457. | 105. | 600. | |
| | | CHBDC | 1 | 65. | 624. | 277. | 347. | 0. | 332. | 258. | 457. | N/C | N/C | |
| | | CHBDC | 1 | 47. | 624. | 277. | 347. | 0. | 242. | 258. | 457. | N/C | N/C | |
| 1/ 5 | 0.500 | CHBDC | 1 | -3. | -624. | 277. | 347. | 0. | 13. | 258. | 457. | N/C | N/C | |
| | | CHBDC | 1 | 34. | 536. | 263. | 273. | 0. | 172. | 258. | 457. | N/C | N/C | |
| | | CHBDC | 1 | -241. | -624. | 277. | 347. | 0. | 1233. | 258. | 457. | 105. | 600. | |
| | | CHBDC | 1 | 241. | 569. | 269. | 301. | 0. | 1233. | 258. | 457. | 105. | 600. | |

Run # 4, Filename: 7108.4b1

Main Span, Exterior Girder, 3 lanes loaded

UNFACTORED RESPONSE - FORCES AND MOMENTS DUE TO NON-MOVING LOADS FOR BRIDGE TYPE 1

STAGE NUMBER = 1

RESPONSE IS GIVEN WITH RESPECT TO ELEMENT AXES.

FOR COLUMN SUPPORTS IN BRIDGE TYPE 3, THE X1 AXIS IS IN THE DIRECTION FROM THE TOP OF COLUMN TO BOTTOM, WITH THE X2 AXIS IN THE SAME DIRECTION AS THE AXIS OF THE BRIDGE (GLOBAL X1) AND THE X3 AXIS IN THE SAME DIRECTION AS THE GLOBAL X2.

- LC = LEFT CANTILEVER.
- RC = RIGHT CANTILEVER.
- LSC = LEFT SPAN CONTRIBUTION (BRIDGE TYPE 1 ONLY).
- RSC = RIGHT SPAN CONTRIBUTION (BRIDGE TYPE 1 ONLY).
- COL = ELEMENT IS A COLUMN (BRIDGE TYPE 3 ONLY).
- SPR = ELEMENT IS A SPRING (BRIDGE TYPE 3 ONLY).

| SPAN ID | SEC ID | SPAN X/L | LOAD # | LOAD KIND | FX1 | FX2 | FX3 | MOMENT (kN.m) | MX1 | MX2 | MX3 |
|---------|--------|----------|--------|-----------|---------|-------|------|---------------|--------|--------|-----|
| LC | 2 | 0.000 | 1 | D1 | 0.0 | | -0.1 | | | 0.0 | |
| | 2 | | P | -287.9 | | -10.2 | | | -52.6 | | |
| | 3 | | D2 | 0.0 | | 0.0 | | | 0.0 | | |
| LC | 2 | 1.000 | 1 | D1 | 0.0 | | -1.3 | | | -0.1 | |
| | 2 | | P | -287.9 | | -10.2 | | | -54.1 | | |
| | 3 | | D2 | 0.0 | | -1.5 | | | -0.1 | | |
| 1 | 2 | 0.000 | 1 | D1 | 0.0 | | 77.3 | | | -0.1 | |
| | 2 | | P | -1003.8 | | -35.1 | | | -188.5 | | |
| | 3 | | D2 | 0.0 | | 105.4 | | | -0.1 | | |
| 1 | 3 | 0.100 | 1 | D1 | 0.0 | | 61.8 | | | 121.5 | |
| | 2 | | P | -2257.9 | | -78.5 | | | -563.4 | | |
| | 3 | | D2 | 0.0 | | 68.3 | | | 137.8 | | |
| 1 | 4 | 0.200 | 1 | D1 | 0.0 | | 46.4 | | | 216.1 | |
| | 2 | | P | -2257.9 | | -78.5 | | | -700.7 | | |
| | 3 | | D2 | 0.0 | | 51.2 | | | 242.3 | | |
| 1 | 4 | 0.300 | 1 | D1 | 0.0 | | 30.9 | | | 283.7 | |
| | 2 | | P | -2257.9 | | -78.5 | | | -837.9 | | |
| | 3 | | D2 | 0.0 | | 34.1 | | | 316.9 | | |
| 1 | 5 | 0.400 | 1 | D1 | 0.0 | | 15.5 | | | 324.2 | |
| | 2 | | P | -2262.0 | | -0.1 | | | -934.5 | | |
| | 3 | | D2 | 0.0 | | 17.1 | | | 361.7 | | |
| 1 | 5 | 0.500 | 1 | D1 | 0.0 | | -0.1 | | | 337.8 | |
| | | | 2 | P | -2262.0 | | 0.0 | | | -934.6 | |

| SPAN ID | SEC ID | SPAN X/L | LOAD # | LOAD KIND | FX1 | FX2 | FX3 | MOMENT (kN m) |
|---------|--------|----------|--------|-----------|-----|-----|-----|---------------|
| | | | 3 | D2 | 0.0 | 0.0 | 0.0 | 376.6 |

UNFACTORED RESPONSE - FORCES AND MOMENTS DUE TO NON-MOVING LOADS FOR BRIDGE TYPE 1

STAGE NUMBER = 2

RESPONSE IS GIVEN WITH RESPECT TO ELEMENT AXES.

FOR COLUMN SUPPORTS IN BRIDGE TYPE 3, THE X1 AXIS IS IN THE DIRECTION FROM THE TOP OF COLUMN TO BOTTOM, WITH THE X2 AXIS IN THE SAME DIRECTION AS THE AXIS OF THE BRIDGE (GLOBAL X1) AND THE X3 AXIS IN THE SAME DIRECTION AS THE GLOBAL X2.

- LC = LEFT CANTILEVER.
- RC = RIGHT CANTILEVER.
- LSC = LEFT SPAN CONTRIBUTION (BRIDGE TYPE 1 ONLY).
- RSC = RIGHT SPAN CONTRIBUTION (BRIDGE TYPE 1 ONLY).
- COL = ELEMENT IS A COLUMN (BRIDGE TYPE 3 ONLY).
- SPR = ELEMENT IS A SPRING (BRIDGE TYPE 3 ONLY).

| SPAN ID | SEC ID | SPAN X/L | LOAD # | LOAD KIND | FX1 | FX2 | FX3 | MX1 | MX2 | MX3 |
|---------|--------|----------|--------|-----------|---------|-----|-------|-----|--------|-----|
| LC | 2 | 0.000 | 2 | P | -287.9 | | -10.2 | | -52.6 | |
| | 5 | | D2 | 0.0 | | | -0.1 | | -0.1 | |
| | 6 | | D4 | 0.0 | | | -0.1 | | -0.1 | |
| IC | 2 | 1.000 | 2 | P | -287.9 | | -10.2 | | -54.1 | |
| | 5 | | D2 | 0.0 | | | -1.2 | | -0.1 | |
| | 6 | | D4 | 0.0 | | | -0.6 | | -0.1 | |
| 1 | 2 | 0.000 | 2 | P | -1003.8 | | -35.1 | | -188.5 | |
| | 5 | | D2 | 0.0 | | | 69.9 | | -0.1 | |
| | 6 | | D4 | 0.0 | | | 35.0 | | -0.1 | |
| 1 | 3 | 0.100 | 2 | P | -2257.9 | | -78.5 | | -563.4 | |
| | 5 | | D2 | 0.0 | | | 55.9 | | 109.9 | |
| | 6 | | D4 | 0.0 | | | 28.0 | | 55.0 | |
| 1 | 4 | 0.200 | 2 | P | -2257.9 | | -78.5 | | -700.7 | |
| | 5 | | D2 | 0.0 | | | 42.0 | | 195.5 | |
| | 6 | | D4 | 0.0 | | | 21.0 | | 97.8 | |
| 1 | 4 | 0.300 | 2 | P | -2257.9 | | -78.5 | | -837.9 | |
| | 5 | | D2 | 0.0 | | | 28.0 | | 256.6 | |
| | 6 | | D4 | 0.0 | | | 14.0 | | 128.3 | |
| 1 | 5 | 0.400 | 2 | P | -2262.0 | | -0.1 | | -934.5 | |
| | 5 | | D2 | 0.0 | | | 14.0 | | 293.3 | |
| | 6 | | D4 | 0.0 | | | 7.0 | | 146.7 | |
| 1 | 5 | 0.500 | 2 | P | -2262.0 | | 0.0 | | -934.6 | |
| | 5 | | D2 | 0.0 | | | -0.1 | | 305.5 | |

| SPAN ID | SEC ID | SPAN X/L | LOAD # | LOAD KIND | FX1 | FX2 | FX3 | MOMENT MX1 | MOMENT MX2 | MOMENT MX3 |
|---------|--------|----------|--------|-----------|-----|-----|------|------------|------------|------------|
| | | | 6 | D4 | 0.0 | | -0.1 | | | 152.8 |

UNFACTORED RESPONSE - FORCES AND MOMENTS DUE TO MOVING LOADS FOR BRIDGE TYPE 1

STAGE NUMBER = 2

RESPONSE IS GIVEN WITH RESPECT TO ELEMENT AXES.

FOR COLUMN SUPPORTS IN BRIDGE TYPE 3, THE X1 AXIS IS IN THE DIRECTION FROM THE TOP OF COLUMN TO BOTTOM, WITH THE X2 AXIS IN THE SAME DIRECTION AS THE AXIS OF THE BRIDGE (GLOBAL X1) AND THE X3 AXIS IN THE SAME DIRECTION AS THE GLOBAL X2.

OPTIMIZED COMPONENT IS MARKED BY "**".

IN SOME CASES OPTIMIZATION MAY NOT PRODUCE BOTH A MAXIMUM (POSITIVE) AND MINIMUM (NEGATIVE) VALUE.

- LC = LEFT CANTILEVER.
- RC = RIGHT CANTILEVER.
- LSC = LEFT SPAN CONTRIBUTION (BRIDGE TYPE 1 ONLY).
- RSC = RIGHT SPAN CONTRIBUTION (BRIDGE TYPE 1 ONLY).
- COL = ELEMENT IS A COLUMN (BRIDGE TYPE 3 ONLY).
- SPR = ELEMENT IS A SPRING (BRIDGE TYPE 3 ONLY).

- GOV LD = GOVERNING LOAD
- TR = TRUCK LOAD
- LA = LANE LOAD
- PE = PEDESTRIAN LOAD (CLAUSE 3.8.9)
- MTR = MAINTENANCE TRUCK LOAD

| SPAN SEC | ID | X/L | # | KIND | LD-> | FORCE (kN) | | | MOMENT (kN m) | | | |
|----------|----|-------|---|------|------|------------|-----|-----|---------------|-----|-----|------|
| | | | | | | FX1 | FX2 | FX3 | MX1 | MX2 | MX3 | |
| LC | 2 | 0.000 | 7 | L | MAX: | 0.0* | | | 0.0 | | | 0.0 |
| | | | | | MIN: | 0.0* | | | 0.0 | | | 0.0 |
| | | | | | MAX: | 0.0 | | | 0.0* | | | 0.0 |
| | | | | | MIN: | 0.0 | | | 0.0* | | | 0.0 |
| | | | | | MAX: | 0.0 | | | 0.0 | | | 0.0* |
| | | | | | MIN: | 0.0 | | | 0.0 | | | 0.0* |
| | 8 | | | L | MAX: | 0.0* | | | 0.0 | | | 0.0 |
| | | | | | MIN: | 0.0* | | | 0.0 | | | 0.0 |
| | | | | | MAX: | 0.0 | | | 0.0* | | | 0.0 |
| | | | | | MIN: | 0.0 | | | 0.0* | | | 0.0 |
| | | | | | MAX: | 0.0 | | | 0.0 | | | 0.0* |
| | | | | | MIN: | 0.0 | | | 0.0 | | | 0.0* |
| | 9 | | | L | MAX: | 0.0* | | | 0.0 | | | 0.0 |
| | | | | | MIN: | 0.0* | | | 0.0 | | | 0.0 |
| | | | | | MAX: | 0.0 | | | 0.0* | | | 0.0 |
| | | | | | MIN: | 0.0 | | | 0.0* | | | 0.0 |
| | | | | | MAX: | 0.0 | | | 0.0 | | | 0.0* |
| | | | | | MIN: | 0.0 | | | 0.0 | | | 0.0* |

| SPAN ID | SEC ID | SPAN X/L | LOAD # | LOAD KIND | LD-> DECK SDWLK | FX1 | FX2 | FX3 | MX1 | MX2 | MX3 | |
|---------|--------|----------|--------|-----------|-----------------|-----------|-----------|-------|-----|--------|-----|--|
| 1 | 2 | 0.000 | 7 | L | | MAX: 0.0* | | 0.0 | | 0.0 | | |
| | | | | | | MIN: 0.0* | | 0.0 | | 0.0 | | |
| | | | | | | MAX: 0.0 | | 0.0* | | 0.0 | | |
| | | | | | | MIN: 0.0 | | 0.0* | | 0.0 | | |
| | | | | | | MAX: 0.0 | | 0.0 | | 0.0* | | |
| | | | | | | MIN: 0.0 | | 0.0 | | 0.0* | | |
| | | TR | | | | 328.8* | | 0.0 | | 0.0 | | |
| | | TR | | | | -1.4* | | 0.0 | | 0.0 | | |
| | | TR | | | | 0.0 | | 0.0* | | 0.0* | | |
| | | TR | | | | 0.0 | | 1.4 | | -19.2* | | |
| | | TR | | | | 0.0 | | 0.0 | | 0.0 | | |
| | 1 | 2 | 1.000 | 7 | L | | MAX: 0.0* | | 0.0 | | 0.0 | |
| | | | | | | MIN: 0.0* | | 0.0 | | 0.0 | | |
| | | | | | | MAX: 0.0 | | 0.0* | | 0.0 | | |
| | | | | | | MIN: 0.0 | | 0.0* | | 0.0 | | |
| | | | | | | MAX: 0.0 | | 0.0 | | 0.0* | | |
| | | | | | | MIN: 0.0 | | 0.0 | | 0.0* | | |
| | | TR | | | | -165.9* | | -19.2 | | 0.0 | | |
| | | TR | | | | -165.9 | | 0.0 | | 0.0 | | |
| | | TR | | | | 0.0 | | 0.0 | | 0.0 | | |
| | | TR | | | | 0.0 | | 0.0 | | 0.0 | | |
| 1 | | 2 | 0.000 | 7 | L | | MAX: 0.0* | | 0.0 | | 0.0 | |
| | | | | | | | MIN: 0.0* | | 0.0 | | 0.0 | |
| | | | | | | MAX: 0.0 | | 0.0* | | 0.0 | | |
| | | | | | | MIN: 0.0 | | 0.0* | | 0.0 | | |
| | | | | | | MAX: 0.0 | | 0.0 | | 0.0* | | |
| | | | | | | MIN: 0.0 | | 0.0 | | 0.0* | | |
| | | TR | | | | -174.8* | | -25.1 | | 0.0 | | |
| | | TR | | | | -174.8 | | 0.0 | | 0.0 | | |
| | | TR | | | | 0.0 | | 0.0 | | 0.0 | | |
| | | TR | | | | 0.0 | | 0.0 | | 0.0 | | |
| | 1 | 2 | 1.000 | 7 | L | | MAX: 0.0* | | 0.0 | | 0.0 | |
| | | | | | | | MIN: 0.0* | | 0.0 | | 0.0 | |
| | | | | | | MAX: 0.0 | | 0.0* | | 0.0 | | |
| | | | | | | MIN: 0.0 | | 0.0* | | 0.0 | | |
| | | | | | | MAX: 0.0 | | 0.0 | | 0.0* | | |
| | | | | | | MIN: 0.0 | | 0.0 | | 0.0* | | |
| | | TR | | | | -174.8* | | -25.1 | | 0.0 | | |
| | | TR | | | | -174.8 | | 0.0 | | 0.0 | | |
| | | TR | | | | 0.0 | | 0.0 | | 0.0 | | |
| | | TR | | | | 0.0 | | 0.0 | | 0.0 | | |
| 1 | | 2 | 0.000 | 7 | L | | MAX: 0.0* | | 0.0 | | 0.0 | |
| | | | | | | | MIN: 0.0* | | 0.0 | | 0.0 | |
| | | | | | | MAX: 0.0 | | 0.0* | | 0.0 | | |
| | | | | | | MIN: 0.0 | | 0.0* | | 0.0 | | |
| | | | | | | MAX: 0.0 | | 0.0 | | 0.0* | | |
| | | | | | | MIN: 0.0 | | 0.0 | | 0.0* | | |
| | | TR | | | | -175.0* | | -26.1 | | 0.0 | | |
| | | TR | | | | -175.0 | | 0.0 | | 0.0 | | |
| | | TR | | | | 0.0 | | 0.0 | | 0.0 | | |
| | | TR | | | | 0.0 | | 0.0 | | 0.0 | | |
| | 1 | 2 | 1.000 | 7 | L | | MAX: 0.0* | | 0.0 | | 0.0 | |
| | | | | | | | MIN: 0.0* | | 0.0 | | 0.0 | |
| | | | | | | MAX: 0.0 | | 0.0* | | 0.0 | | |
| | | | | | | MIN: 0.0 | | 0.0* | | 0.0 | | |
| | | | | | | MAX: 0.0 | | 0.0 | | 0.0* | | |
| | | | | | | MIN: 0.0 | | 0.0 | | 0.0* | | |
| | | TR | | | | 346.5* | | 0.0 | | 0.0 | | |
| | | TR | | | | -1.5* | | 0.0 | | 0.0 | | |
| | | TR | | | | 0.0 | | 0.0 | | 0.0 | | |
| | | TR | | | | 0.0 | | 1.5 | | -25.1* | | |

| SPAN ID | SEC ID | SPAN X/L | LOAD # | LOAD KIND | LD-> | FORCE (kN) | | | MOMENT (kN m) | | | |
|---------|--------|----------|--------|-----------|------|------------|------|--------|---------------|-----|--------|--------|
| | | | | | | FX1 | FX2 | FX3 | MX1 | MX2 | MX3 | |
| 9 | L | | | | | MAX: | 0.0* | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| | | | | | | MIN: | 0.0* | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| | | | | | | TR | 0.0 | 346.5* | 0.0 | 0.0 | 0.0 | 0.0 |
| | | | | | | TR | 0.0 | -1.5* | 0.0 | 0.0 | 0.0 | 0.0 |
| | | | | | | TR | 0.0 | 0.0 | 0.0* | 0.0 | 0.0* | -25.1* |
| | | | | | | TR | 0.0 | 1.5 | 0.0 | 0.0 | 0.0 | 0.0 |
| 10 | L | | | | | MAX: | 0.0* | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| | | | | | | MIN: | 0.0* | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| | | | | | | TR | 0.0 | 388.5* | 0.0 | 0.0 | 0.0 | 0.0 |
| | | | | | | TR | 0.0 | -1.5* | 0.0 | 0.0 | 0.0 | 0.0 |
| | | | | | | TR | 0.0 | 0.0 | 0.0* | 0.0 | 0.0* | -26.1* |
| | | | | | | TR | 0.0 | 1.5 | 0.0 | 0.0 | 0.0 | 0.0 |
| 1 | 3 | 0.100 | 7 | L | | MAX: | 0.0* | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| | | | | | | MIN: | 0.0* | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| | | | | | | TR | 0.0 | 280.2* | 0.0 | 0.0 | 380.6 | 0.0 |
| | | | | | | TR | 0.0 | -16.2* | 0.0 | 0.0 | 198.0 | 0.0 |
| | | | | | | TR | 0.0 | 161.7 | 0.0 | 0.0 | 380.6* | 0.0 |
| | | | | | | TR | 0.0 | 1.4 | 0.0 | 0.0 | -17.3* | 0.0 |
| 8 | L | | | | | MAX: | 0.0* | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| | | | | | | MIN: | 0.0* | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| | | | | | | TR | 0.0 | 295.2* | 0.0 | 0.0 | 496.5 | 0.0 |
| | | | | | | TR | 0.0 | -17.1* | 0.0 | 0.0 | 258.2 | 0.0 |
| | | | | | | TR | 0.0 | 170.3 | 0.0 | 0.0 | 496.5* | 0.0 |
| | | | | | | TR | 0.0 | 1.5 | 0.0 | 0.0 | -22.6* | 0.0 |
| 9 | L | | | | | MAX: | 0.0* | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| | | | | | | MIN: | 0.0* | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| | | | | | | TR | 0.0 | 295.2* | 0.0 | 0.0 | 496.5 | 0.0 |
| | | | | | | TR | 0.0 | -17.1* | 0.0 | 0.0 | 258.2 | 0.0 |
| | | | | | | TR | 0.0 | 170.3 | 0.0 | 0.0 | 496.5* | 0.0 |
| | | | | | | TR | 0.0 | 1.5 | 0.0 | 0.0 | -22.6* | 0.0 |
| 10 | L | | | | | MAX: | 0.0* | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| | | | | | | MIN: | 0.0* | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| | | | | | | TR | 0.0 | 331.0* | 0.0 | 0.0 | 578.6 | 0.0 |
| | | | | | | TR | 0.0 | -18.4* | 0.0 | 0.0 | 289.3 | 0.0 |
| | | | | | | TR | 0.0 | 191.0 | 0.0 | 0.0 | 578.6* | 0.0 |
| | | | | | | TR | 0.0 | 1.5 | 0.0 | 0.0 | -23.5* | 0.0 |
| 1 | 4 | 0.200 | 7 | L | | MAX: | 0.0* | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| | | | | | | MIN: | 0.0* | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| | | | | | | TR | 0.0 | 234.2* | 0.0 | 0.0 | 632.8 | 0.0 |
| | | | | | | TR | 0.0 | -40.8* | 0.0 | 0.0 | 443.9 | 0.0 |
| | | | | | | TR | 0.0 | 115.4 | 0.0 | 0.0 | 635.6* | 0.0 |
| | | | | | | TR | 0.0 | 1.4 | 0.0 | 0.0 | -15.4* | 0.0 |

| SPAN ID | SEC ID | SPAN X/L | LOAD # | LOAD KIND | LD-> DECK SDWLK | FX1 | FX2 | FX3 | MX1 | MX2 | MX3 |
|---------|--------|----------|--------|-----------|--------------------|-------------|--------|--------|-------|-----|-----|
| 1 | 4 | 0.300 | 7 | L | | MAX: 0.0* | | 0.0 | | 0.0 | |
| | | | | | | MIN: 0.0* | 0.0 | | 0.0 | | |
| | | | | | TR | MAX: 246.7* | 246.7* | | 825.5 | | |
| | | | | | TR | MIN: -43.0* | -43.0* | | 579.0 | | |
| 1 | 9 | L | L | | MAX: 0.0* | | 0.0 | | 0.0 | | 0.0 |
| | | | | | MIN: 0.0* | 0.0 | | 0.0 | | 0.0 | |
| | | | | TR | MAX: 246.7* | 246.7* | | 825.5 | | | |
| | | | | TR | MIN: -43.0* | -43.0* | | 579.0 | | | |
| 1 | 10 | L | L | | MAX: 0.0* | | 0.0 | | 0.0 | | 0.0 |
| | | | | | MIN: 0.0* | 0.0 | | 0.0 | | 0.0 | |
| | | | | TR | MAX: 276.6* | 276.6* | | 961.9 | | | |
| | | | | TR | MIN: -46.4* | -46.4* | | 648.8 | | | |
| 1 | 4 | 0.300 | 7 | L | | MAX: 0.0* | | 0.0 | | 0.0 | |
| | | | | | | MIN: 0.0* | 0.0 | | 0.0 | | 0.0 |
| | | | | | TR | MAX: 195.4* | 195.4* | | 796.4 | | |
| | | | | | TR | MIN: -66.6* | -66.6* | | 633.5 | | |
| 1 | 8 | L | L | | MAX: 0.0* | | 0.0 | | 0.0 | | 0.0 |
| | | | | | MIN: 0.0* | 0.0 | | 0.0 | | 0.0 | |
| | | | | TR | MAX: 205.9* | 205.9* | | 1038.8 | | | |
| | | | | TR | MIN: -70.2* | -70.2* | | 826.3 | | | |
| 1 | 9 | L | L | | MAX: 0.0* | | 0.0 | | 0.0 | | 0.0 |
| | | | | | MIN: 0.0* | 0.0 | | 0.0 | | 0.0 | |
| | | | | TR | MAX: 205.9* | 205.9* | | 1038.8 | | | |
| | | | | TR | MIN: -70.2* | -70.2* | | 826.3 | | | |
| 1 | 10 | L | L | | MAX: 0.0* | | 0.0 | | 0.0 | | 0.0 |
| | | | | | MIN: 0.0* | 0.0 | | 0.0 | | 0.0 | |
| | | | | TR | MAX: 230.8* | 230.8* | | 1210.5 | | | |
| | | | | TR | MIN: -75.7* | -75.7* | | 925.9 | | | |

| SPAN ID | SEC ID | SPAN X/L | LOAD # | LOAD KIND | LOAD ID | DECK | FORCE (kN) | | | MOMENT (kN m) | | |
|---------|--------|----------|--------|-----------|---------|------|------------|------|---------|---------------|---------|-----|
| | | | | | | | FX1 | FX2 | FX3 | MX1 | MX2 | MX3 |
| 1 | 5 | 0.400 | 7 | L | | | MAX: | 0.0* | 0.0 | 0.0 | 0.0 | 0.0 |
| | | | | | | | MIN: | 0.0* | 0.0 | 0.0 | 0.0 | 0.0 |
| | | | | | | | TR | | 156.9* | | 852.5 | |
| | | | | | | | TR | | -95.7* | | 779.8 | |
| | | | | | | | TR | | 0.0 | | 928.9* | |
| | | | | | | | TR | | 0.0 | | -11.5* | |
| | | | | | | | TR | | 0.0 | | 1.4 | |
| | | | | | | | MAX: | 0.0* | 0.0 | 0.0 | 0.0 | 0.0 |
| | | | | | | | MIN: | 0.0* | 0.0 | 0.0 | 0.0 | 0.0 |
| | | | | | | | TR | | 165.3* | | 1112.0 | |
| | | | | | | | TR | | -100.8* | | 1017.2 | |
| | | | | | | | TR | | -62.2 | | 1211.7* | |
| TR | | 0.0 | | -15.0* | | | | | | | | |
| 1 | 5 | 0.500 | 7 | L | | | MAX: | 0.0* | 0.0 | 0.0 | 0.0 | |
| | | | | | | | MIN: | 0.0* | 0.0 | 0.0 | 0.0 | |
| | | | | | | | TR | | 185.3* | | 1295.8 | |
| | | | | | | | TR | | -108.7* | | 1139.8 | |
| | | | | | | | TR | | 0.0 | | 1412.0* | |
| | | | | | | | TR | | 0.0 | | -69.7 | |
| | | | | | | | TR | | 0.0 | | 1.5 | |
| | | | | | | | MAX: | 0.0* | 0.0 | 0.0 | 0.0 | 0.0 |
| | | | | | | | MIN: | 0.0* | 0.0 | 0.0 | 0.0 | 0.0 |
| | | | | | | | TR | | 124.7* | | 847.2 | |
| | | | | | | | TR | | -124.7* | | 937.9* | |
| | | | | | | | TR | | 16.7 | | -9.6* | |
| TR | | 0.0 | | -1.4 | | | | | | | | |
| 1 | 5 | 0.400 | 8 | L | | | MAX: | 0.0* | 0.0 | 0.0 | 0.0 | |
| | | | | | | | MIN: | 0.0* | 0.0 | 0.0 | 0.0 | |
| | | | | | | | TR | | 131.4* | | 1105.1 | |
| | | | | | | | TR | | -131.4* | | 1105.1 | |
| | | | | | | | TR | | 0.0 | | 1223.4* | |
| | | | | | | | TR | | 0.0 | | -12.5* | |
| | | | | | | | TR | | 0.0 | | -1.5 | |
| | | | | | | | MAX: | 0.0* | 0.0 | 0.0 | 0.0 | 0.0 |
| | | | | | | | MIN: | 0.0* | 0.0 | 0.0 | 0.0 | 0.0 |
| | | | | | | | TR | | 131.4* | | 1105.1 | |
| | | | | | | | TR | | -131.4* | | 1105.1 | |
| | | | | | | | TR | | 0.0 | | 1223.4* | |
| TR | | 0.0 | | -12.5* | | | | | | | | |
| 1 | 5 | 0.400 | 9 | L | | | MAX: | 0.0* | 0.0 | 0.0 | 0.0 | |
| | | | | | | | MIN: | 0.0* | 0.0 | 0.0 | 0.0 | |
| | | | | | | | TR | | 131.4* | | 1105.1 | |
| | | | | | | | TR | | -131.4* | | 1105.1 | |
| | | | | | | | TR | | 0.0 | | 1223.4* | |
| | | | | | | | TR | | 0.0 | | -12.5* | |
| | | | | | | | TR | | 0.0 | | -1.5 | |
| | | | | | | | MAX: | 0.0* | 0.0 | 0.0 | 0.0 | 0.0 |
| | | | | | | | MIN: | 0.0* | 0.0 | 0.0 | 0.0 | 0.0 |
| | | | | | | | TR | | 131.4* | | 1105.1 | |
| | | | | | | | TR | | -131.4* | | 1105.1 | |
| | | | | | | | TR | | 0.0 | | 1223.4* | |
| TR | | 0.0 | | -12.5* | | | | | | | | |

| SPAN ID | SEC ID | SPAN X/L | LOAD # | LOAD KIND | LD-> DECK SDWLK | FX1 | FX2 | FX3 | MX1 | MX2 | MX3 |
|---------|--------|----------|--------|-----------|--------------------|------|---------|-----|-----|---------|-----|
| 10 | | | L | | | 0.0* | 0.0 | 0.0 | | 0.0 | 0.0 |
| | | | | | | 0.0* | 0.0 | 0.0 | | 1238.3 | 0.0 |
| | TR | | | | | 0.0 | 141.7* | 0.0 | | 1238.3 | 0.0 |
| | TR | | | | | 0.0 | -141.7* | 0.0 | | 1425.6* | 0.0 |
| | TR | | | | | 0.0 | 19.8 | 0.0 | | -13.0* | 0.0 |
| | TR | | | | | 0.0 | -1.5 | 0.0 | | | 0.0 |

Run 9; Filename 7108.9b1

COMPOSITE PRESTRESSED GIRDER - ULTIMATE LIMIT STATES - FLEXURE

STAGE NUMBER = 2

THE IKODE NUMBER IS GIVEN WHEN A CODE CLAUSE IS VIOLATED.

IKODE NO. CODE CLAUSE
 30 8.8.4.3 MIN. LONGITUDINAL R/F
 31 8.8.4.5 MAX. LONGITUDINAL R/F
 32 |Mr/Mf| < 1.0

IC = LEFT CANTILEVER SECTION
 RC = RIGHT CANTILEVER SECTION
 |Mr/Mf| = ABSOLUTE VALUE OF Mr/Mf
 c/d = FACTOR DEFINED IN 8.8.4.5 ; A NEGATIVE VALUE OF c/d INDICATES Asc > As

| SPAN/ SEC | X/L | COMB. TABLE NO. | ULS GROUP | MAX/MIN APPLIED MOMENT (kN-m) | Mf | Mr | (kN-m) | (FACTORED) RESISTANCE MOMENT | CRACKING N.A FROM EXT.COMP FIBRE | Mr/Mf | 1.2McI/Mr | 1.33Mf/Mr | c/d | IKODE NOS. | |
|-----------|-------|-----------------|-----------|-------------------------------|--------|--------|--------|------------------------------|----------------------------------|-------|-----------|-----------|------|------------|--|
| LC/ 2 | 0.000 | CHBDC | 1 MIN | -33. | -1645. | -901. | 0.214 | 50.3 | 0.657 | 0.026 | 0.21 | 0.21 | 0.21 | | |
| | | | 1 MAX | -30. | -1645. | -901. | 0.214 | 55.6 | 0.657 | 0.024 | 0.21 | 0.21 | 0.21 | | |
| | | | CHBDC | 1 | -30. | -1645. | -901. | 0.214 | 55.6 | 0.657 | 0.024 | 0.21 | 0.21 | 0.21 | |
| | | | CHBDC | 1 | -30. | -1645. | -901. | 0.214 | 55.6 | 0.657 | 0.024 | 0.21 | 0.21 | 0.21 | |
| LC/ 3 | 1.000 | CHBDC | 1 MIN | -135. | -1722. | -901. | 0.208 | 12.8 | 0.628 | 0.104 | 0.23 | 0.23 | 0.23 | | |
| | | | 1 MAX | -30. | -1722. | -901. | 0.208 | 57.3 | 0.628 | 0.100 | 0.23 | 0.23 | 0.23 | | |
| | | | CHBDC | 1 | -129. | -1722. | -901. | 0.208 | 13.4 | 0.628 | 0.025 | 0.23 | 0.23 | 0.23 | |
| | | | CHBDC | 1 | -33. | -1722. | -901. | 0.208 | 52.2 | 0.628 | 0.024 | 0.23 | 0.23 | 0.23 | |
| 1/ 3 | 0.000 | CHBDC | 1 MIN | -146. | -1739. | -901. | 0.212 | 11.9 | 0.622 | 0.112 | 0.24 | 0.24 | 0.24 | | |
| | | | 1 MAX | -41. | -1739. | -901. | 0.212 | 42.8 | 0.622 | 0.031 | 0.24 | 0.24 | 0.24 | | |
| | | | CHBDC | 1 | -41. | -1739. | -901. | 0.212 | 42.8 | 0.622 | 0.035 | 0.24 | 0.24 | 0.24 | |
| | | | CHBDC | 1 | -45. | -1739. | -901. | 0.212 | 38.3 | 0.622 | 0.032 | 0.24 | 0.24 | 0.24 | |
| 1/ 4 | 0.100 | CHBDC | 1 MIN | 108. | 3558. | 1687. | 0.086 | 33.0 | 0.569 | 0.040 | 0.09 | 0.09 | 0.09 | | |
| | | | 1 MAX | 853. | 3558. | 1687. | 0.086 | 4.2 | 0.569 | 0.319 | 0.09 | 0.09 | 0.09 | | |
| | | | CHBDC | 1 | 521. | 3558. | 1687. | 0.086 | 6.8 | 0.569 | 0.195 | 0.09 | 0.09 | 0.09 | |
| | | | CHBDC | 1 | 853. | 3558. | 1687. | 0.086 | 4.2 | 0.569 | 0.319 | 0.09 | 0.09 | 0.09 | |
| CHBDC | 1 | 277. | 3558. | 1687. | 0.086 | 12.9 | 0.569 | 0.103 | 0.09 | 0.09 | 0.09 | | | | |

| SPAN/ SEC | X/L | COMP. TABLE NO. | ULS GROUP NO. | MAX/MIN APPLIED MOMENT (kN-m) | (FACTORED) RESISTANCE MOMENT (kN-m) | CRACKING MOMENT (kN-m) | N.A FROM EXT. COMP FIBRE C (m) | Mr/Mf | 1.2McI/Mr | 1.33Mf/Mr | c/d | IKODE NOS. |
|--------------|-------|--------------------|------------------|--|--|------------------------------|--|-------|-----------|-----------|------|------------|
| 1/ 5 | 0.200 | CHBDC | 1 | 199. | 3558. | 1687. | 0.086 | 17.9 | 0.569 | 0.074 | 0.09 | |
| | | CHBDC | 1 | 274. | 3558. | 1601. | 0.086 | 13.0 | 0.540 | 0.102 | 0.09 | |
| | | CHBDC | 1 | 1460. | 3558. | 1601. | 0.086 | 2.4 | 0.540 | 0.546 | 0.09 | |
| | | CHBDC | 1 | 1042. | 3558. | 1601. | 0.086 | 3.4 | 0.540 | 0.389 | 0.09 | |
| | | CHBDC | 1 | 1460. | 3558. | 1601. | 0.086 | 2.4 | 0.540 | 0.546 | 0.09 | |
| | | CHBDC | 1 | 494. | 3558. | 1601. | 0.086 | 7.2 | 0.540 | 0.185 | 0.09 | |
| | | CHBDC | 1 | 355. | 3558. | 1601. | 0.086 | 10.0 | 0.540 | 0.133 | 0.09 | |
| 1/ 5 | 0.300 | CHBDC | 1 | 396. | 3558. | 1539. | 0.086 | 9.0 | 0.519 | 0.148 | 0.09 | |
| | | CHBDC | 1 | 1857. | 3558. | 1539. | 0.086 | 1.9 | 0.519 | 0.694 | 0.09 | |
| | | CHBDC | 1 | 1468. | 3558. | 1539. | 0.086 | 2.4 | 0.519 | 0.549 | 0.09 | |
| | | CHBDC | 1 | 1857. | 3558. | 1539. | 0.086 | 1.9 | 0.519 | 0.694 | 0.09 | |
| | | CHBDC | 1 | 649. | 3558. | 1539. | 0.086 | 5.5 | 0.519 | 0.243 | 0.09 | |
| | | CHBDC | 1 | 466. | 3558. | 1539. | 0.086 | 7.6 | 0.519 | 0.174 | 0.09 | |
| 1/ 6 | 0.400 | CHBDC | 1 | 473. | 3558. | 1502. | 0.086 | 7.5 | 0.507 | 0.177 | 0.09 | |
| | | CHBDC | 1 | 2083. | 3558. | 1502. | 0.086 | 1.7 | 0.507 | 0.779 | 0.09 | |
| | | CHBDC | 1 | 1735. | 3558. | 1502. | 0.086 | 2.1 | 0.507 | 0.649 | 0.09 | |
| | | CHBDC | 1 | 2083. | 3558. | 1502. | 0.086 | 1.7 | 0.507 | 0.779 | 0.09 | |
| | | CHBDC | 1 | 742. | 3558. | 1502. | 0.086 | 4.8 | 0.507 | 0.278 | 0.09 | |
| | | CHBDC | 1 | 533. | 3558. | 1502. | 0.086 | 6.7 | 0.507 | 0.199 | 0.09 | |
| 1/ 6 | 0.500 | CHBDC | 1 | 505. | 3558. | 1490. | 0.086 | 7.0 | 0.502 | 0.189 | 0.09 | |
| | | CHBDC | 1 | 2163. | 3558. | 1490. | 0.086 | 1.6 | 0.502 | 0.809 | 0.09 | |
| | | CHBDC | 1 | 1894. | 3558. | 1490. | 0.086 | 1.9 | 0.502 | 0.708 | 0.09 | |
| | | CHBDC | 1 | 2112. | 3558. | 1490. | 0.086 | 1.7 | 0.502 | 0.790 | 0.09 | |
| | | CHBDC | 1 | 774. | 3558. | 1490. | 0.086 | 4.6 | 0.502 | 0.289 | 0.09 | |
| | | CHBDC | 1 | 556. | 3558. | 1490. | 0.086 | 6.4 | 0.502 | 0.208 | 0.09 | |
| 1/ 6 | 0.600 | CHBDC | 1 | 493. | 3558. | 1502. | 0.086 | 7.2 | 0.507 | 0.184 | 0.09 | |
| | | CHBDC | 1 | 2083. | 3558. | 1502. | 0.086 | 1.7 | 0.507 | 0.779 | 0.09 | |
| | | CHBDC | 1 | 2083. | 3558. | 1502. | 0.086 | 1.7 | 0.507 | 0.779 | 0.09 | |
| | | CHBDC | 1 | 1735. | 3558. | 1502. | 0.086 | 2.1 | 0.507 | 0.649 | 0.09 | |
| | | CHBDC | 1 | 743. | 3558. | 1502. | 0.086 | 4.8 | 0.507 | 0.278 | 0.09 | |
| | | CHBDC | 1 | 533. | 3558. | 1502. | 0.086 | 6.7 | 0.507 | 0.199 | 0.09 | |
| 1/ 7 | 0.700 | CHBDC | 1 | 435. | 3558. | 1539. | 0.086 | 8.2 | 0.519 | 0.163 | 0.09 | |
| | | CHBDC | 1 | 1858. | 3558. | 1539. | 0.086 | 1.9 | 0.519 | 0.694 | 0.09 | |
| | | CHBDC | 1 | 1858. | 3558. | 1539. | 0.086 | 1.9 | 0.519 | 0.694 | 0.09 | |
| | | CHBDC | 1 | 1468. | 3558. | 1539. | 0.086 | 2.4 | 0.519 | 0.549 | 0.09 | |
| | | CHBDC | 1 | 650. | 3558. | 1539. | 0.086 | 5.5 | 0.519 | 0.243 | 0.09 | |
| | | CHBDC | 1 | 467. | 3558. | 1539. | 0.086 | 7.6 | 0.519 | 0.175 | 0.09 | |
| 1/ 7 | 0.800 | CHBDC | 1 | 319. | 3558. | 1600. | 0.086 | 11.1 | 0.540 | 0.119 | 0.09 | |
| | | CHBDC | 1 | 1461. | 3558. | 1600. | 0.086 | 2.4 | 0.540 | 0.546 | 0.09 | |
| | | CHBDC | 1 | 1461. | 3558. | 1600. | 0.086 | 2.4 | 0.540 | 0.546 | 0.09 | |
| | | CHBDC | 1 | 1042. | 3558. | 1600. | 0.086 | 3.4 | 0.540 | 0.390 | 0.09 | |

| SPAN/ SEC | X/L | COMB. TABLE GROUP NO. | ULS GROUP NO. | MAX/MIN APPLIED MOMENT (kN-m) | (FACTORED) RESISTANCE MOMENT Mf (kN-m) | CRACKING MOMENT Mcr (kN-m) | N.A FROM EXT.COMP FIBRE C (m) | Mr/Mf | 1.2Mcr/Mr | 1.33Mf/Mr | c/d | IKODE NOS. |
|--------------|-------|--------------------------------|---------------------|--|--|-------------------------------------|---|-------|-----------|-----------|------|------------|
| 1/ 8 | 0.900 | CHBDC | 1 | 495. | 3558. | 1600. | 0.086 | 7.2 | 0.540 | 0.185 | 0.09 | |
| | | | | 356. | 3558. | 1600. | 0.086 | 10.0 | 0.540 | 0.133 | 0.09 | |
| 1/ 8 | 0.900 | CHBDC | 1 | 159. | 3558. | 1686. | 0.086 | 22.4 | 0.569 | 0.059 | 0.09 | |
| | | | | 854. | 3558. | 1686. | 0.086 | 4.2 | 0.569 | 0.319 | 0.09 | |
| | | | | 854. | 3558. | 1686. | 0.086 | 4.2 | 0.569 | 0.319 | 0.09 | |
| | | | | 522. | 3558. | 1686. | 0.086 | 6.8 | 0.569 | 0.195 | 0.09 | |
| | | | | 278. | 3558. | 1686. | 0.086 | 12.8 | 0.569 | 0.104 | 0.09 | |
| | | | | 200. | 3558. | 1686. | 0.086 | 17.8 | 0.569 | 0.075 | 0.09 | |
| 1/ 9 | 1.000 | CHBDC | 1 | -89. | -1707. | -901. | 0.205 | 19.1 | 0.634 | 0.069 | 0.22 | |
| | | | | -39. | -1707. | -901. | 0.205 | 43.4 | 0.634 | 0.031 | 0.22 | |
| | | | | -44. | -1707. | -901. | 0.205 | 39.2 | 0.634 | 0.034 | 0.22 | |
| | | | | -39. | -1707. | -901. | 0.205 | 43.4 | 0.634 | 0.031 | 0.22 | |
| | | | | -39. | -1707. | -901. | 0.205 | 43.3 | 0.634 | 0.031 | 0.22 | |
| | | | | -89. | -1707. | -901. | 0.205 | 19.1 | 0.634 | 0.069 | 0.22 | |
| RC/ 9 | 0.000 | CHBDC | 1 | -8. | -1706. | -901. | 0.205 | *** | 0.634 | 0.006 | 0.22 | |
| | | | | 42. | 3554. | 792. | 0.086 | 84.2 | 0.267 | 0.016 | 0.09 | |
| | | | | 42. | 3554. | 792. | 0.086 | 84.2 | 0.267 | 0.016 | 0.09 | |
| | | | | 38. | 3554. | 792. | 0.086 | 93.4 | 0.267 | 0.014 | 0.09 | |
| | | | | 42. | 3554. | 792. | 0.086 | 84.4 | 0.267 | 0.016 | 0.09 | |
| | | | | -8. | -1706. | -901. | 0.205 | *** | 0.634 | 0.006 | 0.22 | |
| RC/ 9 | 1.000 | CHBDC | 1 | -43. | -1645. | -901. | 0.214 | 38.6 | 0.657 | 0.034 | 0.21 | |
| | | | | -39. | -1645. | -901. | 0.214 | 42.7 | 0.657 | 0.031 | 0.21 | |
| | | | | -39. | -1645. | -901. | 0.214 | 42.7 | 0.657 | 0.031 | 0.21 | |
| | | | | -43. | -1645. | -901. | 0.214 | 38.6 | 0.657 | 0.034 | 0.21 | |
| | | | | -39. | -1645. | -901. | 0.214 | 42.7 | 0.657 | 0.031 | 0.21 | |
| | | | | -43. | -1645. | -901. | 0.214 | 38.6 | 0.657 | 0.034 | 0.21 | |

COMPOSITE PRESTRESSED GIRDER - ULTIMATE LIMIT STATES - SHEAR

STAGE NUMBER = 2

THE IKODE NUMBER IS GIVEN WHEN A CODE CLAUSE IS VIOLATED.
 VIOLATION OF CL. 8.9.3.11/12 MAY NOT BE CRITICAL IF USER ENSURES THAT CL. 8.9.3.10 IS SATISFIED BY PROPER REBAR DETAILING.
 IKODE NO. CODE CLAUSE N/C ---> NOT CALCULATED, STIRRUPS NOT REQUIRED AS PER CHBDC CLAUSE 8.9.1.2 FOR V_f

33 8.9.3.2
 35 8.9.3.11/12
 36 8.14.6
 37 8.9.1.3

LC = LEFT CANTILEVER SECTION
 RC = RIGHT CANTILEVER SECTION

NOTE: THE APPLICABILITY OF IKODES 36 & 37 FOR SOLID SLAB SECTIONS MUST BE ASCERTAINED BY THE USER.

| SPAN/ SEC | X/L | COMB. TABLE | ULS GRP | MAX/MIN APPLIED SHEAR | FACTORED SHEAR RESISTANCE | V _s (kN) | V _c (kN) | CONCRETE CAPACITY | COMPONENT SHEAR FOR SHEAR STRESS AREA | PRESTRESS NOMINAL <- STIRRUPS-> TOTAL SPACING AREA REQD | MIN (mm) | MAX (mm) | IKODE NOS. |
|--------------|-------|----------------|------------|-----------------------------|---------------------------------|------------------------|------------------------|----------------------|--|--|-------------|-------------|------------|
| LC/ 2 | 0.000 | | | | | | | | | | | | |
| LC/ 3 | 1.000 | | | -311. | -1223. | 1220. | 324. | 0. | 1671. | 398. | 152. | 35. | 600. |
| | | | | -10. | -1223. | 1225. | 331. | 0. | 55. | 398. | 152. | N/C | N/C |
| | | | 1 MIN | -312. | -1223. | 1218. | 321. | 0. | 1673. | 398. | 152. | 35. | 600. |
| | | | 1 MAX | -10. | -1223. | 1225. | 331. | 0. | 55. | 398. | 152. | N/C | N/C |
| | | | | -14. | -1223. | 1225. | 331. | 0. | 76. | 398. | 152. | N/C | N/C |
| | | | | -311. | -1223. | 1220. | 324. | 0. | 1671. | 398. | 152. | 35. | 600. |
| 1/ 3 | | | | 266. | 1223. | 1225. | 331. | 0. | 1429. | 398. | 152. | 35. | 600. |
| | | | | 185. | 1223. | 1225. | 331. | 0. | 995. | 398. | 152. | 35. | 600. |
| | | | 1 MIN | 182. | 1223. | 1225. | 331. | 0. | 975. | 398. | 152. | 35. | 600. |
| | | | 1 MAX | 115. | 1036. | 1036. | 173. | 0. | 4373. | 398. | 152. | 35. | 300. |
| | | | | 258. | 1223. | 1225. | 331. | 0. | 1385. | 398. | 152. | 35. | 600. |
| | | | | 266. | 1223. | 1225. | 331. | 0. | 1429. | 398. | 152. | 35. | 600. |
| 1/ 4 | | | | 156. | 876. | 539. | 338. | 0. | 822. | 258. | 229. | 53. | 600. |
| | | | | 448. | 876. | 539. | 338. | 0. | 2352. | 258. | 229. | 53. | 600. |
| | | | 1 MIN | 110. | 676. | 539. | 338. | 0. | 623. | 258. | 229. | 53. | 600. |
| | | | 1 MAX | 186. | 676. | 539. | 338. | 0. | 3603. | 258. | 229. | 53. | 300. |
| | | | | 207. | 876. | 539. | 338. | 0. | 1085. | 258. | 229. | 53. | 600. |
| | | | | 148. | 876. | 539. | 338. | 0. | 779. | 258. | 229. | 53. | 600. |
| 1/ 5 | | | | 119. | 742. | 404. | 338. | 0. | 627. | 258. | 305. | 70. | 600. |
| | | | | 319. | 742. | 404. | 338. | 0. | 1675. | 258. | 305. | 70. | 600. |
| | | | 1 MIN | 110. | 742. | 404. | 338. | 0. | 209. | 258. | 305. | N/C | N/C |
| | | | 1 MAX | 157. | 742. | 404. | 338. | 0. | 2925. | 258. | 305. | 70. | 300. |

**** OPTIMIZED SHEAR = 0.0 - RESISTANCE NOT DONE ****

SPAN/ X/L COMB. TABLE ULS GRP MAX/MIN APPLIED SHEAR V_f (kN) FACTORED SHEAR RESISTANCE V_t (kN) STIRRUP CAPACITY Vs (kN) CONCRETE CAPACITY V_c (kN) PRESTRESS COMPONENT FOR SHEAR V_p (kN) NOMINAL SHEAR (v) (kPa) TOTAL SPACING AREA REQD (mm) MIN SPACING (mm) MAX SPACING (mm) IKODE NOS.

| SPAN/ X/L | COMB. TABLE | ULS GRP | MAX/MIN APPLIED SHEAR V _f (kN) | FACTORED SHEAR RESISTANCE V _t (kN) | STIRRUP CAPACITY Vs (kN) | CONCRETE CAPACITY V _c (kN) | PRESTRESS COMPONENT FOR SHEAR V _p (kN) | NOMINAL SHEAR (v) (kPa) | TOTAL SPACING AREA REQD (mm) | MIN SPACING (mm) | MAX SPACING (mm) | IKODE NOS. |
|-----------|-------------|---------|---|---|--------------------------|---------------------------------------|---|-------------------------|------------------------------|------------------|------------------|------------|
| 1/ 5 | 0.300 | 1 | 155. | 742. | 404. | 338. | 0. | 814. | 258. | 305. | 70. | 600. |
| | | 1 | 111. | 742. | 404. | 338. | 0. | 584. | 258. | 305. | 70. | 600. |
| 1/ 5 | 0.300 | 1 | 82. | 742. | 404. | 338. | 0. | 433. | 258. | 305. | 70. | 600. |
| | | 1 | 200. | 742. | 404. | 338. | 0. | 1052. | 258. | 305. | 70. | 600. |
| | | 1 | -45. | -742. | 404. | 338. | 0. | 235. | 258. | 305. | N/C | N/C |
| | | 1 | 438. | 652. | 385. | 267. | 0. | 2302. | 258. | 305. | 70. | 600. |
| | | 1 | 103. | 742. | 404. | 338. | 0. | 543. | 258. | 305. | 70. | 600. |
| | | 1 | 74. | 742. | 404. | 338. | 0. | 390. | 258. | 305. | 70. | 600. |
| 1/ 6 | 0.400 | 1 | 45. | 608. | 270. | 338. | 0. | 238. | 258. | 457. | N/C | N/C |
| | | 1 | 93. | 608. | 270. | 338. | 0. | 487. | 258. | 457. | 105. | 600. |
| | | 1 | -130. | -608. | 270. | 338. | 0. | 680. | 258. | 457. | 105. | 600. |
| | | 1 | 331. | 471. | 246. | 225. | 0. | 1737. | 258. | 457. | 105. | 600. |
| | | 1 | 52. | 608. | 270. | 338. | 0. | 272. | 258. | 457. | N/C | N/C |
| | | 1 | 37. | 608. | 270. | 338. | 0. | 195. | 258. | 457. | N/C | N/C |
| 1/ 6 | 0.500 | 1 | 8. | 608. | 270. | 338. | 0. | 43. | 258. | 457. | N/C | N/C |
| | | 1 | -41. | -603. | 269. | 334. | 0. | 214. | 258. | 457. | N/C | N/C |
| | | 1 | -223. | -608. | 270. | 338. | 0. | 1170. | 258. | 457. | 105. | 600. |
| | | 1 | 223. | 511. | 254. | 256. | 0. | 1171. | 258. | 457. | 105. | 600. |
| | | 1 | 0. | 608. | 270. | 338. | 0. | 1. | 258. | 457. | N/C | N/C |
| | | 1 | 0. | 608. | 270. | 338. | 0. | 1. | 258. | 457. | N/C | N/C |
| 1/ 6 | 0.600 | 1 | -29. | -608. | 270. | 338. | 0. | 151. | 258. | 457. | N/C | N/C |
| | | 1 | -92. | -608. | 270. | 338. | 0. | 485. | 258. | 457. | 105. | 600. |
| | | 1 | -330. | -471. | 246. | 225. | 0. | 1735. | 258. | 457. | 105. | 600. |
| | | 1 | 130. | 608. | 270. | 338. | 0. | 682. | 258. | 457. | 105. | 600. |
| | | 1 | -51. | -608. | 270. | 338. | 0. | 270. | 258. | 457. | N/C | N/C |
| | | 1 | -37. | -608. | 270. | 338. | 0. | 194. | 258. | 457. | N/C | N/C |
| 1/ 7 | 0.700 | 1 | -78. | -742. | 404. | 338. | 0. | 408. | 258. | 305. | 70. | 600. |
| | | 1 | -200. | -742. | 404. | 338. | 0. | 1051. | 258. | 305. | 70. | 600. |
| | | 1 | -438. | -651. | 385. | 267. | 0. | 2301. | 258. | 305. | 70. | 600. |
| | | 1 | 45. | 742. | 404. | 338. | 0. | 237. | 258. | 305. | N/C | N/C |
| | | 1 | -103. | -742. | 404. | 338. | 0. | 541. | 258. | 305. | 70. | 600. |
| | | 1 | -74. | -742. | 404. | 338. | 0. | 389. | 258. | 305. | 70. | 600. |
| 1/ 7 | 0.800 | 1 | -115. | -742. | 404. | 338. | 0. | 603. | 258. | 305. | 70. | 600. |
| | | 1 | -319. | -742. | 404. | 338. | 0. | 1673. | 258. | 305. | 70. | 600. |
| | | 1 | -557. | -742. | 404. | 338. | 0. | 2924. | 258. | 305. | 70. | 300. |
| | | 1 | -40. | -742. | 404. | 338. | 0. | 208. | 258. | 305. | N/C | N/C |
| | | 1 | -155. | -742. | 404. | 338. | 0. | 812. | 258. | 305. | 70. | 600. |
| | | 1 | -111. | -742. | 404. | 338. | 0. | 583. | 258. | 305. | 70. | 600. |
| 1/ 8 | 0.900 | 1 | -152. | -876. | 539. | 338. | 0. | 797. | 258. | 229. | 53. | 600. |

SPAN/ X/L COMB. TABLE ULS GRP ULS GRP MAX/MIN APPLIED SHEAR V_f (kN) FACTORED SHEAR RESISTANCE V_r (kN) STIRRUP CAPACITY Vs (kN) CONCRETE CAPACITY V_c (kN) PRESTRESS COMPONENT FOR SHEAR V_p (kN) PRESTRESS NOMINAL COMPONENT SHEAR FOR SHEAR V_p (kPa) MIN TOTAL SPACING AREA REQD (mm) MAX TOTAL SPACING AREA REQD (mm) IKODE NOS.

| SPAN/ X/L COMB. TABLE ULS GRP ULS GRP | MAX/MIN APPLIED SHEAR V _f (kN) | FACTORED SHEAR RESISTANCE V _r (kN) | STIRRUP CAPACITY Vs (kN) | CONCRETE CAPACITY V _c (kN) | PRESTRESS COMPONENT FOR SHEAR V _p (kN) | PRESTRESS NOMINAL COMPONENT SHEAR FOR SHEAR V _p (kPa) | MIN TOTAL SPACING AREA REQD (mm) | MAX TOTAL SPACING AREA REQD (mm) | IKODE NOS. |
|---------------------------------------|---|---|--------------------------|---------------------------------------|---|--|----------------------------------|----------------------------------|------------|
| 1/ 9 | CHBDC 1 | 448. | -876. | 539. | 338. | 0. | 2351. | 229. | 53. 600. |
| | CHBDC 1 | 686. | -876. | 539. | 338. | 0. | 3601. | 229. | 53. 300. |
| | CHBDC 1 | 118. | -876. | 539. | 338. | 0. | 622. | 229. | 53. 600. |
| | CHBDC 1 | 206. | -876. | 539. | 338. | 0. | 1083. | 229. | 53. 600. |
| | CHBDC 1 | 148. | -876. | 539. | 338. | 0. | 778. | 229. | 53. 600. |
| | CHBDC 1 | 261. | -1223. | 1046. | 331. | 0. | 1404. | 178. | 41. 600. |
| | CHBDC 1 | 185. | -1223. | 1046. | 331. | 0. | 994. | 178. | 41. 600. |
| | CHBDC 1 | 177. | 885. | 173. | 173. | 0. | 4372. | 178. | 41. 300. |
| | CHBDC 1 | 258. | 1046. | 331. | 331. | 0. | 950. | 178. | 41. 600. |
| | CHBDC 1 | 261. | 1046. | 331. | 331. | 0. | 1384. | 178. | 41. 600. |
| | CHBDC 1 | 261. | 1046. | 331. | 331. | 0. | 1404. | 178. | 41. 600. |
| RC/ 9 | CHBDC 1 | 304. | 1223. | 1011. | 280. | 0. | 1630. | 178. | 41. 600. |
| | CHBDC 1 | 5. | 1249. | 1069. | 338. | 0. | 24. | 178. | N/C N/C |
| | CHBDC 1 | 5. | 1249. | 1069. | 338. | 0. | 24. | 178. | N/C N/C |
| | CHBDC 1 | 304. | 1249. | 1069. | 338. | 0. | 1596. | 178. | 41. 600. |
| | CHBDC 1 | 6. | 1249. | 1069. | 338. | 0. | 34. | 178. | N/C N/C |
| | CHBDC 1 | 304. | 1223. | 1011. | 280. | 0. | 1630. | 178. | 41. 600. |
| RC/ 9 | CHBDC 1 | 297. | 1223. | 1046. | 331. | 0. | 1597. | 178. | 41. 600. |



Run A: Filename: 7108.ab1

STAGE NUMBER = 2

THE IKODE NUMBER IS GIVEN WHEN A CODE CLAUSE IS VIOLATED.

IKODE NO. CODE CLAUSE

30 8.8.4.3 MIN. LONGITUDINAL R/F
 31 8.8.4.5 MAX. LONGITUDINAL R/F
 32 |Mr/Mf| < 1.0

LC = LEFT CANTILEVER SECTION
 RC = RIGHT CANTILEVER SECTION

|Mr/Mf| = ABSOLUTE VALUE OF Mr/Mf

c/d = FACTOR DEFINED IN 8.8.4.5 ; A NEGATIVE VALUE OF c/d INDICATES Asc > As

SPAN/ X/L COMB. ULS MAX/MIN (FACTORED) CRACKING N.A FROM |Mr/Mf| 1.2McI/Mr 1.33Mf/Mr c/d IKODE NOS.

SEC TABLE GROUP APPLIED RESISTANCE MOMENT EXT. COMP FIBRE

NO. MOMENT Mr McI Mf C (kN-m) (kN-m) (m)

| | | | | | | | | | | | | |
|-------|-------|-------|---|-----|-------|--------|-------|-------|------|-------|-------|------|
| LC/ 2 | 0.000 | CHBDC | 1 | MIN | -33. | -1645. | -860. | 0.214 | 50.3 | 0.627 | 0.026 | 0.21 |
| | | CHBDC | 1 | MAX | -30. | -1645. | -860. | 0.214 | 55.6 | 0.627 | 0.024 | 0.21 |
| | | CHBDC | 1 | | -30. | -1645. | -860. | 0.214 | 55.6 | 0.627 | 0.024 | 0.21 |
| | | CHBDC | 1 | | -30. | -1645. | -860. | 0.214 | 55.6 | 0.627 | 0.024 | 0.21 |
| | | CHBDC | 1 | | -30. | -1645. | -860. | 0.214 | 55.6 | 0.627 | 0.024 | 0.21 |
| | | CHBDC | 1 | | -33. | -1645. | -860. | 0.214 | 50.3 | 0.627 | 0.026 | 0.21 |
| LC/ 3 | 1.000 | CHBDC | 1 | MIN | -135. | -1722. | -860. | 0.208 | 12.8 | 0.599 | 0.104 | 0.23 |
| | | CHBDC | 1 | MAX | -30. | -1722. | -860. | 0.208 | 57.4 | 0.599 | 0.023 | 0.23 |
| | | CHBDC | 1 | | -129. | -1722. | -860. | 0.208 | 13.4 | 0.599 | 0.099 | 0.23 |
| | | CHBDC | 1 | | -33. | -1722. | -860. | 0.208 | 52.2 | 0.599 | 0.025 | 0.23 |
| | | CHBDC | 1 | | -31. | -1722. | -860. | 0.208 | 56.3 | 0.599 | 0.024 | 0.23 |
| | | CHBDC | 1 | | -135. | -1722. | -860. | 0.208 | 12.8 | 0.599 | 0.104 | 0.23 |
| 1/ 3 | 0.000 | CHBDC | 1 | MIN | -146. | -1739. | -860. | 0.212 | 11.9 | 0.593 | 0.112 | 0.24 |
| | | CHBDC | 1 | MAX | -41. | -1739. | -860. | 0.212 | 42.9 | 0.593 | 0.031 | 0.24 |
| | | CHBDC | 1 | | -41. | -1739. | -860. | 0.212 | 42.9 | 0.593 | 0.031 | 0.24 |
| | | CHBDC | 1 | | -45. | -1739. | -860. | 0.212 | 38.4 | 0.593 | 0.035 | 0.24 |
| | | CHBDC | 1 | | -41. | -1739. | -860. | 0.212 | 42.2 | 0.593 | 0.032 | 0.24 |
| | | CHBDC | 1 | | -146. | -1739. | -860. | 0.212 | 11.9 | 0.593 | 0.112 | 0.24 |
| 1/ 4 | 0.100 | CHBDC | 1 | MIN | 102. | 3548. | 1680. | 0.092 | 34.8 | 0.568 | 0.038 | 0.10 |
| | | CHBDC | 1 | MAX | 844. | 3548. | 1680. | 0.092 | 4.2 | 0.568 | 0.316 | 0.10 |
| | | CHBDC | 1 | | 515. | 3548. | 1680. | 0.092 | 6.9 | 0.568 | 0.193 | 0.10 |
| | | CHBDC | 1 | | 844. | 3548. | 1680. | 0.092 | 4.2 | 0.568 | 0.316 | 0.10 |
| | | CHBDC | 1 | | 268. | 3548. | 1680. | 0.092 | 13.3 | 0.568 | 0.100 | 0.10 |

| SPAN/ SEC | X/L | COMB. TABLE NO. | ULS GROUP | MAX/MIN APPLIED MOMENT (kN-m) | Mf | (kN-m) | Mf | (kN-m) | CRACKING MOMENT (kN-m) | Mcr | (kN-m) | C | (m) | N.A FROM EXT. COMP FIBRE | Mr/Mf | 1.2Mcr/Mf | 1.33Mf/Mf | c/d | IKODE NOS. |
|--------------|-------|-----------------------|--------------|--|----|--------|----|--------|------------------------------|------|--------|-------|------|--------------------------------|-------|-----------|-----------|-----|------------|
| | | CHBDC | 1 | 193. | | 3548. | | 1680. | 0.092 | 18.4 | 0.568 | 0.072 | 0.10 | | | | | | |
| 1/ 5 | 0.200 | CHBDC | 1 | 263. | | 3548. | | 1599. | 0.092 | 13.5 | 0.541 | 0.099 | 0.10 | | | | | | |
| | | CHBDC | 1 | 1444. | | 3548. | | 1599. | 0.092 | 2.5 | 0.541 | 0.541 | 0.10 | | | | | | |
| | | CHBDC | 1 | 1031. | | 3548. | | 1599. | 0.092 | 3.4 | 0.541 | 0.386 | 0.10 | | | | | | |
| | | CHBDC | 1 | 1444. | | 3548. | | 1599. | 0.092 | 2.5 | 0.541 | 0.541 | 0.10 | | | | | | |
| | | CHBDC | 1 | 478. | | 3548. | | 1599. | 0.092 | 7.4 | 0.541 | 0.179 | 0.10 | | | | | | |
| | | CHBDC | 1 | 344. | | 3548. | | 1599. | 0.092 | 10.3 | 0.541 | 0.129 | 0.10 | | | | | | |
| 1/ 5 | 0.300 | CHBDC | 1 | 381. | | 3548. | | 1540. | 0.092 | 9.3 | 0.521 | 0.143 | 0.10 | | | | | | |
| | | CHBDC | 1 | 1835. | | 3548. | | 1540. | 0.092 | 1.9 | 0.521 | 0.688 | 0.10 | | | | | | |
| | | CHBDC | 1 | 1454. | | 3548. | | 1540. | 0.092 | 2.4 | 0.521 | 0.545 | 0.10 | | | | | | |
| | | CHBDC | 1 | 1835. | | 3548. | | 1540. | 0.092 | 1.9 | 0.521 | 0.688 | 0.10 | | | | | | |
| | | CHBDC | 1 | 628. | | 3548. | | 1540. | 0.092 | 5.7 | 0.521 | 0.235 | 0.10 | | | | | | |
| | | CHBDC | 1 | 452. | | 3548. | | 1540. | 0.092 | 7.8 | 0.521 | 0.170 | 0.10 | | | | | | |
| 1/ 6 | 0.400 | CHBDC | 1 | 456. | | 3548. | | 1505. | 0.092 | 7.8 | 0.509 | 0.171 | 0.10 | | | | | | |
| | | CHBDC | 1 | 2058. | | 3548. | | 1505. | 0.092 | 1.7 | 0.509 | 0.772 | 0.10 | | | | | | |
| | | CHBDC | 1 | 1719. | | 3548. | | 1505. | 0.092 | 2.1 | 0.509 | 0.644 | 0.10 | | | | | | |
| | | CHBDC | 1 | 2058. | | 3548. | | 1505. | 0.092 | 1.7 | 0.509 | 0.772 | 0.10 | | | | | | |
| | | CHBDC | 1 | 718. | | 3548. | | 1505. | 0.092 | 4.9 | 0.509 | 0.269 | 0.10 | | | | | | |
| | | CHBDC | 1 | 517. | | 3548. | | 1505. | 0.092 | 6.9 | 0.509 | 0.194 | 0.10 | | | | | | |
| 1/ 6 | 0.500 | CHBDC | 1 | 488. | | 3548. | | 1493. | 0.092 | 7.3 | 0.505 | 0.183 | 0.10 | | | | | | |
| | | CHBDC | 1 | 2137. | | 3548. | | 1493. | 0.092 | 1.7 | 0.505 | 0.801 | 0.10 | | | | | | |
| | | CHBDC | 1 | 1877. | | 3548. | | 1493. | 0.092 | 1.9 | 0.505 | 0.704 | 0.10 | | | | | | |
| | | CHBDC | 1 | 2086. | | 3548. | | 1493. | 0.092 | 1.7 | 0.505 | 0.782 | 0.10 | | | | | | |
| | | CHBDC | 1 | 748. | | 3548. | | 1493. | 0.092 | 4.7 | 0.505 | 0.280 | 0.10 | | | | | | |
| | | CHBDC | 1 | 539. | | 3548. | | 1493. | 0.092 | 6.6 | 0.505 | 0.202 | 0.10 | | | | | | |
| 1/ 6 | 0.600 | CHBDC | 1 | 477. | | 3548. | | 1505. | 0.092 | 7.4 | 0.509 | 0.179 | 0.10 | | | | | | |
| | | CHBDC | 1 | 2059. | | 3548. | | 1505. | 0.092 | 1.7 | 0.509 | 0.772 | 0.10 | | | | | | |
| | | CHBDC | 1 | 1719. | | 3548. | | 1505. | 0.092 | 1.7 | 0.509 | 0.772 | 0.10 | | | | | | |
| | | CHBDC | 1 | 718. | | 3548. | | 1505. | 0.092 | 2.1 | 0.509 | 0.645 | 0.10 | | | | | | |
| | | CHBDC | 1 | 517. | | 3548. | | 1505. | 0.092 | 4.9 | 0.509 | 0.269 | 0.10 | | | | | | |
| 1/ 7 | 0.700 | CHBDC | 1 | 421. | | 3548. | | 1540. | 0.092 | 8.4 | 0.521 | 0.158 | 0.10 | | | | | | |
| | | CHBDC | 1 | 1836. | | 3548. | | 1540. | 0.092 | 1.9 | 0.521 | 0.688 | 0.10 | | | | | | |
| | | CHBDC | 1 | 1454. | | 3548. | | 1540. | 0.092 | 2.4 | 0.521 | 0.545 | 0.10 | | | | | | |
| | | CHBDC | 1 | 628. | | 3548. | | 1540. | 0.092 | 5.6 | 0.521 | 0.236 | 0.10 | | | | | | |
| | | CHBDC | 1 | 453. | | 3548. | | 1540. | 0.092 | 7.8 | 0.521 | 0.170 | 0.10 | | | | | | |
| 1/ 7 | 0.800 | CHBDC | 1 | 308. | | 3548. | | 1598. | 0.092 | 11.5 | 0.541 | 0.116 | 0.10 | | | | | | |
| | | CHBDC | 1 | 1445. | | 3548. | | 1598. | 0.092 | 2.5 | 0.541 | 0.542 | 0.10 | | | | | | |
| | | CHBDC | 1 | 1445. | | 3548. | | 1598. | 0.092 | 2.5 | 0.541 | 0.542 | 0.10 | | | | | | |
| | | CHBDC | 1 | 1032. | | 3548. | | 1598. | 0.092 | 3.4 | 0.541 | 0.387 | 0.10 | | | | | | |

SEAN/ X/L COMB. ULS ULS (FACTORED) CRACKING N.A FROM |Mr/Mf| 1.2Mcr/Mr 1.33Mf/Mr c/d IKODE NOS.

| SEC | X/L | COMB. TABLE | ULS GROUP NO. | MAX/MIN APPLIED MOMENT (kN-m) | Mf | (kN-m) | RESISTANCE MOMENT (kN-m) | Mcr | (kN-m) | N.A FROM EXT. COMP FLBRE C (m) | Mr/Mf | 1.2Mcr/Mr | 1.33Mf/Mr | c/d | IKODE NOS. | | |
|-------|-------|-------------|---------------|-------------------------------|-----|--------|--------------------------|-----|--------|--------------------------------|-------|-----------|-----------|------|------------|--|--|
| 1/ 8 | 0.900 | CHBDC | 1 | 479. | | 3548. | 1598. | | 7.4 | 0.092 | 0.541 | 0.179 | 0.10 | | | | |
| | | | 1 | 345. | | 3548. | 1598. | | 10.3 | 0.092 | 0.541 | 0.129 | 0.10 | | | | |
| 1/ 8 | 0.900 | CHBDC | 1 | 153. | MIN | 3548. | 1680. | | 23.2 | 0.092 | 0.568 | 0.057 | 0.10 | | | | |
| | | | 1 | 845. | MAX | 3548. | 1680. | | 4.2 | 0.092 | 0.568 | 0.317 | 0.10 | | | | |
| | | | 1 | 516. | | 3548. | 1680. | | 6.9 | 0.092 | 0.568 | 0.193 | 0.10 | | | | |
| | | | 1 | 269. | | 3548. | 1680. | | 13.2 | 0.092 | 0.568 | 0.101 | 0.10 | | | | |
| | | | 1 | 194. | | 3548. | 1680. | | 18.3 | 0.092 | 0.568 | 0.073 | 0.10 | | | | |
| | | | 1 | -89. | MIN | -1707. | -860. | | 0.205 | 19.1 | 0.205 | 0.605 | 0.069 | 0.22 | | | |
| 1/ 9 | 1.000 | CHBDC | 1 | -39. | MAX | -1707. | -860. | | 43.4 | 0.205 | 0.605 | 0.031 | 0.22 | | | | |
| | | | 1 | -44. | | -1707. | -860. | | 39.2 | 0.205 | 0.605 | 0.034 | 0.22 | | | | |
| | | | 1 | -39. | | -1707. | -860. | | 43.4 | 0.205 | 0.605 | 0.031 | 0.22 | | | | |
| | | | 1 | -39. | | -1707. | -860. | | 43.3 | 0.205 | 0.605 | 0.031 | 0.22 | | | | |
| | | | 1 | -89. | | -1707. | -860. | | 19.1 | 0.205 | 0.605 | 0.069 | 0.22 | | | | |
| | | | 1 | -8. | MIN | -1706. | -860. | | 0.205 | *** | 0.205 | 0.605 | 0.006 | 0.22 | | | |
| RC/ 9 | 0.000 | CHBDC | 1 | 42. | MAX | 3543. | 786. | | 83.9 | 0.092 | 0.266 | 0.016 | 0.10 | | | | |
| | | | 1 | 38. | | 3543. | 786. | | 93.1 | 0.092 | 0.266 | 0.014 | 0.10 | | | | |
| | | | 1 | 42. | | 3543. | 786. | | 84.2 | 0.092 | 0.266 | 0.016 | 0.10 | | | | |
| | | | 1 | -8. | | -1706. | -860. | | *** | 0.205 | 0.605 | 0.006 | 0.22 | | | | |
| | | | 1 | -43. | MIN | -1645. | -860. | | 0.214 | 38.6 | 0.214 | 0.627 | 0.034 | 0.21 | | | |
| | | | 1 | -39. | MAX | -1645. | -860. | | 0.214 | 42.7 | 0.214 | 0.627 | 0.031 | 0.21 | | | |
| RC/ 9 | 1.000 | CHBDC | 1 | -39. | | -1645. | -860. | | 42.7 | 0.214 | 0.627 | 0.031 | 0.21 | | | | |
| | | | 1 | -43. | | -1645. | -860. | | 38.6 | 0.214 | 0.627 | 0.034 | 0.21 | | | | |
| | | | 1 | -39. | | -1645. | -860. | | 42.7 | 0.214 | 0.627 | 0.031 | 0.21 | | | | |
| | | | 1 | -43. | | -1645. | -860. | | 38.6 | 0.214 | 0.627 | 0.034 | 0.21 | | | | |
| | | | 1 | -43. | | -1645. | -860. | | 0.214 | 42.7 | 0.214 | 0.627 | 0.031 | 0.21 | | | |
| | | | 1 | -43. | | -1645. | -860. | | 0.214 | 38.6 | 0.214 | 0.627 | 0.034 | 0.21 | | | |



| SPAN/ SEC | X/L | COMB. TABLE | ULS GRP | MAX/MIN APPLIED SHEAR Vf (kN) | FACTORED SHEAR RESISTANCE Vr (kN) | STIRRUP CAPACITY Vs (kN) | CONCRETE CAPACITY Vc (kN) | PRESTRESS COMPONENT FOR SHEAR Vp (kN) | NOMINAL SHEAR STRESS (v) (kPa) | AV (mm) | 2 (mm) | MIN TOTAL SPACING REQD (mm) | MAX AREA SPACING (mm) | IKODE NOS. |
|--------------|-------|----------------|------------|---|---|-----------------------------------|------------------------------------|---|--|------------|-----------|--------------------------------------|-----------------------------|---------------|
| | | CHBDC | 1 | 150. | 742. | 404. | 338. | 0. | 787. | 258. | 70. | 600. | | |
| | | CHBDC | 1 | 108. | 742. | 404. | 338. | 0. | 567. | 258. | 70. | 600. | | |
| 1/ 5 | 0.300 | CHBDC | 1 | 80. | 742. | 404. | 338. | 0. | 421. | 258. | 70. | 600. | | |
| | | CHBDC | 1 | 197. | 742. | 404. | 338. | 0. | 1034. | 258. | 70. | 600. | | |
| | | CHBDC | 1 | -47. | -742. | 404. | 338. | 0. | 247. | 258. | N/C | N/C | | |
| | | CHBDC | 1 | 435. | 667. | 388. | 279. | 0. | 2284. | 258. | 70. | 600. | | |
| | | CHBDC | 1 | 100. | 742. | 404. | 338. | 0. | 525. | 258. | 70. | 600. | | |
| | | CHBDC | 1 | 72. | 742. | 404. | 338. | 0. | 378. | 258. | 70. | 600. | | |
| 1/ 6 | 0.400 | CHBDC | 1 | 44. | 608. | 270. | 338. | 0. | 232. | 258. | N/C | N/C | | |
| | | CHBDC | 1 | 91. | 608. | 270. | 338. | 0. | 477. | 258. | 105. | 600. | | |
| | | CHBDC | 1 | -131. | -608. | 270. | 338. | 0. | 686. | 258. | 105. | 600. | | |
| | | CHBDC | 1 | 329. | 482. | 248. | 234. | 0. | 1728. | 258. | 105. | 600. | | |
| | | CHBDC | 1 | 50. | 608. | 270. | 338. | 0. | 263. | 258. | N/C | N/C | | |
| | | CHBDC | 1 | 36. | 608. | 270. | 338. | 0. | 189. | 258. | N/C | N/C | | |
| 1/ 6 | 0.500 | CHBDC | 1 | 8. | 608. | 270. | 338. | 0. | 43. | 258. | N/C | N/C | | |
| | | CHBDC | 1 | -41. | -608. | 270. | 338. | 0. | 214. | 258. | N/C | N/C | | |
| | | CHBDC | 1 | -223. | -608. | 270. | 338. | 0. | 1170. | 258. | 105. | 600. | | |
| | | CHBDC | 1 | 223. | 524. | 257. | 268. | 0. | 1171. | 258. | 105. | 600. | | |
| | | CHBDC | 1 | 0. | 608. | 270. | 338. | 0. | 1. | 258. | N/C | N/C | | |
| | | CHBDC | 1 | 0. | 608. | 270. | 338. | 0. | 1. | 258. | N/C | N/C | | |
| 1/ 6 | 0.600 | CHBDC | 1 | -28. | -608. | 270. | 338. | 0. | 145. | 258. | N/C | N/C | | |
| | | CHBDC | 1 | -91. | -608. | 270. | 338. | 0. | 476. | 258. | 105. | 600. | | |
| | | CHBDC | 1 | -329. | -482. | 248. | 234. | 0. | 1726. | 258. | 105. | 600. | | |
| | | CHBDC | 1 | 131. | 608. | 270. | 338. | 0. | 687. | 258. | 105. | 600. | | |
| | | CHBDC | 1 | -50. | -608. | 270. | 338. | 0. | 261. | 258. | N/C | N/C | | |
| | | CHBDC | 1 | -36. | -608. | 270. | 338. | 0. | 188. | 258. | N/C | N/C | | |
| 1/ 7 | 0.700 | CHBDC | 1 | -75. | -742. | 404. | 338. | 0. | 396. | 258. | 70. | 600. | | |
| | | CHBDC | 1 | -197. | -742. | 404. | 338. | 0. | 1033. | 258. | 70. | 600. | | |
| | | CHBDC | 1 | -435. | -667. | 388. | 279. | 0. | 2283. | 258. | 70. | 600. | | |
| | | CHBDC | 1 | 47. | 742. | 404. | 338. | 0. | 248. | 258. | N/C | N/C | | |
| | | CHBDC | 1 | -100. | -742. | 404. | 338. | 0. | 523. | 258. | 70. | 600. | | |
| | | CHBDC | 1 | -72. | -742. | 404. | 338. | 0. | 377. | 258. | 70. | 600. | | |
| 1/ 7 | 0.800 | CHBDC | 1 | -111. | -742. | 404. | 338. | 0. | 585. | 258. | 70. | 600. | | |
| | | CHBDC | 1 | -313. | -742. | 404. | 338. | 0. | 1646. | 258. | 70. | 600. | | |
| | | CHBDC | 1 | -551. | -742. | 404. | 338. | 0. | 2896. | 258. | 70. | 300. | | |
| | | CHBDC | 1 | -36. | -742. | 404. | 338. | 0. | 190. | 258. | N/C | N/C | | |
| | | CHBDC | 1 | -149. | -742. | 404. | 338. | 0. | 785. | 258. | 70. | 600. | | |
| | | CHBDC | 1 | -108. | -742. | 404. | 338. | 0. | 566. | 258. | 70. | 600. | | |
| 1/ 8 | 0.900 | CHBDC | 1 | -147. | -876. | 539. | 338. | 0. | 774. | 258. | 53. | 600. | | |

| SPAN/ SEC | X/L | COMB. TABLE | ULS GRP | MAX/MIN APPLIED SHEAR VF | FACTORED SHEAR RESISTANCE Vr | STIRRUP CAPACITY Vs | CONCRETE CAPACITY Vc | PRESTRESS COMPONENT FOR SHEAR VP | NOMINAL SHEAR STRESS (v) | 2 | | MIN TOTAL SPACING REQD | MAX AREA SPACING | IKODE NOS. |
|--------------|-------|----------------|------------|-----------------------------------|---------------------------------------|---------------------------|----------------------------|---|-----------------------------------|------|------|------------------------------|---------------------|------------|
| | | | | | | | | | | (kN) | (kN) | | | |
| 1/ 9 | 1.000 | CHBDC | 1 | -441. | -876. | 539. | 338. | 0. | 2315. | 258. | 229. | 53. | 600. | 35 |
| | | CHBDC | 1 | -679. | -876. | 539. | 338. | 0. | 3565. | 258. | 229. | 53. | 300. | 35 |
| | | CHBDC | 1 | -114. | -876. | 539. | 338. | 0. | 598. | 258. | 229. | 53. | 600. | 35 |
| | | CHBDC | 1 | -199. | -876. | 539. | 338. | 0. | 1047. | 258. | 229. | 53. | 600. | 35 |
| | | CHBDC | 1 | -144. | -876. | 539. | 338. | 0. | 754. | 258. | 229. | 53. | 600. | 35 |
| | | CHBDC | 1 | -253. | -1223. | 1046. | 331. | 0. | 1357. | 398. | 178. | 41. | 600. | 35 |
| | | CHBDC | 1 | -180. | -1223. | 1046. | 331. | 0. | 964. | 398. | 178. | 41. | 600. | 35 |
| | | CHBDC | 1 | -806. | -1062. | 887. | 175. | 0. | 4325. | 398. | 178. | 41. | 300. | 35 |
| | | CHBDC | 1 | -171. | -1223. | 1046. | 331. | 0. | 920. | 398. | 178. | 41. | 600. | 35 |
| | | CHBDC | 1 | -249. | -1223. | 1046. | 331. | 0. | 1337. | 398. | 178. | 41. | 600. | 35 |
| | | CHBDC | 1 | -253. | -1223. | 1046. | 331. | 0. | 1357. | 398. | 178. | 41. | 600. | 35 |
| RC/ 9 | 0.000 | CHBDC | 1 | 303. | 1223. | 1011. | 280. | 0. | 1628. | 398. | 178. | 41. | 600. | 35 |
| | | CHBDC | 1 | 4. | 1249. | 1069. | 338. | 0. | 23. | 398. | 178. | N/C | N/C | 35 |
| | | CHBDC | 1 | 4. | 1249. | 1069. | 338. | 0. | 23. | 398. | 178. | N/C | N/C | 35 |
| | | CHBDC | 1 | 304. | 1249. | 1069. | 338. | 0. | 1595. | 398. | 178. | 41. | 600. | 35 |
| | | CHBDC | 1 | 6. | 1249. | 1069. | 338. | 0. | 32. | 398. | 178. | N/C | N/C | 35 |
| | | CHBDC | 1 | 303. | 1223. | 1011. | 280. | 0. | 1628. | 398. | 178. | 41. | 600. | 35 |
| RC/ 9 | 1.000 | CHBDC | 1 | 298. | 1223. | 1046. | 331. | 0. | 1597. | 398. | 178. | 41. | 600. | 35 |

COMPOSITE PRESTRESSED GIRDER - ULTIMATE LIMIT STATES - FLEXURE

STAGE NUMBER = 2

THE IKODE NUMBER IS GIVEN WHEN A CODE CLAUSE IS VIOLATED.

| SPAN/ SEC | X/L | COMB. TABLE GROUP | ULS NO. | MAX/MIN APPLIED MOMENT (kN-m) | MIN (kN-m) | MAX/MIN RESISTANCE MOMENT (kN-m) | (FACTORED) | CRACKING MOMENT (kN-m) | N.A FROM EXT.COMP FIBRE C | Mr/Mf | 1.2McI/Mr | 1.33Mf/Mr | c/d | IKODE NOS. |
|--|-------|----------------------|------------|--|---------------|---|------------|------------------------------|------------------------------------|-------|-----------|-----------|------|------------|
| | | | | | | | | | | | | | | |
| CODE CLAUSE 30 8.8.4.3 MIN. LONGITUDINAL R/F 31 8.8.4.5 MAX. LONGITUDINAL R/F 32 Mr/Mf < 1.0 | | | | | | | | | | | | | | |
| IC = LEFT CANTILEVER SECTION RC = RIGHT CANTILEVER SECTION Mr/Mf = ABSOLUTE VALUE OF Mr/Mf c/d = FACTOR DEFINED IN 8.8.4.5 ; A NEGATIVE VALUE OF c/d INDICATES Asc > As | | | | | | | | | | | | | | |
| IC/ 2 | 0.000 | CHBDC | 1 | MIN | -55. | -1764. | -901. | 0.250 | 32.0 | 0.613 | 0.042 | 0.042 | 0.25 | |
| | | CHBDC | 1 | MAX | -50. | -1764. | -901. | 0.250 | 35.3 | 0.613 | 0.038 | 0.038 | 0.25 | |
| | | CHBDC | 1 | | -55. | -1764. | -901. | 0.250 | 32.0 | 0.613 | 0.042 | 0.042 | 0.25 | |
| | | CHBDC | 1 | | -50. | -1764. | -901. | 0.250 | 35.3 | 0.613 | 0.038 | 0.038 | 0.25 | |
| | | CHBDC | 1 | | -50. | -1764. | -901. | 0.250 | 35.3 | 0.613 | 0.038 | 0.038 | 0.25 | |
| | | CHBDC | 1 | | -55. | -1764. | -901. | 0.250 | 32.0 | 0.613 | 0.042 | 0.042 | 0.25 | |
| IC/ 2 | 1.000 | CHBDC | 1 | MIN | -101. | -1744. | -901. | 0.248 | 17.3 | 0.620 | 0.077 | 0.077 | 0.25 | |
| | | CHBDC | 1 | MAX | -51. | -1744. | -901. | 0.248 | 34.4 | 0.620 | 0.039 | 0.039 | 0.25 | |
| | | CHBDC | 1 | | -101. | -1744. | -901. | 0.248 | 17.3 | 0.620 | 0.077 | 0.077 | 0.25 | |
| | | CHBDC | 1 | | -51. | -1744. | -901. | 0.248 | 34.4 | 0.620 | 0.039 | 0.039 | 0.25 | |
| | | CHBDC | 1 | | -51. | -1744. | -901. | 0.248 | 34.3 | 0.620 | 0.039 | 0.039 | 0.25 | |
| | | CHBDC | 1 | | -101. | -1744. | -901. | 0.248 | 17.3 | 0.620 | 0.077 | 0.077 | 0.25 | |
| 1/ 2 | 0.000 | CHBDC | 1 | MIN | -127. | -1859. | -901. | 0.226 | 14.6 | 0.582 | 0.091 | 0.091 | 0.24 | |
| | | CHBDC | 1 | MAX | -75. | -1859. | -901. | 0.226 | 24.8 | 0.582 | 0.054 | 0.054 | 0.24 | |
| | | CHBDC | 1 | | -83. | -1859. | -901. | 0.226 | 22.5 | 0.582 | 0.059 | 0.059 | 0.24 | |
| | | CHBDC | 1 | | -75. | -1859. | -901. | 0.226 | 24.8 | 0.582 | 0.054 | 0.054 | 0.24 | |
| | | CHBDC | 1 | | -75. | -1859. | -901. | 0.226 | 24.8 | 0.582 | 0.054 | 0.054 | 0.24 | |
| | | CHBDC | 1 | | -127. | -1859. | -901. | 0.226 | 14.6 | 0.582 | 0.091 | 0.091 | 0.24 | |
| 1/ 3 | 0.100 | CHBDC | 1 | MIN | 384. | 4818. | 2316. | 0.111 | 12.6 | 0.577 | 0.106 | 0.106 | 0.11 | |
| | | CHBDC | 1 | MAX | 1574. | 4818. | 2316. | 0.111 | 3.1 | 0.577 | 0.434 | 0.434 | 0.11 | |
| | | CHBDC | 1 | | 916. | 4818. | 2316. | 0.111 | 5.3 | 0.577 | 0.253 | 0.253 | 0.11 | |
| | | CHBDC | 1 | | 1574. | 4818. | 2316. | 0.111 | 3.1 | 0.577 | 0.434 | 0.434 | 0.11 | |
| | | CHBDC | 1 | | 590. | 4818. | 2316. | 0.111 | 8.2 | 0.577 | 0.163 | 0.163 | 0.11 | |

SPAN/ X/L COMB. ULS TABLE NO. MAX/MIN APPLIED MOMENT (kN-m) (kN-m) (kN-m) CRACKING N.A FROM EXT. COMP FIBRE MOMENT (kN-m) |Mr/Mf| 1.2Mcr/Mr 1.3Mf/Mr c/d IKODE NOS.

| SPAN/ SEC | X/L | COMB. TABLE NO. | ULS GROUP NO. | MAX/MIN APPLIED MOMENT (kN-m) | Mf (kN-m) | Mr (kN-m) | CRACKING N.A FROM EXT. COMP FIBRE MOMENT (kN-m) | Mr/Mf | 1.2Mcr/Mr | 1.3Mf/Mr | c/d | IKODE NOS. |
|-----------|-------|-----------------|---------------|-------------------------------|-----------|-----------|---|-------|-----------|----------|------|------------|
| | | CHBDC | 1 | 424. | 4818. | 2316. | 0.111 | 11.4 | 0.577 | 0.117 | 0.11 | |
| 1/ 4 | 0.200 | CHBDC | 1 MIN | 718. | 5091. | 2377. | 0.111 | 7.1 | 0.560 | 0.188 | 0.10 | |
| | | CHBDC | 1 MAX | 2692. | 5091. | 2377. | 0.111 | 1.9 | 0.560 | 0.703 | 0.10 | |
| | | CHBDC | 1 | 1857. | 5091. | 2377. | 0.111 | 2.7 | 0.560 | 0.485 | 0.10 | |
| | | CHBDC | 1 | 2684. | 5091. | 2377. | 0.111 | 1.9 | 0.560 | 0.701 | 0.10 | |
| | | CHBDC | 1 | 1049. | 5091. | 2377. | 0.111 | 4.9 | 0.560 | 0.274 | 0.10 | |
| | | CHBDC | 1 | 754. | 5091. | 2377. | 0.111 | 6.8 | 0.560 | 0.197 | 0.10 | |
| 1/ 4 | 0.300 | CHBDC | 1 MIN | 958. | 5363. | 2491. | 0.111 | 5.6 | 0.557 | 0.238 | 0.10 | |
| | | CHBDC | 1 MAX | 3533. | 5363. | 2491. | 0.111 | 1.5 | 0.557 | 0.876 | 0.10 | |
| | | CHBDC | 1 | 2563. | 5363. | 2491. | 0.111 | 2.1 | 0.557 | 0.636 | 0.10 | |
| | | CHBDC | 1 | 3435. | 5363. | 2491. | 0.111 | 1.6 | 0.557 | 0.852 | 0.10 | |
| | | CHBDC | 1 | 1377. | 5363. | 2491. | 0.111 | 3.9 | 0.557 | 0.342 | 0.10 | |
| | | CHBDC | 1 | 989. | 5363. | 2491. | 0.111 | 5.4 | 0.557 | 0.245 | 0.10 | |
| 1/ 5 | 0.400 | CHBDC | 1 MIN | 1104. | 5550. | 2586. | 0.111 | 5.0 | 0.559 | 0.264 | 0.10 | |
| | | CHBDC | 1 MAX | 3974. | 5550. | 2586. | 0.111 | 1.4 | 0.559 | 0.952 | 0.10 | |
| | | CHBDC | 1 | 3068. | 5550. | 2586. | 0.111 | 1.8 | 0.559 | 0.735 | 0.10 | |
| | | CHBDC | 1 | 3777. | 5550. | 2586. | 0.111 | 1.5 | 0.559 | 0.905 | 0.10 | |
| | | CHBDC | 1 | 1574. | 5550. | 2586. | 0.111 | 3.5 | 0.559 | 0.377 | 0.10 | |
| | | CHBDC | 1 | 1130. | 5550. | 2586. | 0.111 | 4.9 | 0.559 | 0.271 | 0.10 | |
| 1/ 5 | 0.500 | CHBDC | 1 MIN | 1155. | 5550. | 2560. | 0.111 | 4.8 | 0.553 | 0.277 | 0.10 | |
| | | CHBDC | 1 MAX | 4063. | 5550. | 2560. | 0.111 | 1.4 | 0.553 | 0.974 | 0.10 | |
| | | CHBDC | 1 | 3282. | 5550. | 2560. | 0.111 | 1.7 | 0.553 | 0.787 | 0.10 | |
| | | CHBDC | 1 | 3744. | 5550. | 2560. | 0.111 | 1.5 | 0.553 | 0.897 | 0.10 | |
| | | CHBDC | 1 | 1639. | 5550. | 2560. | 0.111 | 3.4 | 0.553 | 0.393 | 0.10 | |
| | | CHBDC | 1 | 1177. | 5550. | 2560. | 0.111 | 4.7 | 0.553 | 0.282 | 0.10 | |

COMPOSITE PRESTRESSED GIRDER - ULTIMATE LIMIT STATES - SHEAR

STAGE NUMBER = 2

THE IKODE NUMBER IS GIVEN WHEN A CODE CLAUSE IS VIOLATED.
 VIOLATION OF CL 8.9.3.11/12 MAY NOT BE CRITICAL IF USER ENSURES THAT CL 8.9.3.10 IS SATISFIED BY PROPER REBAR DETAILING.
 IKODE NO. N/C ---> NOT CALCULATED, STIRRUPS NOT REQUIRED AS PER CHBDC CLAUSE 8.9.1.2 FOR VE

33 8.9.3.2
 35 8.9.3.11/12
 36 8.14.6 NOTE: THE APPLICABILITY OF IKODES 36 & 37 FOR SOLID SLAB SECTIONS MUST BE ASCERTAINED BY THE USER.
 37 8.9.1.3

LC = LEFT CANTILEVER SECTION
 RC = RIGHT CANTILEVER SECTION

| SPAN/ SEC | X/L | COMB. TABLE | ULS GRP | MAX/MIN APPLIED SHEAR Vf (kN) | FACTORED SHEAR RESISTANCE Vr (kN) | STIRRUP CAPACITY Vs (kN) | CONCRETE CAPACITY Vc (kN) | PRESTRESS NOMINAL COMPONENT FOR SHEAR VP (kN) | SHEAR STRESS AV (v) | PRESTRESS NOMINAL SHEAR STRESS AV (kPa) | MIN SPACING REQD (mm) | MAX SPACING REQD (mm) | IKODE NOS. |
|--------------|-------|----------------|------------|---|---|-----------------------------------|------------------------------------|---|------------------------------|---|--------------------------------|--------------------------------|------------|
| LC/ 2 | 0.000 | CHBDC | 1 | -11. | -1208. | 1449. | 327. | 0. | 58. | 398. | 127. | N/C | N/C |
| | | CHBDC | 1 | -10. | -1208. | 1449. | 327. | 0. | 52. | 398. | 127. | N/C | N/C |
| | | CHBDC | 1 | MIN | -1208. | 1449. | 327. | 0. | 58. | 398. | 127. | N/C | N/C |
| | | CHBDC | 1 | MAX | -1208. | 1449. | 327. | 0. | 52. | 398. | 127. | N/C | N/C |
| | | CHBDC | 1 | -10. | -1208. | 1449. | 327. | 0. | 52. | 398. | 127. | N/C | N/C |
| | | CHBDC | 1 | -11. | -1208. | 1449. | 327. | 0. | 58. | 398. | 127. | N/C | N/C |
| LC/ 2 | 1.000 | CHBDC | 1 | -314. | -1206. | 1446. | 326. | 0. | 1711. | 398. | 127. | 29. | 600. |
| | | CHBDC | 1 | -14. | -1206. | 1446. | 326. | 0. | 77. | 398. | 127. | N/C | N/C |
| | | CHBDC | 1 | MIN | -1206. | 1446. | 326. | 0. | 1711. | 398. | 127. | 29. | 600. |
| | | CHBDC | 1 | MAX | -1206. | 1446. | 326. | 0. | 77. | 398. | 127. | N/C | N/C |
| | | CHBDC | 1 | -14. | -1206. | 1446. | 326. | 0. | 86. | 398. | 127. | N/C | N/C |
| | | CHBDC | 1 | -16. | -1206. | 1446. | 326. | 0. | 86. | 398. | 127. | N/C | N/C |
| | | CHBDC | 1 | -314. | -1206. | 1446. | 326. | 0. | 1711. | 398. | 127. | 29. | 600. |
| 1/ 2 | | CHBDC | 1 | 362. | 1225. | 1446. | 326. | -19. | 1867. | 398. | 127. | 29. | 600. |
| | | CHBDC | 1 | 256. | 1225. | 1446. | 326. | -19. | 1286. | 398. | 127. | 29. | 600. |
| | | CHBDC | 1 | MIN | 1225. | 1446. | 326. | -19. | 1264. | 398. | 127. | 29. | 600. |
| | | CHBDC | 1 | MAX | 1225. | 1446. | 326. | -19. | 1264. | 398. | 127. | 29. | 600. |
| | | CHBDC | 1 | 361. | 1225. | 1446. | 326. | -19. | 1867. | 398. | 127. | 29. | 600. |
| | | CHBDC | 1 | 362. | 1225. | 1446. | 326. | -19. | 1867. | 398. | 127. | 29. | 600. |
| 1/ 3 | | CHBDC | 1 | 218. | 954. | 540. | 339. | -75. | 752. | 258. | 229. | 53. | 600. |
| | | CHBDC | 1 | 625. | 954. | 540. | 339. | -75. | 2882. | 258. | 229. | 53. | 300. |
| | | CHBDC | 1 | MIN | 954. | 540. | 339. | -75. | 575. | 258. | 229. | 53. | 600. |
| | | CHBDC | 1 | MAX | 954. | 540. | 339. | -75. | 4128. | 258. | 229. | 53. | 300. |
| | | CHBDC | 1 | 300. | 954. | 540. | 339. | -75. | 1182. | 258. | 229. | 53. | 600. |
| | | CHBDC | 1 | 216. | 954. | 540. | 339. | -75. | 739. | 258. | 229. | 53. | 600. |



SPAN/ X/L COMB. ULS GRP MAX/MIN APPLIED SHEAR STRESS ULS GRP MAX ICODE NOS.

STIRRUP CAPACITY PRESTRESS NOMINAL <- STIRRUPTS-> MIN MAX TOTAL SPACING AREA SPACING

| SPAN/ SEC | X/L | COMB. TABLE | ULS GRP | MAX/MIN APPLIED SHEAR STRESS (kN) | FACTORED SHEAR RESISTANCE (kN) | STIRRUP CAPACITY (kN) | CONCRETE CAPACITY (kN) | COMPONENT SHEAR FOR SHEAR STRESS (kN) | PRESTRESS NOMINAL (kPa) | TOTAL SPACING (mm) | MIN REQD (mm) | MAX ICODE NOS. |
|-----------|-------|-------------|---------|-----------------------------------|--------------------------------|-----------------------|------------------------|---------------------------------------|-------------------------|--------------------|---------------|----------------|
| | | | | | | | | | | | | |
| 1/ 4 | 0.200 | CHBDC | 1 | 164. | 803. | 397. | 331. | -75. | 480. | 258. | 305. | 70. 600. |
| | | CHBDC | 1 | 457. | 803. | 397. | 331. | -75. | 2047. | 258. | 305. | 70. 600. |
| | | CHBDC | 1 | 397. | 803. | 397. | 331. | -75. | 44. | 258. | 305. | 70. 600. |
| | | CHBDC | 1 | 397. | 803. | 397. | 331. | -75. | 3324. | 258. | 305. | 70. 300. |
| | | CHBDC | 1 | 225. | 803. | 397. | 331. | -75. | 806. | 258. | 305. | 70. 600. |
| | | CHBDC | 1 | 162. | 803. | 397. | 331. | -75. | 466. | 258. | 305. | 70. 600. |
| 1/ 4 | 0.300 | CHBDC | 1 | 110. | 840. | 417. | 348. | -75. | 182. | 258. | 305. | 70. 600. |
| | | CHBDC | 1 | 296. | 795. | 408. | 312. | -75. | 1131. | 258. | 305. | 70. 600. |
| | | CHBDC | 1 | -21. | -691. | 417. | 348. | -75. | 486. | 258. | 305. | N/C N/C |
| | | CHBDC | 1 | 542. | 726. | 391. | 260. | -75. | 2384. | 258. | 305. | 70. 600. |
| | | CHBDC | 1 | 150. | 840. | 417. | 348. | -75. | 385. | 258. | 305. | 70. 600. |
| | | CHBDC | 1 | 108. | 840. | 417. | 348. | -75. | 169. | 258. | 305. | 70. 600. |
| 1/ 5 | 0.400 | CHBDC | 1 | 56. | 648. | 288. | 360. | 0. | 278. | 258. | 457. | N/C N/C |
| | | CHBDC | 1 | -44. | -558. | 273. | 285. | 0. | 214. | 258. | 457. | N/C N/C |
| | | CHBDC | 1 | -131. | -648. | 288. | 360. | 0. | 645. | 258. | 457. | 105. 600. |
| | | CHBDC | 1 | 390. | 500. | 261. | 238. | 0. | 1923. | 258. | 457. | 105. 600. |
| | | CHBDC | 1 | 75. | 648. | 288. | 360. | 0. | 370. | 258. | 457. | 105. 600. |
| | | CHBDC | 1 | 54. | 648. | 288. | 360. | 0. | 266. | 258. | 457. | N/C N/C |
| 1/ 5 | 0.500 | CHBDC | 1 | -3. | -648. | 288. | 360. | 0. | 13. | 258. | 457. | N/C N/C |
| | | CHBDC | 1 | 34. | 533. | 269. | 265. | 0. | 166. | 258. | 457. | N/C N/C |
| | | CHBDC | 1 | -241. | -648. | 288. | 360. | 0. | 1187. | 258. | 457. | 105. 600. |
| | | CHBDC | 1 | 241. | 560. | 274. | 286. | 0. | 1187. | 258. | 457. | 105. 600. |

Run C; Filename: 7108.cb1

STAGE NUMBER = 2

THE IKODE NUMBER IS GIVEN WHEN A CODE CLAUSE IS VIOLATED.

| IKODE NO. | CODE CLAUSE |
|-----------|-------------------------------|
| 30 | 8.8.4.3 MIN. LONGITUDINAL R/F |
| 31 | 8.8.4.5 MAX. LONGITUDINAL R/F |
| 32 | Mr/Mf < 1.0 |

LC = LEFT CANTILEVER SECTION
RC = RIGHT CANTILEVER SECTION

|Mr/Mf| = ABSOLUTE VALUE OF Mr/Mf

c/d = FACTOR DEFINED IN 8.8.4.5 ; A NEGATIVE VALUE OF c/d INDICATES Asc > As

| SPAN/ SEC | X/L | COMB. TABLE NO. | ULS GROUP | MAX/MIN APPLIED MOMENT Mf (kN-m) | (FACTORED) RESISTANCE MOMENT Mr (kN-m) | CRACKING N.A FROM EXT. COMP FIBRE MOMENT MCr (kN-m) | 1.2McR/Mr | 1.33Mf/Mr | c/d | IKODE NOS. |
|-----------|-------|-----------------|-----------|----------------------------------|--|---|-----------|-----------|-------|------------|
| LC/ 2 | 0.000 | CHBDC | 1 MIN | -55. | -1764. | -860. | 0.250 | 0.585 | 0.042 | 0.25 |
| | | | 1 MAX | -50. | -1764. | -860. | 0.250 | 0.585 | 0.038 | 0.25 |
| | | | 1 | -55. | -1764. | -860. | 0.250 | 0.585 | 0.042 | 0.25 |
| | | | 1 | -50. | -1764. | -860. | 0.250 | 0.585 | 0.038 | 0.25 |
| | | | 1 | -55. | -1764. | -860. | 0.250 | 0.585 | 0.042 | 0.25 |
| LC/ 2 | 1.000 | CHBDC | 1 MIN | -100. | -1744. | -860. | 0.248 | 0.592 | 0.077 | 0.25 |
| | | | 1 MAX | -51. | -1744. | -860. | 0.248 | 0.592 | 0.039 | 0.25 |
| | | | 1 | -100. | -1744. | -860. | 0.248 | 0.592 | 0.077 | 0.25 |
| | | | 1 | -51. | -1744. | -860. | 0.248 | 0.592 | 0.039 | 0.25 |
| | | | 1 | -100. | -1744. | -860. | 0.248 | 0.592 | 0.077 | 0.25 |
| 1/ 2 | 0.000 | CHBDC | 1 MIN | -127. | -1859. | -860. | 0.226 | 0.555 | 0.091 | 0.24 |
| | | | 1 MAX | -75. | -1859. | -860. | 0.226 | 0.555 | 0.054 | 0.24 |
| | | | 1 | -83. | -1859. | -860. | 0.226 | 0.555 | 0.059 | 0.24 |
| | | | 1 | -75. | -1859. | -860. | 0.226 | 0.555 | 0.054 | 0.24 |
| | | | 1 | -127. | -1859. | -860. | 0.226 | 0.555 | 0.091 | 0.24 |
| 1/ 3 | 0.100 | CHBDC | 1 MIN | 374. | 4802. | 2308. | 0.118 | 0.577 | 0.104 | 0.12 |
| | | | 1 MAX | 1558. | 4802. | 2308. | 0.118 | 0.577 | 0.432 | 0.12 |
| | | | 1 | 906. | 4802. | 2308. | 0.118 | 0.577 | 0.251 | 0.12 |
| | | | 1 | 1558. | 4802. | 2308. | 0.118 | 0.577 | 0.432 | 0.12 |
| | | | 1 | 575. | 4802. | 2308. | 0.118 | 0.577 | 0.159 | 0.12 |

| SPAN/ SEC | X/L | COMB. TABLE GROUP NO. | ULS | MAX/MIN APPLIED MOMENT | Mf (kN-m) | Mf (kN-m) | Mr (kN-m) | Mcr (kN-m) | CRACKING MOMENT | N.A FROM EXT. COMP FIBRE C (m) | Mr/Mf | 1.2Mcr/Mr | 1.33Mf/Mr | c/d | IKODE NOS. |
|--------------|-------|--------------------------------|-----|------------------------------|--------------|--------------|--------------|---------------|--------------------|--|-------|-----------|-----------|-----|------------|
| | | CHBDC | 1 | 414. | 4802. | 2308. | 0.118 | 11.6 | 0.577 | 0.115 | 0.12 | | | | |
| 1/ 4 | 0.200 | CHBDC | 1 | MIN | 5076. | 2377. | 0.118 | 7.3 | 0.562 | 0.183 | 0.11 | | | | |
| | | CHBDC | 1 | MAX | 5076. | 2377. | 0.118 | 1.9 | 0.562 | 0.697 | 0.11 | | | | |
| | | CHBDC | 1 | | 5076. | 2377. | 0.118 | 2.8 | 0.562 | 0.481 | 0.11 | | | | |
| | | CHBDC | 1 | | 5076. | 2377. | 0.118 | 1.9 | 0.562 | 0.695 | 0.11 | | | | |
| | | CHBDC | 1 | | 5076. | 2377. | 0.118 | 5.0 | 0.562 | 0.267 | 0.11 | | | | |
| | | CHBDC | 1 | | 5076. | 2377. | 0.118 | 6.9 | 0.562 | 0.192 | 0.11 | | | | |
| 1/ 4 | 0.300 | CHBDC | 1 | MIN | 5347. | 2496. | 0.118 | 5.7 | 0.560 | 0.232 | 0.11 | | | | |
| | | CHBDC | 1 | MAX | 5347. | 2496. | 0.118 | 1.5 | 0.560 | 0.868 | 0.11 | | | | |
| | | CHBDC | 1 | | 5347. | 2496. | 0.118 | 2.1 | 0.560 | 0.631 | 0.11 | | | | |
| | | CHBDC | 1 | | 5347. | 2496. | 0.118 | 1.6 | 0.560 | 0.844 | 0.11 | | | | |
| | | CHBDC | 1 | | 5347. | 2496. | 0.118 | 4.0 | 0.560 | 0.332 | 0.11 | | | | |
| | | CHBDC | 1 | | 5347. | 2496. | 0.118 | 5.6 | 0.560 | 0.239 | 0.11 | | | | |
| 1/ 5 | 0.400 | CHBDC | 1 | MIN | 5535. | 2594. | 0.118 | 5.2 | 0.562 | 0.258 | 0.10 | | | | |
| | | CHBDC | 1 | MAX | 5535. | 2594. | 0.118 | 1.4 | 0.562 | 0.943 | 0.10 | | | | |
| | | CHBDC | 1 | | 5535. | 2594. | 0.118 | 1.8 | 0.562 | 0.730 | 0.10 | | | | |
| | | CHBDC | 1 | | 5535. | 2594. | 0.118 | 1.5 | 0.562 | 0.896 | 0.10 | | | | |
| | | CHBDC | 1 | | 5535. | 2594. | 0.118 | 3.6 | 0.562 | 0.367 | 0.10 | | | | |
| | | CHBDC | 1 | | 5535. | 2594. | 0.118 | 5.0 | 0.562 | 0.264 | 0.10 | | | | |
| 1/ 5 | 0.500 | CHBDC | 1 | MIN | 5535. | 2569. | 0.118 | 4.9 | 0.557 | 0.270 | 0.10 | | | | |
| | | CHBDC | 1 | MAX | 5535. | 2569. | 0.118 | 1.4 | 0.557 | 0.964 | 0.10 | | | | |
| | | CHBDC | 1 | | 5535. | 2569. | 0.118 | 1.7 | 0.557 | 0.781 | 0.10 | | | | |
| | | CHBDC | 1 | | 5535. | 2569. | 0.118 | 1.5 | 0.557 | 0.888 | 0.10 | | | | |
| | | CHBDC | 1 | | 5535. | 2569. | 0.118 | 3.5 | 0.557 | 0.382 | 0.10 | | | | |
| | | CHBDC | 1 | | 5535. | 2569. | 0.118 | 4.8 | 0.557 | 0.275 | 0.10 | | | | |

COMPOSITE PRESTRESSED GIRDER - ULTIMATE LIMIT STATES - SHEAR

STAGE NUMBER = 2

THE IKODE NUMBER IS GIVEN WHEN A CODE CLAUSE IS VIOLATED.
 VIOLATION OF CL 8.9.3.1.1/12 MAY NOT BE CRITICAL IF USER ENSURES THAT CL 8.9.3.1.10 IS SATISFIED BY PROPER REBAR DETAILING.
 IKODE NO. N/C ---> NOT CALCULATED, STIRRUPS NOT REQUIRED AS PER CHBDC CLAUSE 8.9.1.2 FOR Vf

33 8.9.3.2
 35 8.9.3.1.1/12
 36 8.14.6 NOTE: THE APPLICABILITY OF IKODES 36 & 37 FOR SOLID SLAB SECTIONS MUST BE ASCERTAINED BY THE USER.
 37 8.9.1.3

LC = LEFT CANTILEVER SECTION
 RC = RIGHT CANTILEVER SECTION

| SPAN/ SEC | X/L | COMB. TABLE | ULS GRP | MAX/MIN APPLIED SHEAR Vf | FACTORED SHEAR RESISTANCE Vi | STIRRUP CAPACITY Vs | CONCRETE CAPACITY Vc | PRESTRESS NOMINAL COMPONENT FOR SHEAR Vp | SHEAR STRESS AV | MIN TOTAL SPACING REQD | MAX IKODE NOS. |
|--------------|-------|----------------|------------|-----------------------------------|---------------------------------------|---------------------------|----------------------------|---|-----------------------|------------------------------|-------------------|
| | | | | (kN) | (kN) | (kN) | (kN) | (kPa) | (mm) | (mm) | (mm) |
| LC/ 2 | 0.000 | CHBDC | 1 | -11. | -1208. | 1449. | 327. | 0. | 398. | 127. | N/C |
| | | CHBDC | 1 | -10. | -1208. | 1449. | 327. | 0. | 398. | 127. | N/C |
| | | CHBDC | 1 | MIN | -1208. | 1449. | 327. | 0. | 398. | 127. | N/C |
| | | CHBDC | 1 | MAX | -1208. | 1449. | 327. | 0. | 398. | 127. | N/C |
| | | CHBDC | 1 | -10. | -1208. | 1449. | 327. | 0. | 398. | 127. | N/C |
| | | CHBDC | 1 | -11. | -1208. | 1449. | 327. | 0. | 398. | 127. | N/C |
| LC/ 2 | 0.000 | CHBDC | 1 | -314. | -1206. | 1446. | 326. | 0. | 398. | 127. | 29. |
| | | CHBDC | 1 | -14. | -1206. | 1446. | 326. | 0. | 398. | 127. | N/C |
| | | CHBDC | 1 | MIN | -1206. | 1446. | 326. | 0. | 398. | 127. | 29. |
| | | CHBDC | 1 | MAX | -1206. | 1446. | 326. | 0. | 398. | 127. | N/C |
| | | CHBDC | 1 | -16. | -1206. | 1446. | 326. | 0. | 398. | 127. | N/C |
| | | CHBDC | 1 | -314. | -1206. | 1446. | 326. | 0. | 398. | 127. | 29. |
| 1/ 2 | 0.000 | CHBDC | 1 | 374. | 1225. | 1446. | 326. | -19. | 398. | 127. | 29. |
| | | CHBDC | 1 | 265. | 1225. | 1446. | 326. | -19. | 398. | 127. | 29. |
| | | CHBDC | 1 | MIN | 1225. | 1446. | 326. | -19. | 398. | 127. | 29. |
| | | CHBDC | 1 | MAX | 1225. | 1446. | 326. | -19. | 398. | 127. | 29. |
| | | CHBDC | 1 | 373. | 1225. | 1446. | 326. | -19. | 398. | 127. | 29. |
| | | CHBDC | 1 | 374. | 1225. | 1446. | 326. | -19. | 398. | 127. | 29. |
| 1/ 3 | 0.100 | CHBDC | 1 | 212. | 954. | 540. | 339. | -75. | 258. | 229. | 53. |
| | | CHBDC | 1 | 615. | 954. | 540. | 339. | -75. | 258. | 229. | 53. |
| | | CHBDC | 1 | MIN | 954. | 540. | 339. | -75. | 258. | 229. | 53. |
| | | CHBDC | 1 | MAX | 954. | 540. | 339. | -75. | 258. | 229. | 53. |
| | | CHBDC | 1 | 290. | 954. | 540. | 339. | -75. | 258. | 229. | 53. |
| | | CHBDC | 1 | 209. | 954. | 540. | 339. | -75. | 258. | 229. | 53. |

| SPAN/ SEC | X/L | COMB. TABLE | ULS GRP | MAX/MIN APPLIED SHEAR Vf (kN) | FACTORED SHEAR RESISTANCE Vr (kN) | STIRRUP CAPACITY Vs (kN) | CONCRETE CAPACITY Vc (kN) | PRESTRESS NOMINAL COMPONENT SHEAR FOR SHEAR STRESS Vp (kN) | PRESTRESS NOMINAL TOTAL SPACING AREA REQD AV (mm) | MIN TOTAL SPACING AREA REQD AV (mm) | MAX TOTAL SPACING AREA REQD AV (mm) |
|--------------|-------|----------------|------------|---|---|-----------------------------------|------------------------------------|--|---|---|---|
| 1/ 4 | 0.200 | CHBDC | 1 | 159. | 803. | 397. | 331. | -75. | 258. | 305. | 70. |
| | | CHBDC | 1 | 449. | 803. | 397. | 331. | -75. | 258. | 305. | 70. |
| | | CHBDC | 1 | 78. | 803. | 397. | 331. | -75. | 258. | 305. | 70. |
| | | CHBDC | 1 | 688. | 803. | 397. | 331. | -75. | 258. | 305. | 70. |
| | | CHBDC | 1 | 218. | 803. | 397. | 331. | -75. | 258. | 305. | 70. |
| | | CHBDC | 1 | 157. | 803. | 397. | 331. | -75. | 258. | 305. | 70. |
| 1/ 4 | 0.300 | CHBDC | 1 | 107. | 840. | 417. | 348. | -75. | 258. | 305. | 70. |
| | | CHBDC | 1 | 291. | 817. | 413. | 330. | -75. | 258. | 305. | 70. |
| | | CHBDC | 1 | -24. | -691. | 417. | 348. | -75. | 258. | 305. | 70. |
| | | CHBDC | 1 | 537. | 743. | 396. | 273. | -75. | 258. | 305. | 70. |
| | | CHBDC | 1 | 145. | 840. | 417. | 348. | -75. | 258. | 305. | 70. |
| | | CHBDC | 1 | 105. | 840. | 417. | 348. | -75. | 258. | 305. | 70. |
| 1/ 5 | 0.400 | CHBDC | 1 | 55. | 648. | 288. | 360. | 0. | 258. | 457. | N/C |
| | | CHBDC | 1 | -46. | -574. | 276. | 298. | 0. | 258. | 457. | N/C |
| | | CHBDC | 1 | -132. | -648. | 288. | 360. | 0. | 258. | 457. | N/C |
| | | CHBDC | 1 | 388. | 513. | 264. | 249. | 0. | 258. | 457. | 105. |
| | | CHBDC | 1 | 73. | 648. | 288. | 360. | 0. | 258. | 457. | 105. |
| | | CHBDC | 1 | 52. | 648. | 288. | 360. | 0. | 258. | 457. | N/C |
| 1/ 5 | 0.500 | CHBDC | 1 | -3. | -648. | 288. | 360. | 0. | 258. | 457. | N/C |
| | | CHBDC | 1 | 34. | 549. | 272. | 277. | 0. | 258. | 457. | N/C |
| | | CHBDC | 1 | -241. | -648. | 288. | 360. | 0. | 258. | 457. | 105. |
| | | CHBDC | 1 | 241. | 578. | 277. | 301. | 0. | 258. | 457. | 600. |

36

Existing Bridge Load Evaluation Summary

Analysis Case

| | | | | | |
|----|----------|-----------|-----------------|---|--------------|
| A) | 7108.1b1 | End Span | Interior Girder | 3 | Lanes Loaded |
|) | 7108.2b1 | End Span | Exterior Girder | " | " |
| C) | 7108.3b1 | Main Span | Interior Girder | " | " |
|) | 7108.4b1 | Main Span | Exterior Girder | " | " |
| E) | 7108.5b1 | End Span | | 2 | " |
| F) | 7108.6b1 | End Span | | " | " |
|) | 7108.7b1 | Main Span | | " | " |
| t) | 7108.8b1 | Main Span | | " | " |

Results

- 1) SG-06, Cl. 8.9.5.1 violated. Insufficient interface shear transfer near supports, from $x=0.1$ to 2.5 m. and from $x=10.0$ m to 12.4 m. (Report 76). If deck slab & girders were paired monolithically, problem may be avoided.
- 3) SG-06, Cl. 8.14.6 violated. Maximum spacing of reinforcement for shear and torsion exceeded at $x=2.5$ m and $x=10$ m. (Report 75)
spacing provided = 305 mm max. permissible = 300 consider ok.
SG-06, Cl. 8.9.5.1 violated, from $x=0.1$ to 2.5 m. and from $x=10$ m to 12.4 m. If diaphragms & girders were paired monolithically, problem may be avoided. (Report 76)
- SG-06, Cl. 8.9.3.11/12: (Report 75)
- 2) SG-06, Cl. 8.14.6 violated. Maximum spacing of reinforcement for shear and torsion exceeded at $x=3.556$ m & $x=14.224$ m. (Report 75)
see B)
- SG-06, Cl. 8.9.5.1 violated. See A & B. $x=0.-7.112$ m & $x=10.668-17.78$ m.



Deck Rehabilitation Design ($t_s = 225\text{mm}$, $t_a = 90\text{mm}$)

| Analysis | Span | Girder | Live Load |
|-------------|------|----------|----------------|
| A) 7108.9b1 | End | Interior | 3 lanes loaded |
| B) 7108.ab1 | End | Exterior | " " " |
| C) 7108.bb1 | Main | Interior | " " " |
| D) 7108.cb1 | Main | Exterior | " " " |

Results:

A) End Span, Interior Girder code violations:

- 8.14.6: maximum spacing of reinforcement for shear & torsion exceeded $0.2L_s$ & $0.8L_s$. (Report 75)
Spacing provided = 305mm Max. Permissible = 300mm \therefore okay
- 8.9.3.11/12: (Report 75)
 - Long rebar on flexural tension side insufficient; or,

$$F_{lz} = \frac{M_f}{d_v} + 0.5N_f + (V_f - 0.5V_s - V_p) \cot \theta$$

Should be 0 when $0.5V_s > V_f$

$$= \frac{42.6}{d_v} + 0.5(230) + (261 - 0.5(1046 \text{ kN}) - 0) \cot 42^\circ \quad @ x/L = 1.000 \text{ Sec. 9}$$

Note that long rebar in flexural tension does not exist. Long rebar is only provided in the top flange of girder. CANBAS doesn't consider this type of configuration. \therefore Not applicable

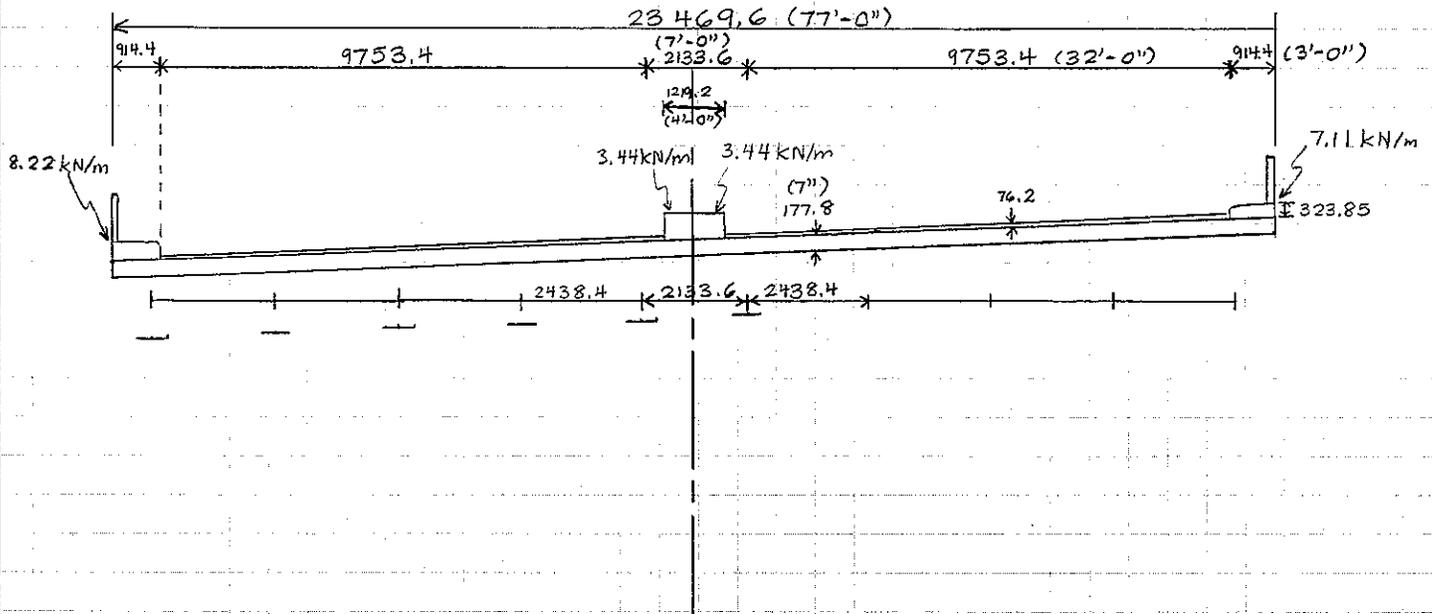
ii) Long rebar on flexural comp. side insufficient

$$F_{lc} = 0.5N_f + (V_f - 0.5V_s - V_p) \cot \theta - \frac{M_f}{d_v}$$

Why is this clause violated only at: Span 1, $x/L = 1.000$;
Span RC, $x/L = 0.000$; and,
Span RC, $x/L = 1.000$?

- 8.9.5.1: (Report 76) Insufficient interface shear transfer near supports





Left curb: $w_{cl} = 24(914.4)(374.65)/1 \times 10^6 = 8.22 \text{ kN/m}$



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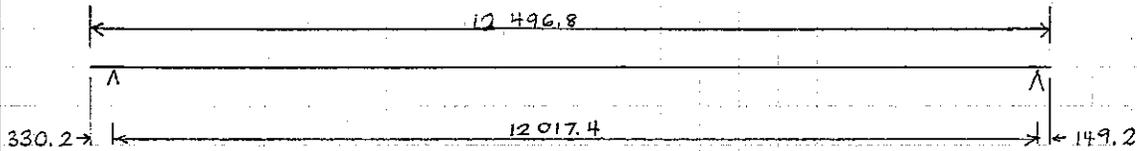
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End Span



Girder Long. Rebar:

| ID | L (mm) | Spacing | Area | CG | Cover |
|----|---------|---------|------|------|---------------|
| 1 | 12496.8 | 286 | 568 | 60.3 | 50.8 |
| 2 | 12496.8 | 286 | 568 | 162 | 50.8 (or 153) |

Girder Stirrups:

| ID | From (mm) | To (mm) | Spacing (mm) | Total Area (mm ²) |
|----|-----------|---------|--------------|-------------------------------|
| 1 | 0 | 228.6 | 177.8 | 398 |
| 2 | 228.6 | 1295.4 | 152.4 | 398 |
| 3 | 1295.4 | 2438.4 | 228.6 | 258 |
| 4 | 2438.4 | 3962.4 | 304.8 | 258 |
| 5 | 3962.4 | 8534.4 | 457.2 | 258 |
| 6 | 8534.4 | 10058.4 | 304.8 | 258 |
| 7 | 10058.4 | 11201.4 | 228.6 | 258 |
| 8 | 11201.4 | 12268.2 | 152.4 | 398 |
| 9 | 12268.2 | 12496.8 | 177.8 | 398 |

Prestressed Straight Cables:

$$CG_2 = \frac{2(304.8) + 2(558.8) + 2(762.0)}{6}$$

$$CG_2 = 541.9 \text{ mm}$$

| ID | Span# | #strands | d _c (mm) |
|----|-------|----------|---------------------|
| 1 | 1 | 12 | 101.6 |
| 2 | 1 | 6 | 541.9 |
| 3 | 1 | 2 | 1066.8 |

Slab Reinforcement

| | Span# | Spacing (mm) | Area (mm ²) | CG |
|-----|--------------|--------------|-------------------------|----|
| TOP | 0 - 12497 mm | 348 | 7(199) = 1393 | 49 |



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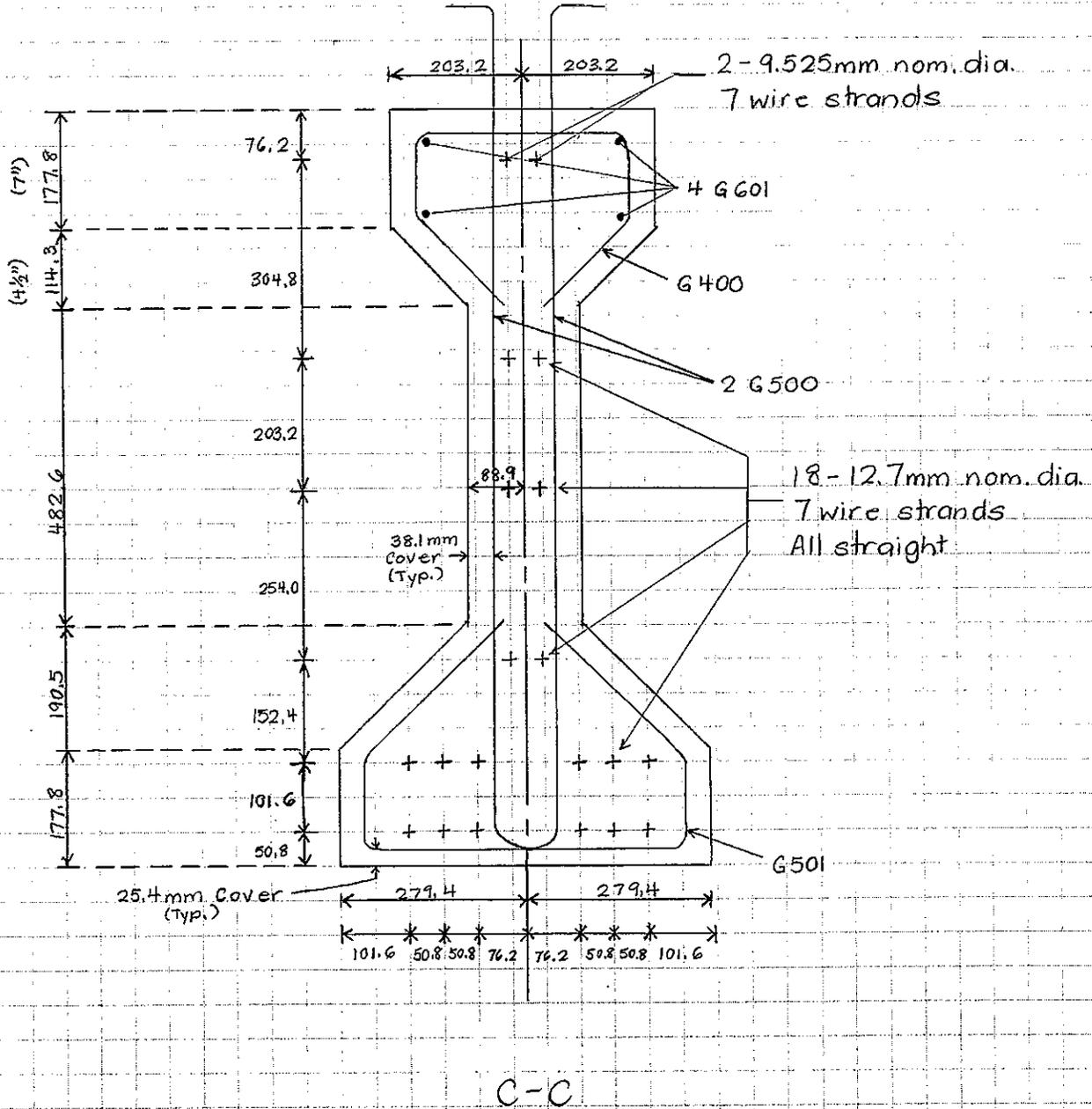
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End Span - Prestressed Girders



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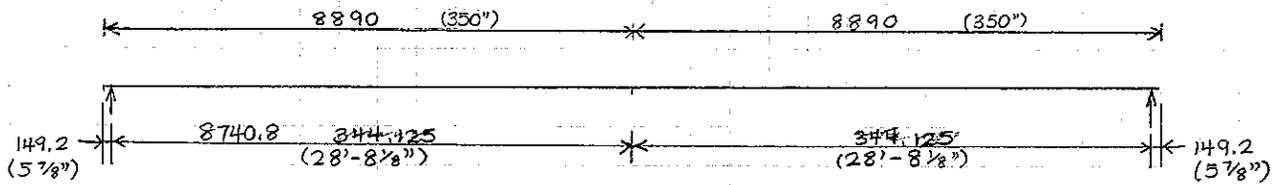
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PAGE OF

Main Span



Girder Long. Rebar:

| ID | L (mm) | Spacing (mm) | Area (mm ²) | CG (mm) | Cover |
|----|--------|--------------|-------------------------|---------|-------------|
| 1 | 17780 | 286 | 568 | 60.3 | 51 |
| 2 | 17780 | 286 | 568 | 162.0 | 51 (or 153) |

Girder Stirrups:

| ID | From (mm) | To (mm) | Spacing (mm) | Total Area (mm ²) |
|----|-----------|---------|--------------|-------------------------------|
| 1 | 0 | 1651.0 | 127.0 | 2(199mm ²) = 398 |
| 2 | 1651.0 | 3251.2 | 228.6 | 2(129mm ²) = 258 |
| 3 | 3251.2 | 5689.6 | 304.8 | 2(129mm ²) = 258 |
| 4 | 5689.6 | 8890.0 | 457.2 | 2(129mm ²) = 258 |
| 5 | 8890.0 | 12090.4 | 457.2 | = 258 |
| 6 | 12090.4 | 14528.8 | 304.8 | = 258 |
| 7 | 14528.8 | 16129.0 | 228.6 | = 258 |
| 8 | 16129.0 | 17780.0 | 127.0 | 398 |

Prestressed Straight Cables

| ID | Span # | # Strands | d _c (mm) <small>from bottom</small> | From (mm) | To (mm) |
|----|--------|-----------|--|-----------|---------|
| 1 | 1 | 16 | 101.6 | 0 | 17780 |
| 2 | 1 | 6 | 76.2 | 6604 | 11176 |
| 3 | 1 | 4 | 139.7 | 6604 | 11176 |

Prestressed Deflected Cables

| ID | Span # | # Strands | d _{c1} (mm) | d _{c2} (mm) |
|----|--------|-----------|----------------------|----------------------|
| 1 | 1 | 6 | 101.6 | 508.0 |
| 2 | 1 | 2 | 127.0 | 914.4 |
| 3 | 1 | 2 | 152.4 | 1066.8 |



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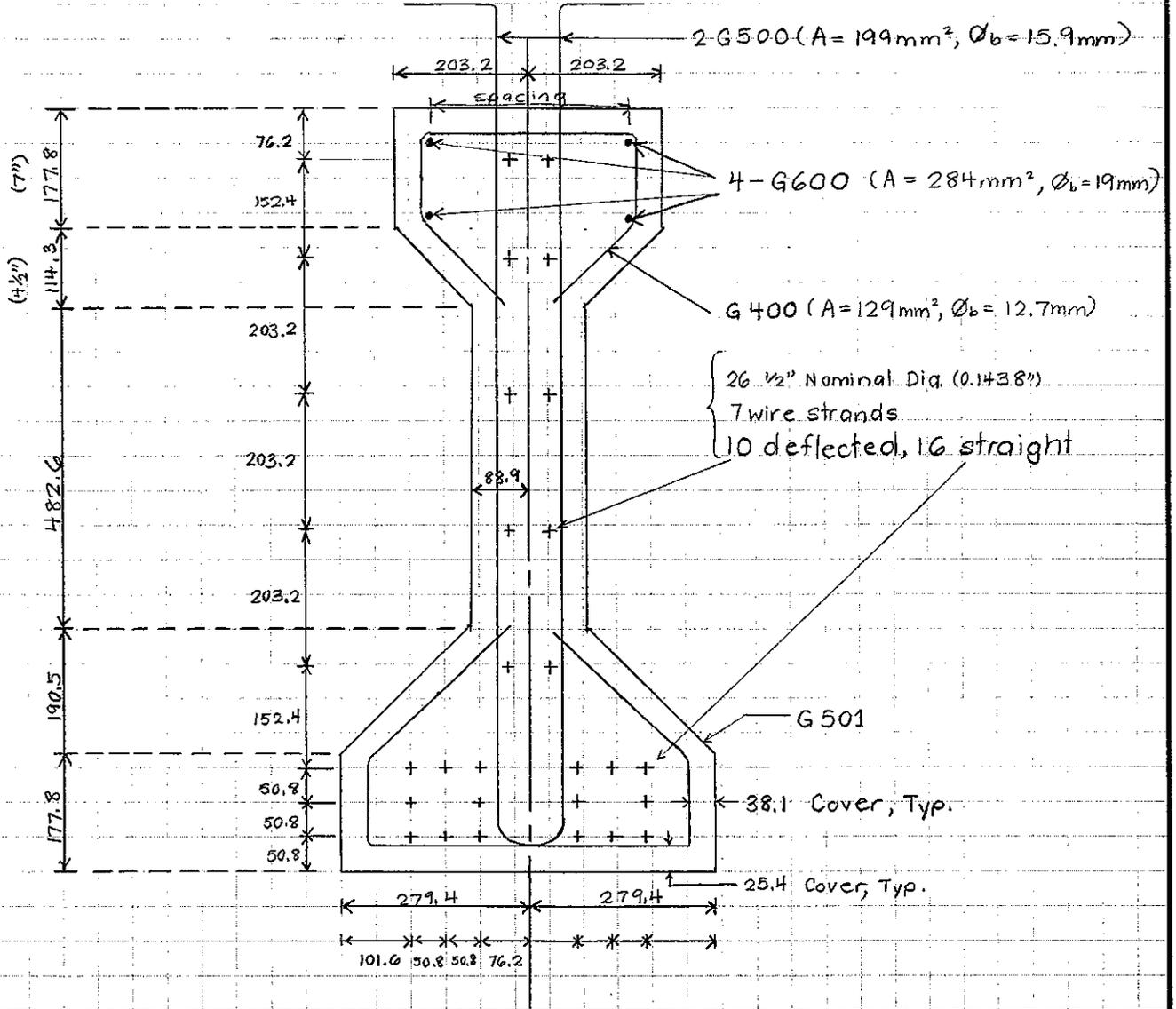
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Main Span - Prestressed Girders



A - A



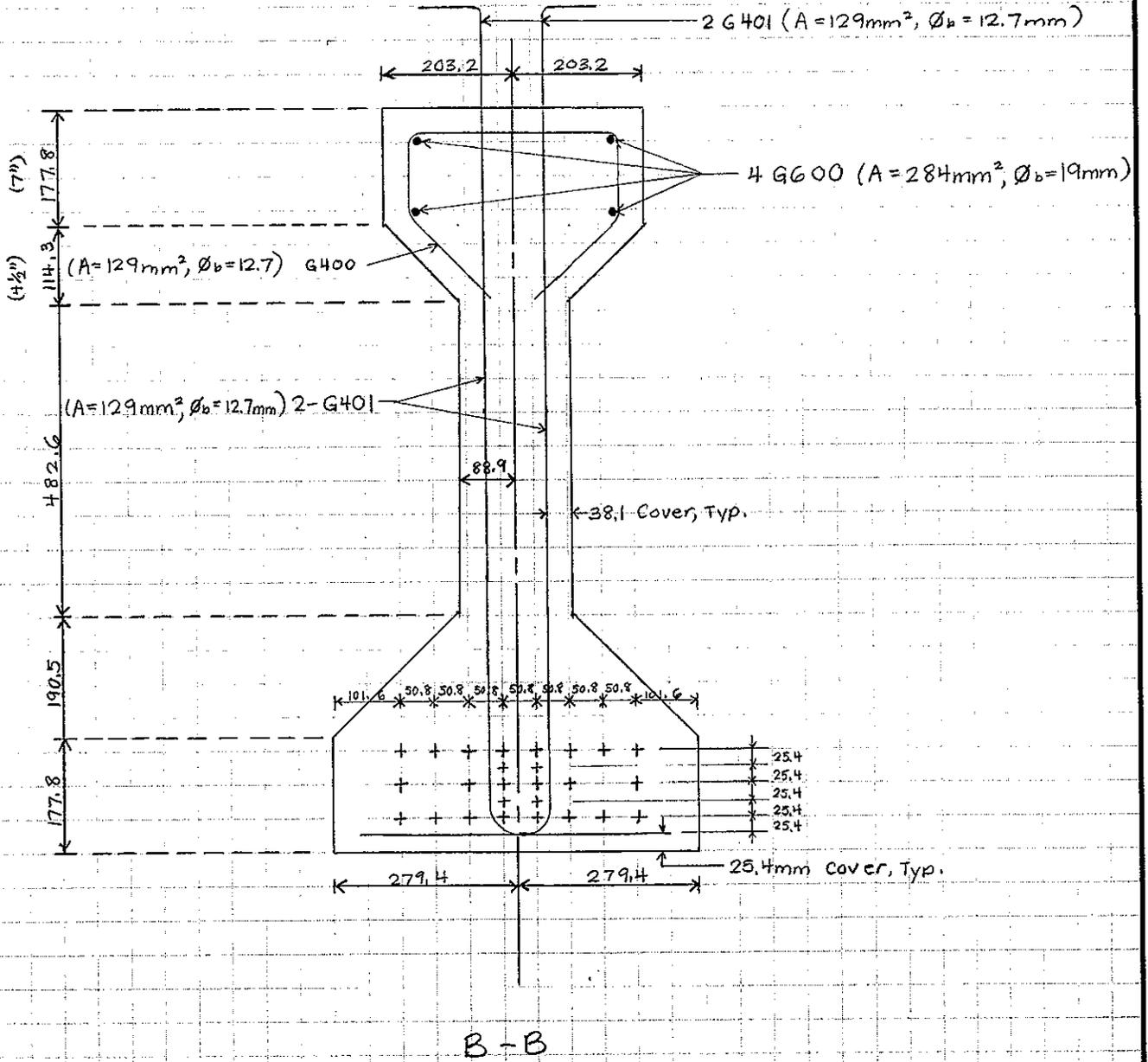
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Main Span - Prestressed Girders



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Working Force Per Girder After All Losses

- i) for main span = 2251.779 kN
- ii) for end spans = 1648.422 kN

| Concrete | f_c' | Aggregate Size (Max) |
|----------------------------|---------------------|----------------------------|
| Prestressed Beams | 5000 psi = 34.5 MPa | $\frac{3}{4}$ " = 19.05 mm |
| Deck ($t=7$ " = 177.8 mm) | 4000 psi = 27.6 MPa | 19.05 mm |
| Remainder | 3000 psi = 20.7 MPa | 19.05 mm |
| Beams @ strand release | 4000 psi = 27.6 MPa | |

Clear Cover

- Deck Slab 1" = 25.4 mm
- Diaphragms 2" = 50.8 mm

Total loss in stress in pretensioning steel:

- i) for main span = 35000 psi
- ii) for end spans = 28000 psi

Girders are A.A.S.H.T.O. Type III

Rebar: $f_y = 275$ MPa assumed { SG-06, Cl. 14.7.4.4, Table 14.2 }

Commentary Table C.8.2

- Analyze
- Generate DOL file for CANBAS
- Run CANBAS complete
- ↓
- Reports

Check effective slab widths



Effective Flange Width {S6-06, Cl. 5.8.2.1}

1) End Spans: $L = 12192 \text{ mm}$ & $b = (2438.4 \text{ mm} - 406.4 \text{ mm}) / 2 = 1016 \text{ mm}$
 $b_{OH} = 610.4 \text{ mm} - 203.2 \text{ mm} = 407.2 \text{ mm}$

$$\frac{b_e}{b} = 1 - \left[1 - \frac{L}{15b} \right]^3 \quad \text{for } \frac{L}{b} \leq 15$$
$$= 1 \quad \text{for } L/b > 15$$

$$\frac{L}{b} = \frac{12192}{1016} = 12.0 \quad b_e = 0.992b = 1007.872 \text{ mm}$$

\therefore effective width = 2422 mm for interior girders
" " = 1821 mm for exterior girders

2) Main Span: $L = 17831 \text{ mm}$ & $b = 1016 \text{ mm}$
 $b_{OH} = 407.2 \text{ mm}$

$$\frac{L}{b} = \frac{17831}{1016} = 18 \quad b_e = 1016 \text{ mm}$$

\therefore effective width = 2438.4 mm for interior girders
" " = 1829.6 mm for exterior girders



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END SPANS

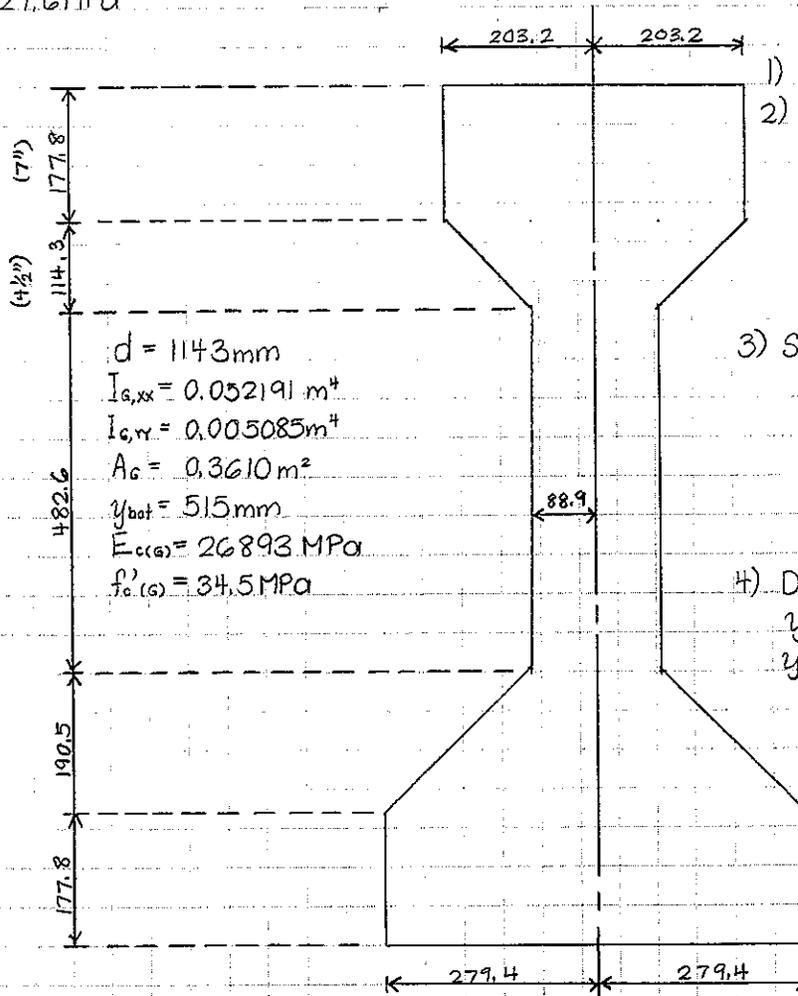
Composite In Girder Properties

Slab thickness = 177.8mm

$$E_{c(\text{slab})} = (3000\sqrt{27.6} + 6900)(2446/2200)^{1.5} = 24852 \text{ MPa}$$

$$f'_c(\text{slab}) = 27.6 \text{ MPa}$$

Interior Effective Slab Width = 2422.0mm
 Interior Trib. Slab Width = 2438.4mm
 Exterior " " " = 1829.6mm
 Exterior Effective " " = 1821.0mm



- 1) Modular Ratio, $n = 0.924$
- 2) Comp. Slab Width = $n \cdot X_{eff}$
 - = 2238mm for effective interior
 - = 2253mm " tributary interior
 - = 1690.6mm " tributary exterior
 - = 1682.6mm " effective exterior

- 3) Slab Area (1n):
 - = 397,916.4 mm² for eff. interior
 - = 400,583.4 mm² " trib. "
 - = 300,588.7 mm² " trib. exterior
 - = 299,166.3 mm² " eff. "

- 4) Distance to bot:
 - $y_{slab,b} = 1231.9 \text{ mm}$
 - $y_{g,b} = 51.5 \text{ mm}$
 - $y_{sn} = \begin{cases} 890.9 \text{ mm} \text{ for eff. interior} \\ 892.1 \text{ mm} \text{ " trib. " } \\ 840.7 \text{ mm} \text{ " trib. exterior} \\ 839.9 \text{ mm} \text{ " eff. " } \end{cases}$

- 5) $I_{xx,slab}$:
 - $I_{xx,slab} = \begin{cases} 1048.272 \times 10^6 \text{ mm}^4, \text{ eff. interior} \\ 1055.298 \times 10^6 \text{ mm}^4, \text{ trib. " } \\ 791.872 \times 10^6 \text{ mm}^4, \text{ " exterior} \\ 788.125 \times 10^6 \text{ mm}^4, \text{ eff. " } \end{cases}$

AASHTO TYPE III

$$I_{1n,xx} = \sum (I_{xx} + A y^2)$$

$$I_{sn} = \begin{cases} 52191 \times 10^6 + 1048.272 \times 10^6 + 361000(515 - 890.9)^2 + 397916.4(1231.9 - 890.9)^2 = 150519 \times 10^6 \text{ mm}^4 \\ 52191 \times 10^6 + 1055.298 \times 10^6 + 361000(515 - 890.9)^2 + 400583.4(1231.9 - 890.9)^2 = 150836 \times 10^6 \text{ mm}^4 \\ 52191 \times 10^6 + 791.872 \times 10^6 + 361000(515 - 890.9)^2 + 300588.7(1231.9 - 890.9)^2 = 138945 \times 10^6 \text{ mm}^4 \\ 52191 \times 10^6 + 788.125 \times 10^6 + 361000(515 - 890.9)^2 + 299166.3(1231.9 - 890.9)^2 = 138776 \times 10^6 \text{ mm}^4 \end{cases}$$



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KWS

DATE Sep. 2009

DATE

W.O. No. 7108.300

PAGE OF

a) Interior Girder:

$$\text{Asphalt weight} = 23.5 \text{ kN/m}^3 (8 \times 304.8 \text{ mm})(76.2 \text{ mm}) = 4.4 \text{ kN/m}$$

Curb = 0

b) Exterior Girder

$$\text{Asphalt weight} = 4.1 \text{ kN/m} = 23.5 (2286)(0.0762)$$

Curb = 8 kN/m

Diaphragms

| Weight | Location | } End Span |
|----------|----------|------------|
| 19.82 kN | 330mm | |
| 20.39 kN | 12348mm | |

Prestressing

$$\text{For main span} = 2251.8 \text{ kN} \rightarrow 87 \text{ kN / cable}$$

$$\text{" end spans} = 1648.5 \text{ kN} \rightarrow 83 \text{ kN / cable}$$



Rehabilitated Deck - Design C/D

Analysis Case

| | | | | | | |
|----|------------|-----------|-----------------|---|-------|--------|
| A) | 7108.9 b1 | End Span | Interior Girder | 3 | Lanes | Loaded |
| B) | 7108. a b1 | End Span | Exterior " | 3 | " | " |
| C) | 7108. b b1 | Main Span | Interior " | 3 | " | " |
| D) | 7108. c b1 | Main Span | Exterior " | 3 | " | " |

New Deck:

| | w_i kN/m | w_e kN/m |
|----------------------------------|---------------|---------------|
| Slab thickness, $t_s = 225$ mm | | |
| Asphalt thickness, $t_a = 90$ mm | 5.16 | 4.84 |



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PROJECT
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CNR Overpass

KWS

DATE Aug.

DATE _____

W.O. No. 7108.300

PAGE _____ OF _____

8.9.5 Interface Shear Transfer

8.9.5.1

$$v = \phi_c (c + \mu \sigma) < \min \{0.25 \phi_c f'_c, 6.5 \text{ MPa}\} \quad \text{where } \phi_c = 0.75$$

8.9.5.2.1

$\lambda_1 = 1$ (normal-density concrete)

- (a) $c = 0.25 \text{ MPa}$; $\mu = 0.60 \lambda_1$ (surface not roughened)
- (b) $c = 0.50 \text{ MPa}$; $\mu = 1.00 \lambda_1$ (" intentionally roughened)
- (c) $c = 1.00 \text{ MPa}$; $\mu = 1.40 \lambda_1$ (monolithic concrete)

8.9.5.3

$$\sigma = \rho_v f_y + \frac{N}{A_{cv}} \quad \text{where } f_y = 275 \text{ MPa}$$

A_{cv} = area of concrete resisting shear transfer
 A_{vf} = area of shear friction rebar
 v = shear resistance of shear friction plane

$$\sigma = \frac{A_{vf}}{A_{cv}} f_y + \frac{N}{A_{cv}}$$

Sub ③ into ①:

$$v = \phi_c \left[c + \mu \left(\frac{A_{vf}}{A_{cv}} f_y + \frac{N}{A_{cv}} \right) \right] \quad N = \text{unfactored permanent load normal to the interface area}$$

$$v = 0.75 \left[0.50 \text{ MPa} + \frac{A_{vf}}{A_{cv}} f_y + \frac{N}{A_{cv}} \right]$$

$$v = 0.75 \left[0.50 \text{ MPa} + \frac{A_{vf}}{A_{cv}} (275 \text{ MPa}) + \frac{N}{A_{cv}} \right]$$

$x = 1219.2 \text{ mm}$
 $\bar{x} = 1532 \text{ mm}$

@ $\frac{z}{L} = 0.10$, $g = 228.6 \text{ mm}$, $A_{vf} = 258 \text{ mm}^2$, $A_{cv} = 406.4 \text{ mm} \times s = 92903.04 \text{ mm}^2$

$z = 225 \rightarrow W_{\text{Deck slab}} = 13.165 \text{ kN/m}$

$z = 90 \rightarrow W_{\text{Asphalt}} = 5.157 \text{ kN/m}$

$\Sigma W = 18.322 \text{ kN/m}$

$$v = 0.75 \left(0.50 \text{ MPa} + 0.00277(275) \text{ MPa} + \frac{82.02 \text{ kN}}{92903.04 \text{ mm}^2} \right)$$

$$v = 0.75 (1.2637 \text{ MPa} + 0.883 \text{ MPa})$$

$$\therefore v = 1.610 \text{ kPa}$$

$$N = \Sigma W \left(\frac{1}{2} - \frac{x}{L} \right)$$

$$= \Sigma W \left(\frac{12.0174 \text{ m}}{2} - 1532 \text{ m} \right)$$

$N = 82.02 \text{ kN}$

@ $\frac{z}{L} = 0.10$, End Span, Deck Rehab. Case
 Interior Girder
 Analysis Case: 7108.9b1



Deck Rehabilitation Design (Main Span)

l = 17481.6 mm
 Interior Girder
 Analysis: 7108.bb1

Interface Shear Transfer

$$v = 0.75 \left[0.50 \text{ MPa} + \frac{A_{vf}}{A_{cv}} (275 \text{ MPa}) + \frac{N}{A_{cv}} \right]$$

@ $\frac{x}{l} = 0.10$, $s = 228.6 \text{ mm}$, $A_{vf} = 258 \text{ mm}^2$, $A_{cv} = 406.4 \text{ mm} \times s = 92903.04 \text{ mm}^2$
 $w_{\text{slab}} = 13.165 \text{ kN/m}$
 $w_{\text{asphalt}} = 5.157 \text{ kN/m}$
 $\Sigma w = 18.322 \text{ kN/m}$

$$N = \Sigma w \left(\frac{l}{2} - x \right)$$

$$= 18.322 \text{ kN/m} (8740.8 - 1748.16) \text{ mm}$$

$$N = 128.1 \text{ kN}$$

$$v = 0.75 \left[0.50 \text{ MPa} + \frac{258}{92903.04} (275 \text{ MPa}) + \frac{128.1 \text{ kN}}{92903.04} \right]$$

$$\therefore v = 1982 \text{ kPa}$$

Interface Shear Stress

$$\tau = \frac{V_f Q}{b I}$$

$$Q = (225 \text{ mm})(2438.4 \text{ mm}) \left(\frac{225 \text{ mm}}{2} + 184 \text{ mm} \right) = 1.627 \times 10^8 \text{ mm}^3$$

$$= \frac{684 \text{ kN} (1.627 \times 10^8 \text{ mm}^3)}{406.2 \text{ mm} (0.171335 \text{ m}^4)}$$

$$\tau = 1.599 \text{ MPa}$$

$$\tau = 1599 \text{ kPa}$$



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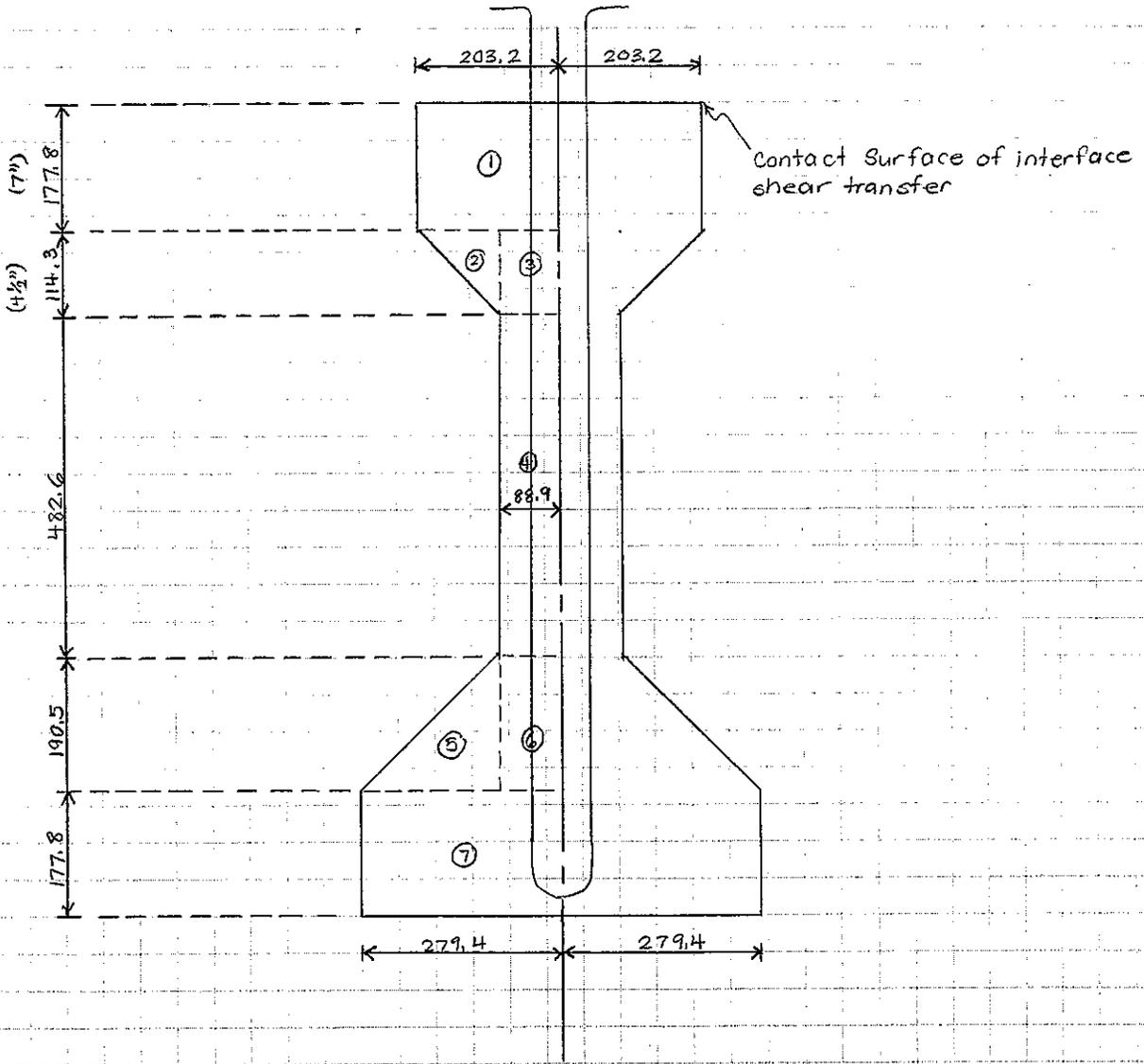
CNR Overpass

DATE

DATE

W.O. No. 7108.300

PAGE ____ OF ____



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DESIGNED KWS DATE Aug. 27/09

CHECKED _____ DATE _____

PAGE _____ OF _____

Barrier Wall

1) Barrier Exposure Index

Design Speed = 80 km/h

$$\begin{aligned} \text{AADT}_i &= \text{interpolation of 2005-2015 AADT forecast} & \text{SS height} &= 540.22 \\ &= \text{AADT}_{2005} + \frac{\text{AADT}_{2015} - \text{AADT}_{2005}}{10 \text{ yrs}} (5 \text{ yrs}) & &= 513.00 \\ &= 29620 + (44430 - 29620)(5)/10 & &= 27.22 \text{ m} \end{aligned}$$

$\text{AADT}_i = 37025$ forecasted for 2010
assuming rehabilitation completes in 2010

$$B_e = \frac{(\text{AADT}_i) K_h K_c K_g K_s}{1000} = \text{Barrier Exposure Index}$$

$K_h = 1.00$ { SG-06, Table 12.1 }
 $K_c = 1.00$ { " , Table 12.2 }
 $K_g = 1.50$ { " , Table 12.3 }
 $K_s = 2.85$

$$\therefore B_e = 158.3$$

2) Performance Level

Barrier clearance = 2589 mm { see Table 12.6, CHBDC SG-06 }
PL-2 Barriers with railings
Truck % = 4

Barrier exposure index = $B_e = 158.3$, falls within the range
8.4 to 247.3 { SG-06, Table 12.6 }, \therefore PL-2 barriers satisfy
CAN/CSA-SG-06 requirements on CNR Overhead.



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CNR Overhead

KWS

DATE Oct. 30/09

DATE

W.O. No. 7108.300

PAGE ____ OF ____

Run # 4: Main Span, Exterior Girder, 3 Lanes Loaded

Bridge Type: Deck-on-girder (Slab-on-girder), Type C

Highway Class A

1) ML: (ULS & SLS) {86-06, 01.5.7.1.2}

deck width = 11431mm

barrier width = 455mm

median " = 610mm

barrier o/n = 610mm

median o/n = 1067mm

S = girder spacing = 2438.4mm

Shallow superstructure

$L_{min} = 17831mm$

$N = 5$ girders

$n = 3$ lanes loaded

$R_L = 0.8$

$W_e = (11431 - 455 - 610) / 3 = 3425mm$

$\mu = \frac{W_e - 3.3m}{0.6} \leq 1.0$

$\mu = 0.259$

$$\left. \begin{aligned} F &= 0.70 - 4/L \\ &= 8.476m \\ C_f &= 10 - 25/L \\ &= 8.598\% \end{aligned} \right\} \begin{array}{l} 86-06 \\ \text{Table 5.3} \end{array}$$

$$M_g = F_m M_{g,avg}$$

$$F_m = \frac{SN}{F \left[1 + \frac{\mu C_f}{100} \right]} \geq 1.05$$

$$= \frac{2438.4mm (5)}{8.476m \left[1 + \frac{0.259(8.598)}{100} \right]}$$

$$F_m = 1.407$$

$$\begin{aligned} M_{g,avg} &= n M_T R_L / N \\ &= (3)(M_T)(0.8) / 5 \\ &= 0.48 M_T \end{aligned}$$



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DATE

W.O. No. 7108.300
PAGE ____ OF ____