## Proposed Milton Quarry East Extension

 JART COMMENT SUMMARY TABLE - Traffic agency objections. Additional, new comments may be provided once a response has been prepared to the comments raised below and additional information provided.

## JART Comments (August 2022) <br> Reference

Report/Date: Traffic Impact Study/ Haul Route Assessment October 2021

1. It is unclear if MTO or other jurisdictions were consulted prior to the preparation of the Traffic Study. If they were, consultation correspondence should be provided.
2. The intersection of No. 5 Sideroad at James Snow Parkway should be analyzed.
3. Future horizon/analysis should be reanalyzed with a peak hour factor of 1.00 for the Town of Milton owned Roads
4. A figure should be provided showing the net increase in the quarry trips on the road network as a result of this expansion

## Source of

 Author: The Municipality Infrastructure Group Applicant Response (December 2022)own of Milton

Haton Region, Town of Miiton, and Town of Halton Hills were consulted prior to the preparation of the Traffic Study. The subjec ands are located beyond MTO's permit contro area. TYLin will circulate MTO a copy of the raffic Impact Assessment, but does no anticipate any response or comments since it is not within their permit control area

Town of Milton As noted in the TIS, 5 Side Road is not part o the haul route and therefore it is TYLin's pinion that this intersection does not warran further assessment.

Town of Milton Noted. However, it was decided to maintain the existing peak hour factors in order to maintain a more conservative analysis.

Town of Milton
There will be no net increase in the number o quarry trips due to the extension, therefore no figure is shown
5. Has Dufferin reached out to MTO for feedback on the proposal and proposed haul routes?

The TIS was to have reviewed the issue of heavy vehicles travelling on 5 Side Road from Milton quarry to Brampton and what mitigation measures can be implemented to avoid this. The Town has confirmed that the presence of heavy vehicles are cutting through the new 5 side road, to/from Trafalgar Road. Please identify mitigation measures, i.e.. Truck Monitoring Station, to eliminate cut through heavy trucks.
7. The TIS was to have reviewed ongoing queuing issues on Dublin Line and 5 Side Road during the A.M. quarry peak time. Field review of existing conditions should be incorporated into the report to describe the real-time operations
8. The TIS was to have reviewed mitigation measures to reduce Illegal parking on 5 Side Road. Additional discussions with The Town of Halton Hills and the applicant/owner and TIS consultant is required on this to remedy any parking issues.

No, the subject lands are located beyond MTO's permit control area. TYL in will circulate MTO a copy of the Traffic Impact Assessment but does not anticipate any Assessment, but does not anticipate any response or control area.

Town of Halton

It is our understanding based on discussions with Dufferin, that this is an infrequent event and 5 Side Road permits truck traffic Furthermore, Dufferin has a close working Furthermore, Dufferin has a close working Works Department and if an issue is identified Dofferin works closely with Town Staff to resolve the issue.

Also, as mentioned in Item 13, it is suggested a traffic group be established to encourage ongoing liaison between the municipalities and Dufferin. Furthermore, Dufferin agrees to install a sign at the entrance/exit on Dublin Line instructing drivers not to use 5 Side Road except for local delivery.

This issue is further discussed by the peer reviewer in Comment \#26 and CIMA+ was satisfied that this has been addressed.

Dufferin has existing protocols in place in the event of queueing, and will arrange a meeting with the Halton Hills Director of Public Weeks discuss further and ensure the existing measures are sufficient.

Also, as mentioned in Item 13, it is suggested a traffic group be established to encourage ongoing liaison between the municipalities and Dufferin.
This issue is further discussed by the peer reviewer in Comment \#27 and CIMA+ was satisfied that this has been addressed.

Pease also see response to Items 6 and above
9. The TIS was to have evaluated existing and/or proposed haul routes for the existing and future road network (i.e., Hwy 401/Tremaine interchange). The Town would like to have a Haul Route agreement, and options provided to mitigate 5 Side Road (not limiting a Truck Monitoring Station i.e., similar to Maple Avenue).
10. Halton Hills is concerned with operational issues (i.e., dirt tracked on Dublin Line). Add the condition for sweeping and cleaning frequency into the ARA site plan/agreement.
11. Update the TIS pertaining to the Dublin Line access pertaining to operational review (i.e., collisions, sightlines). Provide a figure with an aerial, confirming sightlines are met.
12. The proponent shall consult with Halton's Transportation Planning prior to preparing the revised version of the TIS in order to confirm methodologies and assumptions for existing traffic data use and future volume forecasts in the study area

## CIMA Original Recommendation

13. The following comment was made on the Impact of Haul Route on Multiple Municipalities about the impacts to the road network should be coordinated between the municipalities, due to the haul route crossing municipal boundaries.

## This has not been addressed

No mention in the report about how coordination between the various stakeholders will occur.

Town of Halton Hills

## Town of Halton

 HillsFuture haul routes were discussed in Section 5.3 of the TIS.

Regarding a haul route agreement, the situation at 5 Side Road is quite different than the situation at Maple Avenue. Furthermore it is noted that 5 Side Road is a truck route and is noted that 5 Side Road is a truck route and is already used by non-site related trucks due o the proximity of the Milton 401 Industria Items 6 and 7 above.

Dufferin currently, and will continue to, operate with a Sweeping Plan in place. Additionally, monitoring of operations and establishment o the liaison team will assist with resolving these issues.

This is not appropriate for inclusion on an ARA site plan as it deals with lands outside of the icence boundary.
This was addressed in TYLin's Safety letter and Sightline Memo dated March, 2022 and July 2022 respectively (Attachments \#1 \& 2).

Halton Region was consulted during the pre consultation / Terms of Reference stage where methodologies and assumptions for existing traffic data use and future volume forecasts in the study area were agreed upon

CIMA+
o address this comment, Dufferin commits to adding the following requirement to the ARA site plans for the proposed extension:
"The Licencee shall invite the Region of Halton the Town of Halton Hills, and Town of Milton to an annual meeting to discuss and address any truck traffic concerns including, but not limited to, the use of 5 Side Road, off-site queuing, and street sweeping on Dublin Line."
14. The following comment was made on the Study Area Intersections about how it should include No. 5 Sideroad at James Snow Parkway (signalized) intersection and the stopcontrolled quarry site access on Dublin Line, and provide clarification for the current and future use of the existing quarry site access on Sixth Line Nassagaweya located approximately 2.85 km east of 15 Side Road.

## This has been partially addressed:

Section 2.2-Study Intersections discussed reason for the omission of No. 5 Sideroad at James Snow Parkway (signalized) intersection

## This has been addressed:

Section 5.3 discussed future haul route option 1 and 2. Neither option used Sixth Line Nassagaweya access

- Pre-consultation response \#7 states that the Sixth Line Nassagaweya quarry access is currently being utilized by staff to enter and exit the premises. The access is projected to remain exclusive to staff use under future conditions, with staff trips not projected to change. Accordingly, operations at the existing staff access were not reviewed as no changes are projected to the traffic volume or distribution/assignment as part of the proposed quarry extension.

15. The following comments were made on the future roadway network on how Section 2 should include a map showing the future roadway network and modified haul route along the Tremaine Road realignment and new Highway 401 interchange as part of the ToR. Study scope includes future Highway 401 ramp terminals on new Tremaine Road. As these ramp terminals are MTO jurisdiction, the Town of Milton should ensure that the study is circulated to the MTO for their review.

## This has been addressed:

Figure 5-1 illustrates both future haul route options. It includes the modified haul route along the Tremaine Road realignment and new Highway 401 interchange. Report does not mention circulating the report to the MTO for review.
16. The following comments were made on Future Conditions on how it should include a comparative analysis of the existing and future haul routes, analyze and compare future traffic operations for both the existing haul route and modified haul route to determine the impacts to traffic operations of modifying the haul route vs. maintaining the existing haul route, and provide justification and demonstrate that the proposed modified haul route is easible from a traffic operations perspective

## This has not been addressed:

- Report does not conduct a comparative analysis of the existing and future haul routes. The existing haul was examined under 2021 existing conditions.
- In Section 5.3 Future Haul Route Option 1 is the preferred option, as it does no encroach on the Niagara Escarpment Natural Area among other issues such as reduced distances and noise pollution; therefore, it was the only studied haul route in the future scenarios.


## This has been addressed:

Future haul route option 1 is expected to operate well under 2026 future total conditions. Section 8.2 summaries intersection operational results.

As noted in the TIS and in the responses to Items 2 and 6 above, 5 Side Road is not part o the haul route and therefore it is TYL in's opinion that this intersection does not warrant further assessment.

TYLin has reviewed traffic operations analysis of the scenario in which the existing haul route is maintained under future conditions, as par of a comparative future analysis. The results o the analysis are presented in Tables 1 and 2 (Attachments \#3 and \#4), compared to operations using the future haul route; Arcady was used for roundabout analysis, and Synchro was used for all other intersections Synchro and Arcady reports outputs are included in Attachment \#5.

Under both existing and future haul routes, all study area intersections are operating well within capacity and acceptable delays during he AM peak hour as shown in Table (Attachment \#3). Overall, intersections are operating with LOS D or better. Critical movements included the eastbound through movement at Regional Road 25 / Highway 40 Eastbound Off-Ramp with a LOS E. While this

17. The following comments were made on Trip Distribution and Assignment on how it should indicate what are the intended trip distribution assumptions (e.g. truck routes data collected from Dufferin Aggregate - Milton Quarry)

## This has been partially addressed:

No trip distribution assumptions were made.
Section 3 states that TMIG utilized historical haulage data provided by the project team from 2020 as well as existing truck assignment along the haulage route
Section 5.4 discusses the use of the MRC study for directional distribution at the future Tremaine interchange.
18. The following comments were made on Study Parameters:

- Discusses a review of the projected queues at the turning movements impacted by the truck routes;
- Include existing and projected queue lengths (per Region's TIS Guidelines, Section 3.6.1) at all study area intersections as well as mitigation measures for queues that are expected to exceed available storage. The use of SimTraffic is recommended for the queuing analysis.


## his has not been addressed:

- No review of the projected queues at the turning movements impacted by the truck routes (due to some study area intersection queue analysis not done)
- Section 6.1 indicates that the trip assignment to JSP @ RR25 and RR25 @ HWY 401 are negligible; therefore no assessment was done.


## This has been partially addressed:

- Study area intersections including RR25 @ JSP, RR25 @ HWY 401 WB offramp and RR25 @ HWY 401 EB off-ramps were not assessed.
- Arcady is used for assessing the roundabout at Dublin Line / Tremaine Roadat James Snow Parkway / Campbellville Road and the longest reported $95^{\text {th }}$ percentile queue is 36 m
- SimTraffic was used for assessing the queues at Tremaine Road at Highway 401 Eastbound and Westbound Off-Ramps. The $95^{\text {th }}$ percentile queues are all less than available storage
continues to support the future proposed haul route, however, as the diversion of trucks to the remaine Road interchange will lessen the remaine Road interchange will lessen the and also reduce the distance travelled on and also reduce the distance travelled on consumption and travel times for drivers.

No trip assumptions were made because of the use of historical haulage data to provide actual assignment. Explanation of the future hau oute assumptions (from the MRC study) wa provided in Section 5.4 of the TIS dated October 2021.

SimTraffic Queuing report outputs have been included in Attachment \#5

Under the existing haul route, all movements operate with acceptable 95th percentile queues during the AM and PM peak hours as shown in Table 3 (Attachment \#6), with the exception of the northbound left movement a Regional Road 25 / James Snow Parkway. Although the 95th percentile queue length fo his movement exceeds the available storage by 34 metres, this is not anticipated to occu regularly and the majority of the queue will be accommodated within the effective taper Notably, the 50 th percentile queue is only expected to exceed the available storage by ess than one car length, and is expected to be accommodated within the effective taper Additionally, the 95th percentile queue for the westbound right movement at the same intersection is expected to exceed the available storage by 11 metres, but can be accommodated in the effective lane taper.

Under the future haul route, the 95th percentile queue for the northbound left movement a Regional Road 25 / James Snow Parkway is expected to continue to exceed the available storage but significantly less than compared to storage but significantly less than compared to Table 3 (Attachment \#6). This is likely due to the reassignment of site traffic to the Tremaine Road intersection. The 50th percentile queue or the westbound right movement is expected exceed the available storage (by 14 metres)

The eastbound left movement at the Regiona Road 25 / Highway 401 Eastbound Offramp Road 25 / Highway 401 Eastbound Off-ramp exceeds in the AM peak hour for both the isting and future haul routes. Hower, thi expected to be resolved with the extension is expected to be resolved with the extension repes Highway 401 improvements, proposed Highway 401 improvent 30 to 470 metres and resulting in no queuin or this mond in the future

The above noted 95th percentile queue projected at the roundabout as shown in Table 4 (Attachment \#7) do not encroach onto any adjacent intersection. Accordingly, TYLin does not foresee any queuing concerns at the oundabout and expects queues to be lowe during a typical day when the quarry trip eneration is reduced compared to thi onservative site trip forecast scenario.

Overall, it is projected neither the existing nor he future haul route are expected to result in eignificant hath route are expected to result in ny of the govercentile queueing issues a any with thevements affected by either hau
 queue at Regional Road 25 James Snow Parkway. However, the future haul route pacts to this movement are less significan than those resulting from employing the xisting haul route under conditions. This provides further justification for the use of the future Option 1 haul route over the existing hau route

This was addressed in TYLin's Safety lette and Sightline Memo dated March, 2022, and July 2022 respectively (Attachments \#1 \& \#2)
20. The following comments were made on the Region's Aggregate Resource Reference Manual:

- Section 4.0 which identifies the purpose and objectives of each study
- Section C identifies all policies in any Provincial, Regional or local planning document that deal with the subject matter of the report
- Appendix A (specifically Section 8.0) - include and address the requirements identified by the most current versions of the PPS, Greenbelt Plan and Niagara Escarpment Plan
- Consideration should be given to traffic safety components including (but not limited to) heavy truck maneuverability at the Dublin Road and James Snow Parkway roundabout and the impacts of increased truck volumes on both the existing and modified haul routes.


## This has been addressed:

- Section 1.2 outlines the study objectives
- Section 1.1 outlines all the policy documents that apply to the TIS.
- The preferred route option avoids the Niagara Escarpment Area; however, Section 1.1 indicates that an amendment to the Niagara Escarpment Plan and a Niagara Escarpment Development permit is needed


## This has not been addressed:

No traffic safety components, such as those listed, were included in the report.

As there are no increase in truck volumes As ditional truck satety components were no additional truck safety components were no considered. It is noted that the existing quarry has been in operation since 1962 and has utilized this haul route with no documented traight road, with good visibility and no blind pots.

Regarding the Dublin Line roundabout and the remainder of the haul route, which are majo remainder of the haul route, which are major tuture Tremaine Road) it is assumed that this frastructure was designed by the Region to rastr accommodate heavy trucks based on xisting truck trips tolfrom the subiect land and background truck traftic subina land and background truck traffic originating and destined to the Mron 401 Industrial Business Park.

## Pre-Consultation Inquiries

21. The following comments were made on Operational Review about the Dublin Line and Main Access - operational review (i.e., collisions, sightlines).

## This has not been addressed:

Response (shown below) was a review based on solely aerial and street imagery. Not site visit was conducted to confirm sightlines.
A collision analysis or influence of heavy truck traffic on safety was not mentioned in the report.
Response: Dublin Line is a relatively flat and straight roadway, with a posted speed limit of $60 \mathrm{~km} / \mathrm{h}$. Based on the Transportation Association of Canada (TAC) Geometric Design Standards (2017), a stopping sight distance requirement of 130 m is applicable to a design speed of $80 \mathrm{~km} / \mathrm{h}$ (assuming $20 \mathrm{~km} / \mathrm{h}$ over the posted speed
CRH Canada Group Inc. Traffic Impact Study/ Haul Route Assessment Dufferin Aggregates Milton Quarry East Extension TMIG PROJECT NUMBER 10108 limit). Based on the vertical and horizontal curvature of the roadway (as reviewed based on aerial on

## street imagery), it is TMIG's opinion that the stopping sight distance requirement is met at

 the existing quarry access intersection.22. The following comments were made on Trip Distribution:

Trip distribution is to be based on anticipated truck routes to/from the site, with detailed justification provided.

## This has been partially addressed:

Trip distribution is based on the future planned truck route (Option 1). Justification for Option 1 is for short travel distances, preventing encroachment on Niagara Escarpment Plan. More detailed justification should be provided in Section 5.3.
23. The following comments were made on Electronic Synchro Analysis Submission to please provide the synchro analysis electronically as part of the submission.
24. The following comments were made on Processing Site to identify local aggregate processing sites (i.e., Armstrong Avenue, Georgetown plant).

## (Not addressed)

25. The following comments were made on Education for Truck Routes to identify the measures implemented by the Milton Quarry to educate truck drivers with regard to truck route.

## Not addressed)

26. The following comments were made on heavy traffic:

Review of the issue of heavy vehicles travelling on 5 Side Road from Milton quarry to Brampton and what mitigation measures can be implemented to avoid this

## This has been addressed

Under existing conditions, 5 Sideroad terminates in a cul-de-sac east of Dublin Line and no longer intersects with Dublin Line / Campbellville Road. Accordingly, traffic to/from the quarry no longer has direct access to 5 Sideroad via Dublin Line. (Confirmed in Google Street view that there is no longer access to 5 Sideroad.
27. The following comments were made on queuing issues:

Review of ongoing queuing issues on Dublin Line and 5 Sideroad during the AM quarry peak time

## This has been addressed

Since implementation of the roundabout, Dublin Line no longer has a direct connection to 5 Sideroad and any concerns regarding queuing on 5 Sideroad would no longer apply. Furthermore, queues projected at the Dublin Line intersection to James Snow Parkway during the 2026 future conditions are projected to be acceptable and would not encroach onto any adjacent intersection.

CIMA+ It is TYLin's opinion that no further justification It is TYLin's opinion that no further justification needed. Sufficient justification has been provided in Section 5.3 regarding the future planned truck route. Regarding trip distribution, sufficient justification has been provided since it is based on actual trip distribution data from the existing quarry operation.

## Noted: Synchro files have been attached as a zip file.

This was deemed outside the scope of work in the Terms of Reference. Furthermore, trip distribution has been provided for this operation based on actual conditions and the appropriate haul route analysis has been completed

This was deemed outside the scope of work in the Terms of Reference. However, Dufferin will provide updated signage on-site to remind drivers of the haul route and to encourage drivers to use James Snow Parkway and Tremaine Road.

## Noted.

## This has been addressed:

Trucks no longer travel along 5 Sideroad and would no longer park along the roadway Based on input from the project team, TMIG understands that illegal parking did occur along 5 Sideroad on few instances throughout the year. It should be noted that queuing along the boundary roadway has significantly reduced since the opening of the roundabout and the transition of the truck route to James Snow Parkway.
29. The following comment was made on operational issues:

Dirt tracked on Dublin Line.

## This has been addressed:

Based on input from the project team, TMIG understands that Dublin Line is being swept as required to remove any dirt from the pavement. As the cleanliness of the roadway remains an issue, TMIG recommends that Dufferin Aggregates continue to organize street sweeps on an "as-needed" basis in order to keep the roadway clean, with sweeping frequency as often as daily should it be required to keep the roadway clear. 30. The following comment was made on safety review:

Safety review at the Dublin Line roundabout to James Snow Parkway and overall haul route.

## This has been addressed

The existing roundabout at Dublin Line and James Snow Parkway, as well as the roadway included within the existing and planned haul routes, have been designed and approved by Halton Region and its consultants to accommodate heavy truck movement long the roadway segments and intersections. For this reason, it is TMIG's understanding that no safety issues related to heavy truck movement would occur from a design standpoint.
31. The following comments were made on the use of existing access

## This has been addressed

As confirmed with the project team, the Sixth Line Nassagaweya quarry access is currently being utilized by staff to enter and exit the premises. The access is projected to emain exclusive to staff use under future conditions, with staff trips not projected to hange. Accordingly, operations at the existing staff access were not reviewed as no changes are projected to the traffic volume or distribution/assignment as part of the proposed quarry extension.
32. The following comment was made on impacts to natural area on the Impacts on the Niagara Escarpment Natural Area.

## This has been addressed

The preferred haul route reviewed as part of the study does not encroach onto the Niagara Escarpment Natural Area, whereas haul route Option 2 partially would Accordingly, the choice of Option 1 as the preferred alternative is further solidified.
33. The following comments were made on reports:

Note that traffic count data and Synchro analysis reports shall be appended to the TIS document.

## This has been addressed:

Reports in Appendix C.
34. The following comments were made on truck routes:

Review and identify truck route(s) to/from the Milton Quarry.

## This has been addressed

Figures 2-1 and 5-1.
35. The following comments were made on study periods:

Assess traffic operations under the weekday AM and PM peak hours of the roadway to quantify the impacts of the expansion on the boundary road network

## This has been addressed

36. The following comments were made on study intersection:

- Dublin Line at James Snow Parkway (roundabout);
- Regional Road 25 at James Snow Parkway (signalized)
- Regional Road 25 at Highway 401 WB Off-Ramp (signalized); and
- Regional Road 25 at Highway 401 EB Off-Ramp (signalized)
- New south leg (New Tremaine Road) at Dublin Line and James Snow Parkway (roundabout); and
- •The new intersections of New Tremaine Road at the Highway 401 WB OffRamp \& EB Off-Ramp (signalized).


## This has been addressed

37. The following comments were made on traffic data

AADT is proposed to be used to derive annual historical growth rates along the study roadways to be applied to the historical traffic volumes in order to derive 2021 existing traffic volumes.
For the interchange intersections at Regional Road 25, TMIG proposes to acquire various historical TMC surveys to derive an average annual growth for the ramps should AADT not be available. Should historical TMC data sets not be available, TMIG proposes to apply the AADT derived for Regional Road 25 to the Highway 401 ramps as applicable.

## This has been addressed

Due to the pandemic historical traffic data used as a baseline within this study is based on surveys completed within the study area (either commissioned by TMIG in the past or provided by Halton Region).
TMIG derived 2021 existing traffic volumes based on historical traffic data and adequate growth rates.
38. The following comments were made on Conservative Baseline Traffic Volumes:

- remove the surveyed haulage volumes (based on the historical traffic data) from the derived 2021 volumes and replace them with conservative haulage volumes derived based on the operations of the quarry as detailed below.
- derive trip generation rates for the development based on standard 'first principles' approach (applying a Passenger Car Equivalent (PCE)) and the existing Quarry operations.
- Section 3.1 outlines the removal of the surveyed haulage volume followed by section 3.2 a conservative quarry trip generation.
- Trip generation rates are based on daily highest haulage recorded in 2020 , which represents the highest haulage day of the year

39. The following comments were made on future conditions: 5 -year study horizon to 2026 to assess the impact of the proposed expansion.

This has been addressed
40. The following comments were made on Traffic Data Model Alternative:

Using a previous TIS report within the study area. Use Emery Milton Business Park TIS
41. The following comments were made on Trip Distribution and Assignment: The Trip Distribution and assignment for the haulage volume substitution and rerouting to the modified route under future conditions will be based on input from the project

## eam.

## This has been addressed

42. The following comments were made on Study Parameters

Assess the following conditions:

- 2021 Conservative Existing Conditions
- 2026 Future Conditions

Using Synchro 10 and review of projected queues at turning movements impacted by the truck routes.

## This has been addressed

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| CIMA+ | Noted. |  |

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CIMA+
Noted.

Noted.

CIMA+
Noted.

## TOR Comments

43. The following comments were made on Traffic Data Model Alternative about using a

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\text { Attachment } 1
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## PROJECT NUMBER 10108

March 22, 2022

Kevin Mitchell, Director of Property, Planning \& Approvals
CRH Canada Group Inc.
2300 Steeles Avenue West, 4th Floor
Concord, ON
L4K 5X6

Dear Mr. Mitchell,

## Re: Proposed Dufferin Aggregates Milton Quarry East Extension - Safety Analysis Letter

The Municipal Infrastructure Group Ltd. (TMIG), a T.Y. Lin International Company, was retained by Dufferin Aggregates (a division of CRH Canada Group Inc.) to prepare a Traffic Impact Study (TIS) and Haul Route Assessment in support of the proposed Milton Quarry East Extension, in the Town of Milton. The TIS report was prepared in October 2021. Subsequent to the study submission, Halton Region staff provided comments to the project team identifying that the Safety Analysis component of the study (required as per the 2015 Halton Region TIS guidelines) was incomplete. Accordingly, this letter was prepared as an additional component to the development application in order to address the Region's request for a safety analysis.

Dufferin Aggregates is proposing to extend the quarry over a total area of 30.2 hectare, of which 15.9 hectares is proposed for extraction. This extension refers only to the extraction area, as the production capacity and access to the subject lands are proposed to remain as under existing conditions. As per the TIS findings, the preferred haul route to/from the quarry would remain as under existing conditions with a direct access via Dublin Line. The only potential changes to the haul route under future conditions would be for vehicles travelling via Highway 401 as multiple vehicles may utilize the planned Tremaine Road interchange (i.e., no longer use the Regional Road 25 interchange) based on its proximity to the site.
As per the Region's request, TMIG completed a safety analysis for the proposed extension based on the 2015 Halton Region TIS guidelines. Each component required for review as part of the guidelines has been detailed below, along with the associated analysis findings in relations to the future haul route.

Please refer to Figure 1 for an illustration of the future haul route assessed as part of this safety analysis.

Figure 1 Preferred Future Haul Route


Source: Google Earth

## Weaving \& Merging

Since the quarry opened in 1962, access has been located onto Dublin Line, which is classified as a local road with a rural two-lane cross-section. Dublin Line does not provide access to non-local traffic as it terminates in a cul-de-sac approximately 2.1 km north of Campbellville Road, with one farm and two golf courses located north of the quarry, and two farms and fifteen residential dwellings south of the quarry, along the roadway. Accordingly, non-quarry related traffic along Dublin Line is minor in magnitude and is not projected to increase. Moreover, traffic generated by the quarry is not projected to change.

Based on the nominal volume of non-quarry related traffic crossing the quarry access, the access is expected to operate with an acceptable level of service allowing for ample gaps for vehicles attempting to enter Dublin Line. As a result, there are no concerns for trucks merging to/from the access and the roadway, with no need to weave along Dublin Line per its two-lane cross-section. Furthermore, along the haulage route, the majority of trucks will travel north-south through the roundabout to access Tremaine Road and the Highway 401 interchange, while select vehicles will travel onto James Snow Parkway and Campbellville Road as illustrated in Figure 1.
Outside of the site access intersection to Dublin Line, all traffic generated by the quarry will utilize the Town and Region roads, which have been designed and signed to accommodate the truck routes utilized by the development. Accordingly, as the study area roadways have been designed per the Town and Region standards (including intersection spacing, lane widths, curb radius, all standards to accommodate weaving and merging along the roadway), it is TMIG's opinion that there should be no concerns.

## Transit operational conflicts

The previous Milton Transit Route 1, which travelled along Regional Road 25, James Snow Parkway and 5 Sideroad, has been put out of service and transit accessibility to the study area is now provided on an on-demand basis. Accordingly, there would be no transit operational conflicts within the study area.
Assuming the Milton Transit Route 1 is brought back into service following the on-going Covid-19 pandemic, it is TMIG's opinion that the proposed Dufferin Quarry East Extension would not generate any transit operational conflicts along the haul route based on the following:

- Under future conditions, multiple trucks will utilize the new Highway 401 interchange to Tremaine Road, thus reducing the magnitude of trucks sharing the road with transit services compared to previous conditions and reducing the possibility of transit operational conflicts.
- The minor number of trucks projected to continue travelling along Regional Road 25 and James Snow Parkway are not anticipated to create conflicts with transit services as the roadways have been designed to accommodate both heavy vehicles and transit. In the past, the development was operating with the same trip generation as is projected under future conditions and trucks were sharing the roadway network with the previously existing Transit Route 1 without any concern, which is presumed to continue under future conditions.


## Corner clearances

Based on The Transportation Association of Canada (TAC) Geometric Design Guidelines (2017) Figure 8.8.2, the minimum corner clearance required between the Dufferin Quarry access and Campbellville Road along Dublin Line (which is classified as a local road) is 15 m .

The quarry access is proposed to remain as under existing conditions as part of the planned extension and is located approximately 1.2 km north of Campbellville Road along

Dublin Line. Per the above, the location of the quarry access exceeds the minimum corner clearance requirements set by TAC, which is acceptable.
Similarly, the site access is located over 180m from either adjacent access along Dublin Line, exceeding the access spacing requirement of 3 m for commercial and industrial developments per TAC Figure 8.9.2. The spacing between accesses allows enough space for trucks to accelerate to the posted speed limit without impacting traffic along Dublin Line.

## Sight distances

The review of sight distances has been provided in the responses to JART comments provided in Appendix F of the October 2021 TIS, which has been copied below for reference.

Dublin Line is a relatively flat and straight roadway, with a posted speed limit of $60 \mathrm{~km} / \mathrm{h}$. Based on the Transportation Association of Canada (TAC) Geometric Design Standards (2017), a stopping sight distance requirement of 130 m is applicable to a design speed of $80 \mathrm{~km} / \mathrm{h}$ (assuming $20 \mathrm{~km} / \mathrm{h}$ over the posted speed limit). Based on the vertical and horizontal curvature of the roadway (as reviewed based on aerial on street imagery), it is TMIG's opinion that the stopping sight distance requirement is met at the existing quarry access intersection.
The satisfaction of the stopping sight distance along Dublin Line provides drivers traveling along the roadway with ample time to identify trucks entering the roadway and react accordingly.

## Vehicle-pedestrian conflicts \& Cycling Movements

The quarry access is located onto Dublin Line, which is a local road with a rural two-lane cross-section. Per the absence of sidewalks or cycling facilities along the roadway, it is presumed that there is negligible to no volumes of pedestrians or cyclists travelling along the corridor. Accordingly, the probability of conflicts between vehicles and pedestrians/cyclists at the access is minimal.
The remainder of the haul route is composed of municipal and regional roadways that have been designed to account for pedestrian and cyclists safety at each intersection and midblock. Accordingly, it is TMIG's opinion that there would not be any emphasized possibility of vehicle-pedestrian/cyclist conflicts for the specific quarry trucks compared to any other vehicles travelling along the roadway within the study area. As the roadways are presumed to be designed appropriately as per the Town and Region standards, it is TMIG's opinion that vehicle-pedestrian/cyclist conflicts would not be of concern regarding the proposed quarry extension.
Notwithstanding the above, TMIG understands that the implementation of the roundabout at the intersection of Dublin Line at James Snow Parkway has now provided pedestrian facilities with priority to pedestrian users. Accordingly, TMIG recommends that the applicant provides informational material to their drivers (in the form of pamphlets/informational boards located within the site) that would identify all potential
conflict locations between their vehicles and active transportation users. This information would be provided for the portion of the haul route located adjacent to the lands (i.e., north of Highway 401 along Dublin Line/Tremaine Road/Regional Road 25) to further assure that drivers are aware of the need to yield to active transportation users where applicable.

## Traffic infiltration

The quarry access is located onto Dublin Line, which terminates in a cul-de-sac approximately 2.1 km north of Campbellville Road.
There is a total of twenty developments located north of Campbellville Road along Dublin Line, which consist of three farms, fifteen residential dwellings and two golf courses. Accordingly, all traffic travelling along Dublin Line is local to the area. Except for non-local drivers unfamiliar with area, there is a nominal chance of traffic infiltration along Dublin Line. This is projected to remain the case under future conditions as Dublin Line is not planned to be extended further north of its current terminal point.

Finally, as the access is proposed to remain as under existing conditions, it is TMIG's opinion that there would be no changes to the existing operations at the access and along the roadway thus eliminating the concern related to quarry traffic infiltration to the neighbouring driveways along Dublin Line.

## Access conflicts

As stated previously, all traffic travelling along Dublin Line at the site access intersection is local to the study area, minor in magnitude, and is not anticipated to create any congestion at the access as per the traffic operations review completed as part of the TIS.

Additionally, based on a desktop review of the roadway curvature using aerial imagery, there are no anticipated vertical or horizontal sightline concerns at the site access intersection.

Finally, per the absence of pedestrian and cycling facilities along Dublin Line, it is presumed that the volume of active transportation users is very minor in magnitude thus removing any significant concern for conflict between trucks and active transportation users.

Per the above, it is TMIG's opinion that there would be no concern for conflict at the site access between traffic travelling to/form the quarry and traffic along Dublin Line or with active transportation users.

## Heavy truck movement conflicts

The existing quarry access to Dublin Line has been designed to accommodate heavy truck movements to/from the roadway when the quarry was first implemented and is projected to remain the principal access post extension.
As previously stated, Dublin Line only provides access to local traffic. Accordingly, the large majority of trucks travelling along the roadway will be to/from the quarry, thus limiting the number of conflicts between heavy vehicles on Dublin Line. Operations are projected
to remain as under existing conditions, with no anticipated concerns for heavy vehicle movements.
Finally, outside of the site access intersection to Dublin Line, all traffic generated by the quarry will utilize the Town and Region roads, which have been designed to accommodate the truck routes utilized by the development. Accordingly, as the study area roadways have been designed per the Town and Region standards, it is TMIG's opinion that there should also be no concerns related to heavy truck movement. As per the Region's Transportation Master Plan, Tremaine Road, James Snow Parkway and Regional Road 25 are classified as C4 Urban roadway, while Campbellville Road is classified as a Town minor arterial, which are designed to accommodate heavy trucks. Furthermore, the roundabout at Dublin Line allows for reduced conflict points compared to a standard 4-legged intersection, which further improves circulation as opposed to previous conditions.

## Queuing

As previously stated, the trip generation associated with the quarry is projected to remain as under existing conditions post extension, with the multiple trucks projected to be rerouted from the Highway 401 interchange at Regional Road 25 to the planned interchange at Tremaine Road.

As detailed in the October 2021 TIS completed for the proposed development, queues at the roundabout and future Highway 401 interchange to Tremaine Road are projected to be acceptable. Furthermore, as the site traffic volume is projected to be reduced along Regional Road 25, queues associated with the site traffic are projected to remain as under existing conditions or improve at the Regional Road 25 intersections along the haul route.
Per the above, it is TMIG's opinion that there would be no queuing concerns associated with the development application.

Overall, the analysis detailed within this letter confirms that there would be no safety concerns associated with the proposed development application. Please do not hesitate to contact the undersigned should you require any additional assistance.

Sincerely,

## TMIG | THE MUNICIPAL INFRASTRUCTURE GROUP LTD.



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Michael Dowdall C.E.T., MITE Director, Traffic | mdowdall@tmig.ca

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\text { Attachment } 2
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PROJECT No. 10108

## To: Kevin Mitchell, Director of Property, Planning \& Approvals

Address: CRH Canada Group Inc.<br>2300 Steeles Avenue West, $4^{\text {th }}$ FI Concord, ON, L4K5X6

## From: Michael Dowdall, TYLin

Date: July 22, 2022

## CC: Brian Zeman, MHBC Ellen Ferris, MHBC

## Re: Proposed Dufferin Aggregates Milton Quarry East Extension - Sightline Analysis

## MEMORANDUM

TYLin (formerly, the Municipal Infrastructure Group Ltd. (TMIG), a T.Y. Lin International Company), was retained by Dufferin Aggregates (a division of CRH Canada Group Inc.) to prepare a Traffic Impact Study (TIS) and Haul Route Assessment in support of the proposed Milton Quarry East Extension in the Town of Milton. The TIS report was prepared in October 2021, which included an initial response to pre-consultation comments detailing a desktop review of quarry access stopping sight distance sightlines based on aerial and street imagery. Subsequent to the study submission, Halton Region staff provided comments to the project team identifying that the Safety Analysis component of the study (required as per the 2015 Halton Region TIS guidelines) was incomplete. Accordingly, a letter was prepared as an additional component to the development application in order to address the Region's request for a safety analysis.
Further comments were received from the review agencies stating that the review of quarry access sightlines was based solely on aerial and street imagery, and should be informed by a site visit to confirm sightlines. Accordingly, TYLin conducted a site visit to confirm sightlines in the field, with the results summarized in the memo below. The visit was conducted on Thursday, July 21, 2022.

The sightline review was undertaken based on values from the Transportation Association of Canada (TAC) Geometric Design Guide for Canadian Roads, 2017. From the posted speed limit of $60 \mathrm{~km} / \mathrm{h}$, a conservative design speed of $80 \mathrm{~km} / \mathrm{h}$ was determined (typically taken to be 20 $\mathrm{km} / \mathrm{h}$ over the posted speed limit). Based on the design speed, the desired design values for both stopping sight distance (SSD), intersection sight distance (ISD) and the more conservative minimum decision sight distance (DSD) are provided in Table 1 in accordance with TAC Tables 9.9.4 and 9.9.6., and Figure 9.10.1. Excerpts from the TAC Manual are supplied in Attachment 1.

## TYLin

PROJECT No. 10108

Table 1 Minimum Sight Distances for Passenger Cars from TAC 2017

| Design Speed <br> $\mathbf{( k m} / \mathbf{h r})$ | Left-Turn from Stop |  | Right-Turn from Stop |  | Minimum Decision <br> Sight Distance (m) |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | SSD (m) | ISD (m) | SSD (m) | ISD (m) |  |
| 80 | 130 | 170 | 130 | 145 |  |

Based on the values above, the SSD and DSD were reviewed in the field for the quarry access at 9410 Dublin Line, Milton, Ontario.

As per the TAC manual, sight distances were observed considering the following key variables:

- Driver's eye vertical height of 1.08 metres from the ground;
- Height to the top of car bumper of 0.6 metres (conservative approach) and height to the top of the car of 1.3 metres from the ground.

The field observation confirmed that both the minimum SSD of 130 metres as well as the DSD of 230 metres were met on Dublin Line both north and south of the quarry access. As the DSD was met, it was inferred that the ISD requirement was also satisfied. TYLin staff members were able to observe both the 0.6 -metre and 1.3 -metre-high object approaching from the north, while from the south the 1.3 metre-high object was visible at both distances. Although the 0.6 metrehigh object was not visible from the south, the sightline was still deemed acceptable given that the 1.3 -metre high object was observed, indicating that vehicles entering Dublin Line from the quarry access will be able to see a vehicle approaching from the south at the desired distance. Photos documenting the sight distances are included in Attachment 2, in which photos from the SSD and DSD both south and north of the quarry access were taken at the driver's eye height.

In conclusion, the applicable SSD and DSD requirements for the Milton Quarry access were deemed to be met based on field observation by TYLin staff (thereby also meeting ISD requirements).

Attachments:
Attachment 1 - Excerpts from TAC 2017
Attachment 2 - Site Visit Photos (2022-07-21)

## 'TYLin

Attachment 1: Excerpts from TAC 2017


Note: Intersection sight distance shown is for a stopped passenger car to turn left onto a two-lane highway with no median and grades $3 \%$ or less. For other conditions, the time gap should be adjusted and the sight distance recalculated.

Sight distance design for left turns at divided-highway intersections should consider multiple design vehicles and median width. If the design vehicle used to determine sight distance for a divided-highway intersection is larger than a passenger car, then sight distance for left turns will need to be checked for that selected design vehicle and for smaller design vehicles as well. If the divided-highway median is wide enough to store the design vehicle with a clearance to the through lanes of approximately 1 m at both ends of the vehicle, no separate analysis for the departure sight triangle for left turns is needed on the minor-road approach for the near roadway to the left. In most cases, the departure sight triangle for right turns (case B2) will provide sufficient sight distance for a passenger car to cross the near roadway to reach the median. Possible exceptions are addressed in the discussion of case B3.

Table 9.9.6: Design Intersection Sight Distance - Case B2, Right Turn from Stop, and Case B3, Crossing Maneuver

| Design Speed <br> $\mathbf{( k m / h )}$ | Stopping Sight <br> Distance $\mathbf{( m )}$ | Intersection Sight Distance for Passenger Cars |  |
| :---: | :---: | :---: | :---: |
| 20 | 20 | Calculated $\mathbf{( m )}$ | Design $\mathbf{( m )}$ |
| 30 | 35 | 54.1 | 40 |
| 40 | 50 | 72.3 | 55 |
| 50 | 65 | 90.4 | 75 |
| 60 | 85 | 108.4 | 95 |
| 70 | 105 | 126.5 | 110 |
| 80 | 130 | 144.6 | 130 |
| 90 | 160 | 162.6 | 145 |
| 100 | 185 | 180.7 | 165 |
| 110 | 220 | 198.8 | 185 |
| 120 | 250 | 216.8 | 200 |
| 130 | 285 | 234.9 | 220 |

Note: Intersection sight distance shown is for a stopped passenger car to turn right onto or to cross a two-lane highway with no median and with grades of $3 \%$ or less. For other conditions, the time gap should be adjusted and the sight distance recalculated.


Figure 9.9.5: Intersection Sight Distance - Case B2, Right Turn from Stop, and Case B3, Crossing Maneuver (Calculated and Design Values Plotted)

Maneuver time is the time to accomplish a vehicle maneuver. For design purposes, the calculated values are rounded. For guidance on selecting decision sight distance, refer to Chapter 2.


Figure 9.10.1: Decision Sight Distance ${ }^{72}$

### 9.11 SIGHT DISTANCE AT BRIDGE STRUCTURES

Where a bridge is close to an at-grade intersection, such as at the intersection of an interchange ramp with a cross road adjacent to an overpass, particular attention is required to ensure adequate sight distance is provided. This is due to the potential visual obstruction created by the bridge railing or other structural components. The typical critical factor, at a ramp intersection, is the sight distance required for the left-turning vehicle departing from the ramp to clear the traffic approaching from the left on the cross road. If the intersection is signalized, the minimum critical sight distance is then the distance needed for vehicles turning right, off the ramp, to clear vehicles approaching from the left. However, it


## 'M/Lin



## 'IYLin



Photo 5: View from object marker from 130 m SSD, south of access


Photo 6: Decision sight distance of 230 m , south of access

## TYLin



## TYLin



## TYLin



## 'TYLin



## 'IYLin

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\text { Attachment } 3
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## TYLin

Table 12026 Future AM Traffic Synchro and Arcady Results

| Intersection | Control Type | Existing Haul Route |  |  | Future Haul Route |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | AM Peak Hour |  |  |  |  |  |
| Turning Movement | - | V/C | Delay | LOS | V/C | Delay | LOS |
| Dublin Line / Tremaine Road at James Snow Parkway / Campbellville Road | Roundabout | - | 5.22 | A | - | 6.94 | A |
| James Snow Parkway (Westbound Approach) | - | 0.49 | 3.07 | A | 0.41 | 2.64 | A |
| Dublin Line (Southbound Approach) | - | 0.43 | 13.82 | B | 0.43 | 13.76 | B |
| Campbellville Road (Eastbound Approach) | - | 0.52 | 4.77 | A | 0.52 | 4.76 | A |
| Tremaine Road (Northbound Approach) | - | 0.22 | 5.22 | A | 0.50 | 9.60 | A |
| Tremaine Road at Highway 401 Westbound Off-Ramp | Signal | 0.52 | 14 | B | 0.71 | 19 | B |
| Westbound Right | - | 0.65 | 24 | C | 0.84 | 33 | C |
| Tremaine Road at Highway 401 Eastbound Off-Ramp | Signal | 0.45 | 15 | B | 0.45 | 15 | B |
| Regional Road 25 / James Snow Parkway | Signal | 0.59 | 21 | C | 0.50 | 18 | B |
| Northbound Left | - | 0.65 | 13 | B | 0.33 | 9 | A |
| Eastbound Through | - | 0.20 | 52 | D | 0.23 | 52 | D |
| Eastbound Right | - | 0.18 | 52 | D | 0.03 | 51 | D |
| Westbound Through | - | 0.24 | 47 | D | 0.26 | 47 | D |
| Regional Road 25 / Highway 401 Westbound Off-Ramp | Signal | 0.45 | 10 | A | 0.40 | 10 | A |
| Northbound Through | - | 0.30 | 6 | A | 0.30 | 6 | A |
| Westbound Left | - | 0.56 | 24 | C | 0.56 | 24 | C |
| Southbound Through | - | 0.41 | 7 | A | 0.35 | 7 | A |
| Regional Road 25 / Highway 401 Eastbound Off-Ramp | Signal | 0.70 | 34 | C | 0.70 | 34 | C |
| Northbound Through-Right | - | 0.62 | 31 | C | 0.62 | 31 | C |
| Eastbound Left | - | 0.94 | 63 | E | 0.94 | 61 | E |
| Southbound Through | - | 0.51 | 24 | C | 0.51 | 24 | C |

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\text { Attachment } 4
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## TYLin

Table 22026 Future PM Traffic Synchro and Arcady Results

| Intersection | Control Type | Existing Haul Route |  |  | Future Haul Route |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | PM Peak Hour |  |  |  |  |  |
| Turning Movement | - | V/C | Delay | LOS | V/C | Delay | LOS |
| Dublin Line / Tremaine Road at James Snow Parkway / Campbellville Road | Roundabout | - | 6.79 | A | - | 6.97 | A |
| James Snow Parkway (Westbound Approach) | - | 0.75 | 5.42 | A | 0.74 | 5.19 | A |
| Dublin Line (Southbound Approach) | - | 0.52 | 39.25 | E | 0.52 | 39.20 | E |
| Campbellville Road (Eastbound Approach) | - | 0.55 | 7.35 | A | 0.55 | 7.34 | A |
| Tremaine Road (Northbound Approach) | - | 0.18 | 4.16 | A | 0.27 | 5.40 | A |
| Tremaine Road at Highway 401 Westbound Off-Ramp | Signal | 0.73 | 17 | B | 0.74 | 18 | B |
| Westbound Right | - | 0.24 | 15 | B | 0.33 | 15 | B |
| Tremaine Road at Highway 401 Eastbound Off-Ramp | Signal | 0.80 | 27 | C | 0.80 | 27 | C |
| Regional Road 25 / James Snow Parkway | Signal | 0.57 | 29 | C | 0.58 | 29 | C |
| Northbound Left | - | 0.39 | 13 | B | 0.24 | 13 | B |
| Eastbound Through | - | 0.45 | 56 | E | 0.46 | 56 | E |
| Eastbound Right | - | 0.17 | 53 | D | 0.13 | 53 | D |
| Westbound Through | - | 0.20 | 45 | D | 0.20 | 45 | D |
| Regional Road 25 / Highway 401 Westbound Off-Ramp | Signal | 0.49 | 9 | A | 0.48 | 9 | A |
| Northbound Through | - | 0.40 | 7 | A | 0.40 | 7 | A |
| Westbound Left | - | 0.56 | 23 | C | 0.56 | 23 | C |
| Southbound Through | - | 0.47 | 8 | A | 0.45 | 7 | A |
| Regional Road 25 / <br> Highway 401 Eastbound Off-Ramp | Signal | 0.57 | 22 | C | 0.57 | 22 | C |
| Northbound Through-Right | - | 0.68 | 21 | C | 0.68 | 21 | C |
| Eastbound Left | - | 0.56 | 38 | D | 0.55 | 38 | D |
| Southbound Through | - | 0.43 | 14 | B | 0.43 | 14 | B |

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|  | $\rangle$ | $\rightarrow$ |  | $\checkmark$ |  | 4 | 4 | $\uparrow$ | p |  | $\downarrow$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Right Turn Channelized |  |  |  |  |  |  |  |  |  |  |  |  |
| Traffic Volume (veh/h) | 8 | 405 | 309 | 575 | 254 | 169 | 178 | 0 | 712 | 167 | 0 | 7 |
| Future Volume (veh/h) | 8 | 405 | 309 | 575 | 254 | 169 | 178 | 0 | 712 | 167 | 0 | 7 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Hourly flow rate (vph) | 9 | 440 | 336 | 625 | 276 | 184 | 193 | 0 | 774 | 182 | 0 | 8 |
| Approach Volume (veh/h) |  | 785 |  |  | 1085 |  |  | 967 |  |  | 190 |  |
| Crossing Volume (veh/h) |  | 807 |  |  | 202 |  |  | 631 |  |  | 1094 |  |
| High Capacity (veh/h) |  | 729 |  |  | 1182 |  |  | 840 |  |  | 576 |  |
| High v/c (veh/h) |  | 1.08 |  |  | 0.92 |  |  | 1.15 |  |  | 0.33 |  |
| Low Capacity (veh/h) |  | 575 |  |  | 977 |  |  | 672 |  |  | 443 |  |
| Low v/c (veh/h) |  | 1.37 |  |  | 1.11 |  |  | 1.44 |  |  | 0.43 |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Maximum v/c High |  |  | 1.15 |  |  |  |  |  |  |  |  |  |
| Maximum v/c Low |  |  | 1.44 |  |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization |  |  | 104.4\% |  | CU Level | f Service |  |  | G |  |  |  |


| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | \％ | ¢ $\uparrow$ | F | \％ | ¢ $\uparrow$ | F | 7 | 个个4 | F | ${ }^{7}$ | 个中的 |  |
| Traffic Volume（vph） | 12 | 57 | 182 | 62 | 117 | 62 | 309 | 552 | 418 | 231 | 483 | 32 |
| Future Volume（vph） | 12 | 57 | 182 | 62 | 117 | 62 | 309 | 552 | 418 | 231 | 483 | 32 |
| Ideal Flow（vphpl） | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.0 | 3.5 | 3.5 | 3.0 | 3.5 | 3.5 |
| Total Lost time（s） | 4.0 | 6.6 | 6.6 | 4.0 | 6.6 | 6.6 | 4.0 | 6.9 | 6.9 | 4.0 | 6.9 |  |
| Lane Util．Factor | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.91 | 1.00 | 1.00 | 0.91 |  |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 0.99 |  |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |  |
| Satd．Flow（prot） | 1190 | 2625 | 1079 | 1231 | 3077 | 1166 | 1416 | 4071 | 1426 | 1359 | 4015 |  |
| FIt Permitted | 0.68 | 1.00 | 1.00 | 0.56 | 1.00 | 1.00 | 0.44 | 1.00 | 1.00 | 0.43 | 1.00 |  |
| Satd．Flow（perm） | 846 | 2625 | 1079 | 723 | 3077 | 1166 | 656 | 4071 | 1426 | 612 | 4015 |  |
| Peak－hour factor，PHF | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 |
| Adj．Flow（vph） | 12 | 59 | 188 | 64 | 121 | 64 | 319 | 569 | 431 | 238 | 498 | 33 |
| RTOR Reduction（vph） | 0 | 0 | 167 | 0 | 0 | 54 | 0 | 0 | 188 | 0 |  | 0 |
| Lane Group Flow（vph） | 12 | 59 | 21 | 64 | 121 | 10 | 319 | 569 | 243 | 238 | 527 | 0 |
| Heavy Vehicles（\％） | 50\％ | 36\％ | 48\％ | 45\％ | 16\％ | 37\％ | 19\％ | 26\％ | 12\％ | 24\％ | 25\％ | 50\％ |
| Turn Type | pm＋pt | NA | Perm | pm＋pt | NA | Perm | pm＋pt | NA | Perm | pm＋pt | NA |  |
| Protected Phases | 7 | 4 |  | ， | 8 |  | 5 | 2 |  | 1 | 6 |  |
| Permitted Phases | 4 |  | 4 | 8 |  | 8 | 2 |  | 2 | 6 |  |  |
| Actuated Green，G（s） | 17.0 | 14.1 | 14.1 | 27.2 | 20.3 | 20.3 | 82.2 | 71.1 | 71.1 | 80.8 | 70.4 |  |
| Effective Green， $\mathrm{g}(\mathrm{s})$ | 17.0 | 14.1 | 14.1 | 27.2 | 20.3 | 20.3 | 82.2 | 71.1 | 71.1 | 80.8 | 70.4 |  |
| Actuated g／C Ratio | 0.13 | 0.11 | 0.11 | 0.22 | 0.16 | 0.16 | 0.65 | 0.56 | 0.56 | 0.64 | 0.56 |  |
| Clearance Time（s） | 4.0 | 6.6 | 6.6 | 4.0 | 6.6 | 6.6 | 4.0 | 6.9 | 6.9 | 4.0 | 6.9 |  |
| Vehicle Extension（s） | 3.0 | 5.0 | 5.0 | 3.0 | 5.0 | 5.0 | 3.0 | 5.0 | 5.0 | 3.0 | 5.0 |  |
| Lane Grp Cap（vph） | 121 | 293 | 120 | 192 | 494 | 187 | 494 | 2293 | 803 | 453 | 2239 |  |
| v／s Ratio Prot | 0.00 | 0.02 |  | c0．02 | 0.04 |  | c0．06 | 0.14 |  | 0.04 | 0.13 |  |
| v／s Ratio Perm | 0.01 |  | 0.02 | c0．05 |  | 0.01 | c0．36 |  | 0.17 | 0.29 |  |  |
| v／c Ratio | 0.10 | 0.20 | 0.18 | 0.33 | 0.24 | 0.06 | 0.65 | 0.25 | 0.30 | 0.53 | 0.24 |  |
| Uniform Delay，d1 | 47.7 | 50.9 | 50.8 | 41.0 | 46.3 | 44.8 | 10.1 | 14.0 | 14.5 | 9.9 | 14.2 |  |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |
| Incremental Delay，d2 | 0.4 | 0.7 | 1.5 | 1.0 | 0.5 | 0.3 | 2.9 | 0.3 | 1.0 | 1.1 | 0.2 |  |
| Delay（s） | 48.1 | 51.6 | 52.2 | 42.1 | 46.8 | 45.1 | 13.0 | 14.2 | 15.5 | 11.0 | 14.5 |  |
| Level of Service | D | D | D | D | D | D | B | B | B | B | B |  |
| Approach Delay（s） |  | 51.9 |  |  | 45.1 |  |  | 14.3 |  |  | 13.4 |  |
| Approach LOS |  | D |  |  | D |  |  | B |  |  | B |  |


| Intersection Summary |  |  |  |
| :--- | ---: | :--- | ---: |
| HCM 2000 Control Delay | 20.8 | HCM 2000 Level of Service | C |
| HCM 2000 Volume to Capacity ratio | 0.59 |  | 21.5 |
| Actuated Cycle Length（s） | 126.2 | Sum of lost time（s） | B |
| Intersection Capacity Utilization | $61.6 \%$ | ICU Level of Service |  |

c Critical Lane Group


Analysis Period (min)
15
c Critical Lane Group

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | \% | $\uparrow$ | F |  | $\uparrow$ |  |  | 个蚛 |  | ${ }^{7}$ | 444 |  |
| Traffic Volume (vph) | 502 | 20 | 638 | 20 | - | 26 | 0 | 997 | 27 | 24 | 962 | 0 |
| Future Volume (vph) | 502 | 20 | 638 | 20 | 0 | 26 | 0 | 997 | 27 | 24 | 962 | 0 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width | 3.8 | 3.8 | 3.8 | 3.2 | 3.7 | 3.5 | 3.4 | 3.4 | 3.4 | 3.0 | 3.4 | 3.4 |
| Total Lost time (s) | 6.6 | 6.6 | 6.6 |  | 6.8 |  |  | 6.6 |  | 3.0 | 6.6 |  |
| Lane Util. Factor | 1.00 | 0.95 | 0.95 |  | 1.00 |  |  | 0.91 |  | 1.00 | 0.91 |  |
| Frt | 1.00 | 0.86 | 0.85 |  | 0.92 |  |  | 1.00 |  | 1.00 | 1.00 |  |
| Flt Protected | 0.95 | 1.00 | 1.00 |  | 0.98 |  |  | 1.00 |  | 0.95 | 1.00 |  |
| Satd. Flow (prot) | 1693 | 1474 | 1466 |  | 1532 |  |  | 4480 |  | 1440 | 4449 |  |
| Flt Permitted | 0.95 | 1.00 | 1.00 |  | 0.98 |  |  | 1.00 |  | 0.17 | 1.00 |  |
| Satd. Flow (perm) | 1693 | 1474 | 1466 |  | 1532 |  |  | 4480 |  | 261 | 4449 |  |
| Peak-hour factor, PHF | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 |
| Adj. Flow (vph) | 512 | 20 | 651 | 20 | 0 | 27 | 0 | 1017 | 28 | 24 | 982 | 0 |
| RTOR Reduction (vph) | 0 | 125 | 125 | 0 | 44 | 0 | 0 | 3 | 0 | 0 | 0 | 0 |
| Lane Group Flow (vph) | 512 | 214 | 207 | 0 | 3 | 0 | 0 | 1042 | 0 | 24 | 982 | 0 |
| Heavy Vehicles (\%) | 9\% | 16\% | 7\% | 15\% | 0\% | 12\% | 0\% | 13\% | 4\% | 17\% | 14\% | 0\% |
| Turn Type | Split | NA | Perm | Split | NA |  |  | NA |  | pm+pt | NA |  |
| Protected Phases | 4 | 4 |  | 8 | 8 |  |  | 2 |  | 1 | 6 |  |
| Permitted Phases |  |  | 4 |  |  |  |  |  |  | 6 |  |  |
| Actuated Green, G (s) | 36.4 | 36.4 | 36.4 |  | 7.6 |  |  | 42.4 |  | 49.4 | 49.4 |  |
| Effective Green, g (s) | 36.4 | 36.4 | 36.4 |  | 7.6 |  |  | 42.4 |  | 49.4 | 49.4 |  |
| Actuated g/C Ratio | 0.32 | 0.32 | 0.32 |  | 0.07 |  |  | 0.37 |  | 0.44 | 0.44 |  |
| Clearance Time (s) | 6.6 | 6.6 | 6.6 |  | 6.8 |  |  | 6.6 |  | 3.0 | 6.6 |  |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 |  | 3.0 |  |  | 3.0 |  | 3.0 | 3.0 |  |
| Lane Grp Cap (vph) | 543 | 473 | 470 |  | 102 |  |  | 1675 |  | 155 | 1938 |  |
| v/s Ratio Prot | c0.30 | 0.15 |  |  | c0.00 |  |  | c0.23 |  | 0.01 | c0.22 |  |
| v/s Ratio Perm |  |  | 0.14 |  |  |  |  |  |  | 0.06 |  |  |
| $\mathrm{v} / \mathrm{c}$ Ratio | 0.94 | 0.45 | 0.44 |  | 0.03 |  |  | 0.62 |  | 0.15 | 0.51 |  |
| Uniform Delay, d1 | 37.5 | 30.6 | 30.4 |  | 49.5 |  |  | 29.0 |  | 19.5 | 23.2 |  |
| Progression Factor | 1.00 | 1.00 | 1.00 |  | 1.00 |  |  | 1.00 |  | 1.00 | 1.00 |  |
| Incremental Delay, d2 | 25.1 | 0.7 | 0.7 |  | 0.1 |  |  | 1.8 |  | 0.5 | 0.9 |  |
| Delay (s) | 62.5 | 31.3 | 31.1 |  | 49.6 |  |  | 30.7 |  | 20.0 | 24.1 |  |
| Level of Service | E | C | C |  | D |  |  | C |  | B | C |  |
| Approach Delay (s) |  | 44.8 |  |  | 49.6 |  |  | 30.7 |  |  | 24.0 |  |
| Approach LOS |  | D |  |  | D |  |  | C |  |  | C |  |


| Intersection Summary |  |  |  |
| :--- | ---: | :--- | ---: |
| HCM 2000 Control Delay | 34.0 | HCM 2000 Level of Service | C |
| HCM 2000 Volume to Capacity ratio | 0.70 |  | 23.0 |
| Actuated Cycle Length (s) | 113.4 | Sum of lost time (s) | C |
| Intersection Capacity Utilization | $69.9 \%$ | ICU Level of Service |  |

Analysis Period (min)
15
c Critical Lane Group

|  |  | $4$ | $\dagger$ | \% | $1$ | $\frac{1}{7}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |  |
| Lane Configurations | ${ }^{7} 1$ | 「 | 中4 |  |  | 44 |  |
| Traffic Volume (vph) | 406 | 431 | 459 | 0 | 0 | 755 |  |
| Future Volume (vph) | 406 | 431 | 459 | 0 | 0 | 755 |  |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |  |
| Lane Width | 3.8 | 3.8 | 3.4 | 3.4 | 3.4 | 3.4 |  |
| Total Lost time (s) | 6.2 | 6.2 | 6.4 |  |  | 6.4 |  |
| Lane Util. Factor | 0.97 | 1.00 | 0.95 |  |  | 0.95 |  |
| Frt | 1.00 | 0.85 | 1.00 |  |  | 1.00 |  |
| Flt Protected | 0.95 | 1.00 | 1.00 |  |  | 1.00 |  |
| Satd. Flow (prot) | 3284 | 1448 | 3180 |  |  | 3096 |  |
| Flt Permitted | 0.95 | 1.00 | 1.00 |  |  | 1.00 |  |
| Satd. Flow (perm) | 3284 | 1448 | 3180 |  |  | 3096 |  |
| Peak-hour factor, PHF | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |
| Adj. Flow (vph) | 406 | 431 | 459 | 0 | 0 | 755 |  |
| RTOR Reduction (vph) | 0 | 183 | 0 | 0 | 0 | 0 |  |
| Lane Group Flow (vph) | 406 | 248 | 459 | 0 | 0 | 755 |  |
| Heavy Vehicles (\%) | 9\% | 14\% | 11\% | 0\% | 0\% | 14\% |  |
| Turn Type | Prot | Perm | NA |  |  | NA |  |
| Protected Phases | 8 |  | 2 |  |  | 6 |  |
| Permitted Phases |  | 8 |  |  |  |  |  |
| Actuated Green, G (s) | 16.1 | 16.1 | 32.5 |  |  | 32.5 |  |
| Effective Green, g (s) | 16.1 | 16.1 | 32.5 |  |  | 32.5 |  |
| Actuated g/C Ratio | 0.26 | 0.26 | 0.53 |  |  | 0.53 |  |
| Clearance Time (s) | 6.2 | 6.2 | 6.4 |  |  | 6.4 |  |
| Vehicle Extension (s) | 3.0 | 3.0 | 4.4 |  |  | 4.4 |  |
| Lane Grp Cap (vph) | 863 | 380 | 1688 |  |  | 1644 |  |
| v/s Ratio Prot | 0.12 |  | 0.14 |  |  | c0.24 |  |
| v/s Ratio Perm |  | c0.17 |  |  |  |  |  |
| v/c Ratio | 0.47 | 0.65 | 0.27 |  |  | 0.46 |  |
| Uniform Delay, d1 | 19.0 | 20.1 | 7.9 |  |  | 8.9 |  |
| Progression Factor | 1.00 | 1.00 | 1.00 |  |  | 1.00 |  |
| Incremental Delay, d2 | 0.4 | 4.0 | 0.4 |  |  | 0.9 |  |
| Delay (s) | 19.4 | 24.0 | 8.3 |  |  | 9.8 |  |
| Level of Service | B | C | A |  |  | A |  |
| Approach Delay (s) | 21.8 |  | 8.3 |  |  | 9.8 |  |
| Approach LOS | C |  | A |  |  | A |  |
| Intersection Summary |  |  |  |  |  |  |  |
| HCM 2000 Control Delay |  |  | 14.3 |  | HCM 2000 | evel of Service | B |
| HCM 2000 Volume to Capacity ratio |  |  | 0.52 |  |  |  |  |
| Actuated Cycle Length (s) |  |  | 61.2 |  | Sum of los | ime (s) | 12.6 |
| Intersection Capacity Utilization |  |  | 53.9\% |  | ICU Level | Service | A |
| Analysis Period (min) |  |  | 15 |  |  |  |  |

C Critical Lane Group

|  | $\dagger$ | $\rightarrow$ |  | $\dagger$ |  | 4 |  | $\dagger$ | \％ |  | $\downarrow$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \％ | $\uparrow$ | F | \％ |  | 「 |  | 个 ${ }^{\text {a }}$ |  | 7 | 个 4 |  |
| Traffic Volume（vph） | 76 | 3 | 101 | 25 | 0 | 25 | 0 | 762 | 45 | 45 | 851 | 0 |
| Future Volume（vph） | 76 | 3 | 101 | 25 | 0 | 25 | 0 | 762 | 45 | 45 | 851 | 0 |
| Ideal Flow（vphpl） | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width | 3.8 | 3.8 | 3.8 | 3.2 | 3.7 | 3.5 | 3.4 | 3.4 | 3.4 | 3.0 | 3.4 | 3.4 |
| Total Lost time（s） | 6.6 | 6.6 | 6.6 | 6.8 |  | 6.8 |  | 6.6 |  | 3.0 | 6.6 |  |
| Lane Util．Factor | 1.00 | 0.95 | 0.95 | 1.00 |  | 1.00 |  | 0.95 |  | 1.00 | 0.95 |  |
| Frt | 1.00 | 0.86 | 0.85 | 1.00 |  | 0.85 |  | 0.99 |  | 1.00 | 1.00 |  |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 |  | 1.00 |  | 1.00 |  | 0.95 | 1.00 |  |
| Satd．Flow（prot） | 1693 | 1473 | 1466 | 1500 |  | 1426 |  | 3111 |  | 1440 | 3096 |  |
| Flt Permitted | 0.95 | 1.00 | 1.00 | 0.95 |  | 1.00 |  | 1.00 |  | 0.29 | 1.00 |  |
| Satd．Flow（perm） | 1693 | 1473 | 1466 | 1500 |  | 1426 |  | 3111 |  | 438 | 3096 |  |
| Peak－hour factor，PHF | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 |
| Adj．Flow（vph） | 78 | 3 | 103 | 26 | 0 | 26 | 0 | 778 | 46 | 46 | 868 | 0 |
| RTOR Reduction（vph） | 0 | 46 | 48 | 0 | 0 | 25 | 0 | 3 | 0 | 0 | 0 | 0 |
| Lane Group Flow（vph） | 78 | 7 | 5 | 26 | 0 | 1 | 0 | 821 | 0 | 46 | 868 | 0 |
| Heavy Vehicles（\％） | 9\％ | 16\％ | 7\％ | 15\％ | 0\％ | 12\％ | 0\％ | 13\％ | 4\％ | 17\％ | 14\％ | 0\％ |
| Turn Type | Split | NA | Perm | Prot |  | Perm |  | NA |  | pm＋pt | NA |  |
| Protected Phases | 4 | 4 |  | 8 |  |  |  | 2 |  | 1 | 6 |  |
| Permitted Phases |  |  | 4 |  |  | 8 |  |  |  | 6 |  |  |
| Actuated Green，G（s） | 8.8 | 8.8 | 8.8 | 5.5 |  | 5.5 |  | 59.0 |  | 65.9 | 65.9 |  |
| Effective Green， $\mathrm{g}(\mathrm{s})$ | 8.8 | 8.8 | 8.8 | 5.5 |  | 5.5 |  | 59.0 |  | 65.9 | 65.9 |  |
| Actuated g／C Ratio | 0.09 | 0.09 | 0.09 | 0.05 |  | 0.05 |  | 0.59 |  | 0.66 | 0.66 |  |
| Clearance Time（s） | 6.6 | 6.6 | 6.6 | 6.8 |  | 6.8 |  | 6.6 |  | 3.0 | 6.6 |  |
| Vehicle Extension（s） | 3.0 | 3.0 | 3.0 | 3.0 |  | 3.0 |  | 3.0 |  | 3.0 | 3.0 |  |
| Lane Grp Cap（vph） | 148 | 129 | 128 | 82 |  | 78 |  | 1831 |  | 327 | 2036 |  |
| v／s Ratio Prot | c0．05 | 0.01 |  | c0．02 |  |  |  | c0．26 |  | 0.01 | c0．28 |  |
| v／s Ratio Perm |  |  | 0.00 |  |  | 0.00 |  |  |  | 0.09 |  |  |
| v／c Ratio | 0.53 | 0.06 | 0.04 | 0.32 |  | 0.02 |  | 0.45 |  | 0.14 | 0.43 |  |
| Uniform Delay，d1 | 43.7 | 41.9 | 41.8 | 45.5 |  | 44.8 |  | 11.5 |  | 6.6 | 8.2 |  |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 |  | 1.00 |  | 1.00 |  | 1.00 | 1.00 |  |
| Incremental Delay，d2 | 3.4 | 0.2 | 0.1 | 2.2 |  | 0.1 |  | 0.8 |  | 0.2 | 0.7 |  |
| Delay（s） | 47.1 | 42.1 | 41.9 | 47.8 |  | 44.9 |  | 12.3 |  | 6.8 | 8.8 |  |
| Level of Service | D | D | D | D |  | D |  | B |  | A | A |  |
| Approach Delay（s） |  | 44.2 |  |  | 46.3 |  |  | 12.3 |  |  | 8.7 |  |
| Approach LOS |  | D |  |  | D |  |  | B |  |  | A |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 2000 Control Delay |  |  | 14.5 |  | CM 2000 | evel of S | ervice |  | B |  |  |  |
| HCM 2000 Volume to Capacity ratio |  |  | 0.45 |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length（s） |  |  | 100.2 |  | m of los | time（s） |  |  | 23.0 |  |  |  |
| Intersection Capacity Utilization |  |  | 55．8\％ | ICULevel or Service |  |  |  |  | B |  |  |  |
| Analysis Period（min） |  |  | 15 |  |  |  |  |  |  |  |  |  |

Analysis Period（min） 15
c Critical Lane Group

## Intersection: 1: Tremaine Road/Dublin Line \& Campbellville Road /James Snow Parkway

| Movement | EB | EB | WB | WB | NB | NB | SB |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | LT | R | LT | R | LT | R | LTR |
| Maximum Queue (m) | 82.6 | 48.5 | 1012.0 | 999.7 | 324.1 | 482.1 | 89.6 |
| Average Queue $(\mathrm{m})$ | 39.3 | 21.0 | 733.5 | 713.0 | 84.5 | 236.8 | 54.7 |
| 95th Queue $(\mathrm{m})$ | 75.0 | 37.1 | 1183.5 | 1190.0 | 276.1 | 477.2 | 98.3 |
| Link Distance $(\mathrm{m})$ | 622.3 | 622.3 | 1788.0 | 1788.0 | 764.7 | 764.7 | 71.8 |
| Upstream Blk Time (\%) |  |  |  |  |  |  | 26 |
| Queuing Penalty (veh) |  |  |  |  |  |  | 0 |

Storage Bay Dist (m)
Storage Blk Time (\%)
Queuing Penalty (veh)

## Intersection: 2: Regional Road 25 \& James Snow Parkway

| Movement | EB | EB | EB | EB | WB | WB | WB | WB | NB | NB | NB | NB |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Directions Served | L | T | T | R | L | T | T | R | L | T | T | T |
| Maximum Queue (m) | 19.5 | 26.2 | 25.2 | 46.6 | 51.1 | 38.5 | 36.5 | 31.3 | 84.4 | 55.7 | 50.9 | 45.9 |
| Average Queue (m) | 3.1 | 7.6 | 8.5 | 23.1 | 20.3 | 17.0 | 12.9 | 11.7 | 38.9 | 21.9 | 21.5 | 17.4 |
| 95th Queue (m) | 12.6 | 19.8 | 20.7 | 38.5 | 43.4 | 32.0 | 28.1 | 24.8 | 69.3 | 45.0 | 42.0 | 38.3 |
| Link Distance (m) |  | 1788.0 | 1788.0 |  |  | 728.6 | 728.6 |  |  | 744.3 | 744.3 | 744.3 |
| Upstream Blk Time (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |  |  |  |  |  |  |  |
| Storage Bay Dist (m) | 80.0 |  |  | 115.0 | 85.0 |  |  | 35.0 | 35.0 |  |  |  |
| Storage Blk Time (\%) |  |  |  |  |  |  | 1 | 0 | 12 | 2 |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |  | 0 | 0 | 22 | 7 |  |  |

Intersection: 2: Regional Road 25 \& James Snow Parkway

| Movement | NB | SB | SB | SB | SB |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Directions Served | R | L | T | T | TR |
| Maximum Queue $(\mathrm{m})$ | 85.7 | 76.0 | 49.1 | 53.1 | 46.2 |
| Average Queue $(\mathrm{m})$ | 22.9 | 33.5 | 21.0 | 22.2 | 15.2 |
| 95th Queue $(\mathrm{m})$ | 62.3 | 61.7 | 40.3 | 42.7 | 35.1 |
| Link Distance $(\mathrm{m})$ | 744.3 |  | 994.0 | 994.0 | 994.0 |
| Upstream Blk Time (\%) |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |
| Storage Bay Dist (m) |  | 75.0 |  |  |  |
| Storage Blk Time (\%) | 0 |  |  |  |  |
| Queuing Penalty (veh) |  | 1 |  |  |  |

Intersection: 3: Regional Road 25 \& Hwy 401 Westbound Off-Ramp

| Movement | WB | WB | NB | NB | NB | SB | SB | SB |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | L | L | T | T | T | T | T | T |
| Maximum Queue $(\mathrm{m})$ | 51.1 | 57.8 | 46.4 | 41.9 | 49.9 | 50.3 | 52.4 | 49.3 |
| Average Queue $(\mathrm{m})$ | 19.8 | 32.7 | 20.4 | 16.0 | 21.0 | 24.2 | 24.2 | 21.6 |
| 95th Queue $(\mathrm{m})$ | 40.5 | 50.5 | 38.5 | 34.3 | 41.0 | 41.7 | 43.5 | 42.1 |
| Link Distance $(\mathrm{m})$ |  |  | 339.1 | 339.1 | 339.1 | 744.3 | 744.3 | 744.3 |
| Upstream Blk Time (\%) |  |  |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |  |  |  |
| Storage Bay Dist (m) | 80.0 | 80.0 |  |  |  |  |  |  |
| Storage Blk Time (\%) |  | 0 |  |  |  |  |  |  |
| Queuing Penalty (veh) |  | 0 |  |  |  |  |  |  |

Intersection: 4: Regional Road 25 \& Hwy 401 Eastbound Off-Ramp/Carpool Lot

| Movement | EB | EB | EB | WB | NB | NB | NB | SB | SB | SB | SB |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Directions Served | L | TR | R | LTR | T | T | TR | L | T | T | T |
| Maximum Queue (m) | 147.3 | 134.2 | 70.0 | 33.6 | 106.4 | 96.8 | 65.9 | 28.0 | 70.1 | 78.2 | 84.7 |
| Average Queue (m) | 93.8 | 42.6 | 33.0 | 12.3 | 64.5 | 50.4 | 28.2 | 6.5 | 38.0 | 42.0 | 45.5 |
| 95th Queue (m) | 141.4 | 99.8 | 58.6 | 26.1 | 97.5 | 88.1 | 55.2 | 18.5 | 60.8 | 67.8 | 72.6 |
| Link Distance (m) |  | 434.1 |  | 85.8 | 183.3 | 183.3 | 183.3 |  | 339.1 | 339.1 | 339.1 |
| Upstream Blk Time (\%) |  |  |  |  |  |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |  |  |  |  |  |  |
| Storage Bay Dist (m) | 130.0 |  | 130.0 |  |  |  |  | 30.0 |  |  |  |
| Storage Blk Time (\%) | 3 | 0 |  |  |  |  |  | 0 | 14 |  |  |
| Queuing Penalty (veh) | 17 | 0 |  |  |  |  |  | 0 | 3 |  |  |

Intersection: 5: Tremaine Road \& Hwy 401 Westbound Off-Ramp

| Movement | WB | WB | WB | NB | NB | SB | SB |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Directions Served | L | L | R | T | T | T | T |
| Maximum Queue (m) | 53.6 | 48.8 | 67.8 | 50.9 | 46.3 | 54.7 | 48.2 |
| Average Queue (m) | 29.9 | 21.0 | 32.9 | 23.5 | 20.1 | 26.9 | 25.7 |
| 95th Queue (m) | 46.9 | 39.7 | 55.5 | 42.9 | 39.1 | 46.4 | 41.7 |
| Link Distance (m) | 387.2 | 387.2 |  | 301.3 | 301.3 | 764.7 | 764.7 |
| Upstream Blk Time (\%) |  |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |
| Storage Blk Time (\%) |  |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |  |  |

Intersection: 6: Tremaine Road \& Hwy 401 Eastbound Off-Ramp/Carpool Lot

| Movement | EB | EB | EB | WB | WB | NB | NB | SB | SB | SB |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Directions Served | L | TR | R | L | R | T | TR | L | T | T |
| Maximum Queue (m) | 41.7 | 22.2 | 15.6 | 23.4 | 20.2 | 76.6 | 67.8 | 25.9 | 64.3 | 64.2 |
| Average Queue (m) | 17.6 | 10.5 | 4.9 | 7.1 | 5.3 | 36.4 | 23.1 | 7.0 | 22.6 | 27.9 |
| 95th Queue (m) | 34.3 | 18.8 | 13.0 | 18.8 | 14.9 | 64.7 | 52.6 | 18.3 | 47.8 | 51.7 |
| Link Distance (m) |  | 455.1 |  | 125.3 |  | 250.9 | 250.9 |  | 301.3 | 301.3 |
| Upstream Blk Time (\%) |  |  |  |  |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |  |  |  |  |  |
| Storage Bay Dist (m) | 300.0 |  | 165.0 |  | 20.0 |  |  | 120.0 |  |  |
| Storage BIk Time (\%) |  |  |  | 2 | 0 |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  | 1 | 0 |  |  |  |  |  |

## Network Summary

Network wide Queuing Penalty: 51

|  | 4 | $\rightarrow$ |  | 7 |  | 4 | 4 | $\uparrow$ | 7 | - | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Right Turn Channelized |  |  |  |  |  |  |  |  |  |  |  |  |
| Traffic Volume (veh/h) | 8 | 405 | 309 | 575 | 254 | 16 | 178 | 153 | 712 | 14 | 153 | 7 |
| Future Volume (veh/h) | 8 | 405 | 309 | 575 | 254 | 16 | 178 | 153 | 712 | 14 | 153 | 7 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Hourly flow rate (vph) | 9 | 440 | 336 | 625 | 276 | 17 | 193 | 166 | 774 | 15 | 166 | 8 |
| Approach Volume (veh/h) |  | 785 |  |  | 918 |  |  | 1133 |  |  | 189 |  |
| Crossing Volume (veh/h) |  | 806 |  |  | 368 |  |  | 464 |  |  | 1094 |  |
| High Capacity (veh/h) |  | 729 |  |  | 1037 |  |  | 961 |  |  | 576 |  |
| High v/c (veh/h) |  | 1.08 |  |  | 0.89 |  |  | 1.18 |  |  | 0.33 |  |
| Low Capacity (veh/h) |  | 575 |  |  | 847 |  |  | 779 |  |  | 443 |  |
| Low v/c (veh/h) |  | 1.37 |  |  | 1.08 |  |  | 1.46 |  |  | 0.43 |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Maximum v/c High |  |  | 1.18 |  |  |  |  |  |  |  |  |  |
| Maximum v/c Low |  |  | 1.46 |  |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization |  |  | 108.2\% |  | CU Level | Service |  |  | G |  |  |  |


| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | \％ | 个4 | F | \％ | ¢ $\uparrow$ | 「 | \％ | 个个4 | F | ${ }^{7}$ | 恌 ${ }^{\text {d }}$ |  |
| Traffic Volume（vph） | 12 | 57 | 29 | 62 | 117 | 62 | 156 | 552 | 418 | 231 | 483 | 32 |
| Future Volume（vph） | 12 | 57 | 29 | 62 | 117 | 62 | 156 | 552 | 418 | 231 | 483 | 32 |
| Ideal Flow（vphpl） | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.0 | 3.5 | 3.5 | 3.0 | 3.5 | 3.5 |
| Total Lost time（s） | 4.0 | 6.6 | 6.6 | 4.0 | 6.6 | 6.6 | 4.0 | 6.9 | 6.9 | 4.0 | 6.9 |  |
| Lane Util．Factor | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.91 | 1.00 | 1.00 | 0.91 |  |
| Frpb，ped／bikes | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.99 | 1.00 | 1.00 |  |
| Flpb，ped／bikes | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 0.99 |  |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |  |
| Satd．Flow（prot） | 1190 | 2625 | 1079 | 1231 | 3077 | 1166 | 1416 | 4071 | 1407 | 1358 | 4015 |  |
| Flt Permitted | 0.68 | 1.00 | 1.00 | 0.54 | 1.00 | 1.00 | 0.44 | 1.00 | 1.00 | 0.42 | 1.00 |  |
| Satd．Flow（perm） | 846 | 2625 | 1079 | 701 | 3077 | 1166 | 662 | 4071 | 1407 | 604 | 4015 |  |
| Peak－hour factor，PHF | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 |
| Adj．Flow（vph） | 12 | 59 | 30 | 64 | 121 | 64 | 161 | 569 | 431 | 238 | 498 | 33 |
| RTOR Reduction（vph） | 0 | 0 | 27 | 0 | 0 | 54 | 0 | 0 | 186 | 0 | ， | 0 |
| Lane Group Flow（vph） | 12 | 59 | 3 | 64 | 121 | 10 | 161 | 569 | 245 | 238 | 528 | 0 |
| Confl．Peds．（\＃／hr） |  |  |  |  |  |  |  |  | 1 | 1 |  |  |
| Heavy Vehicles（\％） | 50\％ | 36\％ | 48\％ | 45\％ | 16\％ | 37\％ | 19\％ | 26\％ | 12\％ | 24\％ | 25\％ | 50\％ |
| Turn Type | pm＋pt | NA | Perm | pm＋pt | NA | Perm | pm＋pt | NA | Perm | pm＋pt | NA |  |
| Protected Phases | 7 | 4 |  | 3 | 8 |  | 5 | 2 |  | 1 | 6 |  |
| Permitted Phases | 4 |  | 4 | 8 |  | 8 | 2 |  | 2 | 6 |  |  |
| Actuated Green，G（s） | 15.2 | 12.3 | 12.3 | 25.4 | 18.5 | 18.5 | 79.9 | 70.4 | 70.4 | 81.5 | 71.2 |  |
| Effective Green， g （s） | 15.2 | 12.3 | 12.3 | 25.4 | 18.5 | 18.5 | 79.9 | 70.4 | 70.4 | 81.5 | 71.2 |  |
| Actuated g／C Ratio | 0.12 | 0.10 | 0.10 | 0.21 | 0.15 | 0.15 | 0.65 | 0.57 | 0.57 | 0.66 | 0.58 |  |
| Clearance Time（s） | 4.0 | 6.6 | 6.6 | 4.0 | 6.6 | 6.6 | 4.0 | 6.9 | 6.9 | 4.0 | 6.9 |  |
| Vehicle Extension（s） | 3.0 | 5.0 | 5.0 | 3.0 | 5.0 | 5.0 | 3.0 | 5.0 | 5.0 | 3.0 | 5.0 |  |
| Lane Grp Cap（vph） | 112 | 261 | 107 | 183 | 460 | 174 | 485 | 2318 | 801 | 461 | 2312 |  |
| v／s Ratio Prot | 0.00 | 0.02 |  | c0．03 | 0.04 |  | 0.03 | 0.14 |  | c0．04 | 0.13 |  |
| v／s Ratio Perm | 0.01 |  | 0.00 | c0．05 |  | 0.01 | 0.19 |  | 0.17 | c0．30 |  |  |
| v／c Ratio | 0.11 | 0.23 | 0.03 | 0.35 | 0.26 | 0.06 | 0.33 | 0.25 | 0.31 | 0.52 | 0.23 |  |
| Uniform Delay，d1 | 48.0 | 51.3 | 50.3 | 41.2 | 46.5 | 45.1 | 8.7 | 13.3 | 13.9 | 8.7 | 12.8 |  |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |
| Incremental Delay，d2 | 0.4 | 0.9 | 0.2 | 1.2 | 0.6 | 0.3 | 0.4 | 0.3 | 1.0 | 1.0 | 0.2 |  |
| Delay（s） | 48.4 | 52.2 | 50.5 | 42.4 | 47.2 | 45.3 | 9.1 | 13.6 | 14.9 | 9.7 | 13.0 |  |
| Level of Service | D | D | D | D | D | D | A | B | B | A | B |  |
| Approach Delay（s） |  | 51.2 |  |  | 45.5 |  |  | 13.4 |  |  | 12.0 |  |
| Approach LOS |  | D |  |  | D |  |  | B |  |  | B |  |


| Intersection Summary |  |  |  |
| :--- | ---: | :--- | ---: |
| HCM 2000 Control Delay | 18.1 | HCM 2000 Level of Service | B |
| HCM 2000 Volume to Capacity ratio | 0.50 |  | 21.5 |
| Actuated Cycle Length（s） | 123.6 | Sum of lost time（s） | C |
| Intersection Capacity Utilization | $67.5 \%$ | ICU Level of Service |  |
| Analysis Period（min） | 15 |  |  |
| C Critical Lane Group |  |  |  |



Analysis Period (min) 15
c Critical Lane Group

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | \％ | $\hat{F}$ | 「 |  | ¢ |  |  | 快 |  | ${ }^{7}$ | 个性 |  |
| Traffic Volume（vph） | 497 | 20 | 638 | 20 | 0 | 26 | 0 | 997 | 27 | 24 | 962 | 0 |
| Future Volume（vph） | 497 | 20 | 638 | 20 | 0 | 26 | 0 | 997 | 27 | 24 | 962 | 0 |
| Ideal Flow（vphpl） | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width | 3.8 | 3.8 | 3.8 | 3.2 | 3.7 | 3.5 | 3.4 | 3.4 | 3.4 | 3.0 | 3.4 | 3.4 |
| Total Lost time（s） | 6.6 | 6.6 | 6.6 |  | 6.8 |  |  | 6.6 |  | 3.0 | 6.6 |  |
| Lane Util．Factor | 1.00 | 0.95 | 0.95 |  | 1.00 |  |  | 0.91 |  | 1.00 | 0.91 |  |
| Frpb，ped／bikes | 1.00 | 1.00 | 1.00 |  | 1.00 |  |  | 1.00 |  | 1.00 | 1.00 |  |
| Flpb，ped／bikes | 1.00 | 1.00 | 1.00 |  | 1.00 |  |  | 1.00 |  | 1.00 | 1.00 |  |
| Frt | 1.00 | 0.86 | 0.85 |  | 0.92 |  |  | 1.00 |  | 1.00 | 1.00 |  |
| Flt Protected | 0.95 | 1.00 | 1.00 |  | 0.98 |  |  | 1.00 |  | 0.95 | 1.00 |  |
| Satd．Flow（prot） | 1693 | 1474 | 1466 |  | 1532 |  |  | 4476 |  | 1440 | 4449 |  |
| Flt Permitted | 0.95 | 1.00 | 1.00 |  | 0.98 |  |  | 1.00 |  | 0.17 | 1.00 |  |
| Satd．Flow（perm） | 1693 | 1474 | 1466 |  | 1532 |  |  | 4476 |  | 261 | 4449 |  |
| Peak－hour factor，PHF | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 |
| Adj．Flow（vph） | 507 | 20 | 651 | 20 | 0 | 27 | 0 | 1017 | 28 | 24 | 982 | 0 |
| RTOR Reduction（vph） | 0 | 125 | 125 | 0 | 44 | 0 | 0 | 3 | 0 | 0 | 0 | 0 |
| Lane Group Flow（vph） | 507 | 214 | 207 | 0 | 3 | 0 | 0 | 1042 | 0 | 24 | 982 | 0 |
| Confl．Peds．（\＃／hr） |  |  |  |  |  |  |  |  | 3 | 3 |  |  |


| Heavy Vehicles（\％） | $9 \%$ | $16 \%$ | $7 \%$ | $15 \%$ | $0 \%$ | $12 \%$ | $0 \%$ | $13 \%$ | $4 \%$ | $17 \%$ | $14 \%$ | $0 \%$ |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Turn Type | Split | NA | Perm | Split | NA |  | NA | pm＋pt | NA |  |  |  |
| Protected Phases | 4 | 4 |  | 8 | 8 |  |  | 2 | 1 | 6 |  |  |


| Permitted Phases | 4 |  |  |  | 6 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Actuated Green，G（s） | 36.3 | 36.3 | 36.3 | 7.6 | 42.4 | 49.4 | 49.4 |
| Effective Green，g（s） | 36.3 | 36.3 | 36.3 | 7.6 | 42.4 | 49.4 | 49.4 |
| Actuated g／C Ratio | 0.32 | 0.32 | 0.32 | 0.07 | 0.37 | 0.44 | 0.44 |
| Clearance Time（s） | 6.6 | 6.6 | 6.6 | 6.8 | 6.6 | 3.0 | 6.6 |
| Vehicle Extension（s） | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap（vph） | 542 | 472 | 469 | 102 | 1675 | 155 | 1939 |
| v／s Ratio Prot | c0．30 | 0.15 |  | c0．00 | c0．23 | 0.01 | c0．22 |
| v／s Ratio Perm |  |  | 0.14 |  |  | 0.06 |  |
| v／c Ratio | 0.94 | 0.45 | 0.44 | 0.03 | 0.62 | 0.15 | 0.51 |
| Uniform Delay，d1 | 37.4 | 30.6 | 30.5 | 49.4 | 28.9 | 19.5 | 23.1 |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Incremental Delay，d2 | 23.6 | 0.7 | 0.7 | 0.1 | 1.8 | 0.5 | 0.9 |
| Delay（s） | 60.9 | 31.3 | 31.1 | 49.5 | 30.7 | 19.9 | 24.1 |


| Level of Service | E | C | C | D | C | B | C |
| :--- | :---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Approach Delay（s） |  | 44.0 |  | 49.5 | 30.7 | C | C |


| Intersection Summary |  |  |  |
| :--- | ---: | :--- | ---: |
| HCM 2000 Control Delay | 33.7 | HCM 2000 Level of Service | C |
| HCM 2000 Volume to Capacity ratio | 0.70 |  | 23.0 |
| Actuated Cycle Length（s） | 113.3 | Sum of lost time（s） | C |
| Intersection Capacity Utilization | $69.9 \%$ | ICU Level of Service |  |
| Analysis Period（min） | 15 |  |  |
| c Critical Lane Group |  |  |  |



Analysis Period (min) 15
c Critical Lane Group


Analysis Period (min) 15
c Critical Lane Group

Intersection: 1: Tremaine Road/Dublin Line \& Campbellville Road /James Snow Parkway

| Movement | EB | EB | WB | WB | NB | NB | SB |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | LT | $R$ | LT | $R$ | LT | R | LTR |
| Maximum Queue $(\mathrm{m})$ | 81.8 | 39.7 | 740.9 | 475.1 | 139.9 | 228.2 | 41.6 |
| Average Queue $(\mathrm{m})$ | 31.9 | 19.8 | 457.2 | 172.0 | 32.3 | 102.8 | 14.9 |
| 95th Queue $(\mathrm{m})$ | 60.7 | 33.4 | 875.7 | 455.5 | 106.5 | 226.2 | 30.0 |
| Link Distance $(\mathrm{m})$ | 622.3 | 622.3 | 1788.0 | 1788.0 | 764.7 | 764.7 | 71.8 |
| Upstream Blk Time $(\%)$ |  |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |  |  |
| Storage Bay Dist $(\mathrm{m})$ |  |  |  |  |  |  |  |
| Storage Blk Time $(\%)$ |  |  |  |  |  |  |  |

Intersection: 2: Regional Road 25 \& James Snow Parkway

| Movement | EB | EB | EB | EB | WB | WB | WB | WB | NB | NB | NB | NB |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Directions Served | L | T | T | R | L | T | T | R | L | T | T | T |
| Maximum Queue (m) | 21.5 | 27.6 | 25.6 | 21.8 | 48.0 | 37.1 | 37.1 | 24.4 | 48.4 | 55.2 | 46.2 | 43.1 |
| Average Queue (m) | 4.6 | 8.2 | 9.4 | 7.1 | 19.3 | 17.1 | 14.5 | 11.4 | 17.9 | 22.6 | 19.9 | 16.0 |
| 95th Queue (m) | 15.2 | 21.0 | 21.1 | 18.5 | 39.6 | 31.0 | 29.2 | 23.5 | 36.6 | 45.5 | 41.1 | 37.0 |
| Link Distance (m) |  | 1788.0 | 1788.0 |  |  | 728.6 | 728.6 |  |  | 744.3 | 744.3 | 744.3 |
| Upstream BIk Time (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |  |  |  |  |  |  |  |
| Storage Bay Dist (m) | 80.0 |  |  | 115.0 | 85.0 |  |  | 35.0 | 35.0 |  |  |  |
| Storage Blk Time (\%) |  |  |  |  |  |  | 1 |  | 1 | 3 |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |  | 0 |  | 2 | 4 |  |  |

Intersection: 2: Regional Road 25 \& James Snow Parkway

| Movement | NB | SB | SB | SB | SB |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Directions Served | R | L | T | T | TR |
| Maximum Queue $(\mathrm{m})$ | 65.9 | 73.1 | 44.9 | 49.9 | 44.6 |
| Average Queue $(\mathrm{m})$ | 22.0 | 28.9 | 17.7 | 19.6 | 12.1 |
| 95th Queue $(\mathrm{m})$ | 47.7 | 55.4 | 36.1 | 40.5 | 32.1 |
| Link Distance $(\mathrm{m})$ | 744.3 |  | 994.0 | 994.0 | 994.0 |
| Upstream Blk Time (\%) |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |
| Storage Bay Dist (m) |  | 75.0 |  |  |  |
| Storage Blk Time (\%) |  | 0 |  |  |  |
| Queuing Penalty (veh) |  | 0 |  |  |  |

Intersection: 3: Regional Road 25 \& Hwy 401 Westbound Off-Ramp

| Movement | WB | WB | NB | NB | NB | SB | SB | SB |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | L | L | T | T | T | T | T | T |
| Maximum Queue $(\mathrm{m})$ | 51.3 | 58.9 | 44.7 | 43.9 | 55.2 | 46.7 | 51.8 | 48.4 |
| Average Queue $(\mathrm{m})$ | 20.9 | 34.1 | 16.6 | 15.3 | 24.1 | 22.1 | 20.7 | 17.9 |
| 95th Queue $(\mathrm{m})$ | 43.0 | 51.7 | 34.3 | 33.5 | 45.8 | 37.0 | 40.2 | 38.0 |
| Link Distance $(\mathrm{m})$ |  |  | 339.1 | 339.1 | 339.1 | 744.3 | 744.3 | 744.3 |
| Upstream Blk Time (\%) |  |  |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |  |  |  |
| Storage Bay Dist (m) | 80.0 | 80.0 |  |  |  |  |  |  |
| Storage Blk Time (\%) |  | 0 |  |  |  |  |  |  |
| Queuing Penalty (veh) |  | 0 |  |  |  |  |  |  |

Intersection: 4: Regional Road 25 \& Hwy 401 Eastbound Off-Ramp/Carpool Lot

| Movement | EB | EB | EB | WB | NB | NB | NB | SB | SB | SB | SB |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Directions Served | L | TR | R | LTR | T | T | TR | L | T | T | T |
| Maximum Queue (m) | 160.6 | 222.2 | 127.0 | 28.2 | 108.8 | 94.1 | 58.3 | 23.1 | 68.1 | 74.7 | 78.8 |
| Average Queue (m) | 99.2 | 56.8 | 37.8 | 11.5 | 62.1 | 47.6 | 29.5 | 6.1 | 39.4 | 42.5 | 45.5 |
| 95th Queue (m) | 154.1 | 166.5 | 81.8 | 24.0 | 93.8 | 81.3 | 54.2 | 16.8 | 62.4 | 67.2 | 71.4 |
| Link Distance (m) |  | 434.1 |  | 85.8 | 183.3 | 183.3 | 183.3 |  | 339.1 | 339.1 | 339.1 |
| Upstream Blk Time (\%) |  | 0 |  |  |  |  |  |  |  |  |  |
| Queuing Penalty (veh) |  | 0 |  |  |  |  |  |  |  |  |  |
| Storage Bay Dist (m) | 130.0 |  | 130.0 |  |  |  |  | 30.0 |  |  |  |
| Storage Blk Time (\%) | 6 | 0 | 0 |  |  |  |  | 0 | 15 |  |  |
| Queuing Penalty (veh) | 37 | 2 | 0 |  |  |  |  | 0 | 4 |  |  |

Intersection: 5: Tremaine Road \& Hwy 401 Westbound Off-Ramp

| Movement | WB | WB | WB | NB | NB | SB | SB |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Directions Served | L | L | R | T | T | T | T |
| Maximum Queue (m) | 53.2 | 44.8 | 99.7 | 60.1 | 59.8 | 75.0 | 71.4 |
| Average Queue (m) | 29.3 | 20.0 | 49.9 | 27.1 | 23.1 | 41.2 | 40.8 |
| 95th Queue (m) | 47.5 | 38.4 | 83.1 | 47.5 | 45.3 | 65.7 | 62.3 |
| Link Distance (m) | 387.2 | 387.2 |  | 301.3 | 301.3 | 764.7 | 764.7 |
| Upstream Blk Time (\%) |  |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |
| Storage Blk Time (\%) |  |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |  |  |

Intersection: 6: Tremaine Road \& Hwy 401 Eastbound Off-Ramp/Carpool Lot

| Movement | EB | EB | EB | WB | WB | NB | NB | SB | SB | SB |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Directions Served | L | TR | R | L | R | T | TR | L | T | T |
| Maximum Queue (m) | 41.6 | 24.5 | 15.6 | 23.0 | 20.6 | 85.2 | 73.7 | 24.9 | 64.4 | 66.8 |
| Average Queue (m) | 17.1 | 10.7 | 4.7 | 7.3 | 5.1 | 35.6 | 23.4 | 8.2 | 27.1 | 30.5 |
| 95th Queue (m) | 34.2 | 19.6 | 13.1 | 19.0 | 14.8 | 67.3 | 55.6 | 19.5 | 56.2 | 58.3 |
| Link Distance (m) |  | 455.1 |  | 125.3 |  | 250.9 | 250.9 |  | 301.3 | 301.3 |
| Upstream BIk Time (\%) |  |  |  |  |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |  |  |  |  |  |
| Storage Bay Dist (m) | 300.0 |  | 165.0 |  | 20.0 |  |  | 120.0 |  |  |
| Storage Blk Time (\%) |  |  |  | 3 | 0 |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  | 1 | 0 |  |  |  |  |  |

## Network Summary

Network wide Queuing Penalty: 50

|  | 4 |  |  | $\checkmark$ |  | 4 | 4 | $\dagger$ |  |  | $\downarrow$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Right Turn Channelized |  |  |  |  |  |  |  |  |  |  |  |  |
| Traffic Volume (veh/h) | 4 | 299 | 222 | 1259 | 446 | 69 | 172 | 0 | 690 | 74 | 0 | 10 |
| Future Volume (veh/h) | 4 | 299 | 222 | 1259 | 446 | 69 | 172 | 0 | 690 | 74 | 0 | 10 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Hourly flow rate (vph) | 4 | 325 | 241 | 1368 | 485 | 75 | 187 | 0 | 750 | 80 | 0 | 11 |
| Approach Volume (veh/h) |  | 570 |  |  | 1928 |  |  | 937 |  |  | 91 |  |
| Crossing Volume (veh/h) |  | 1448\# |  |  | 191 |  |  | 409 |  |  | 2040\# |  |
| High Capacity (veh/h) |  | 429 |  |  | 1193 |  |  | 1004 |  |  | 259 |  |
| High v/c (veh/h) |  | 1.33 |  |  | 1.62 |  |  | 0.93 |  |  | 0.35 |  |
| Low Capacity (veh/h) |  | 319 |  |  | 987 |  |  | 817 |  |  | 182 |  |
| Low v/c (veh/h) |  | 1.78 |  |  | 1.95 |  |  | 1.15 |  |  | 0.50 |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Maximum v/c High |  |  | 1.62 |  |  |  |  |  |  |  |  |  |
| Maximum v/c Low |  |  | 1.95 |  |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization |  |  | 130.6\% |  | CU Level | Service |  |  | H |  |  |  |
| \# Crossing flow exceeds 1200, method is not applicable |  |  |  |  |  |  |  |  |  |  |  |  |


| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | \％ | 个 $\uparrow$ | 「 | \％ | 个 $\uparrow$ | 「 | \％ | 中4亩 | 「 | \％ | 快 ${ }^{\text {d }}$ |  |
| Traffic Volume（vph） | 30 | 177 | 211 | 175 | 102 | 218 | 126 | 875 | 143 | 132 | 492 | 5 |
| Future Volume（vph） | 30 | 177 | 211 | 175 | 102 | 218 | 126 | 875 | 143 | 132 | 492 | 5 |
| Ideal Flow（vphpl） | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.0 | 3.5 | 3.5 | 3.0 | 3.5 | 3.5 |
| Total Lost time（s） | 4.0 | 6.6 | 6.6 | 4.0 | 6.6 | 6.6 | 4.0 | 6.9 | 6.9 | 4.0 | 6.9 |  |
| Lane Util．Factor | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.91 | 1.00 | 1.00 | 0.91 |  |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 |  |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |  |
| Satd．Flow（prot） | 1487 | 3336 | 1365 | 1513 | 2746 | 1365 | 1154 | 4347 | 1521 | 1370 | 4217 |  |
| Flt Permitted | 0.68 | 1.00 | 1.00 | 0.50 | 1.00 | 1.00 | 0.42 | 1.00 | 1.00 | 0.25 | 1.00 |  |
| Satd．Flow（perm） | 1066 | 3336 | 1365 | 791 | 2746 | 1365 | 516 | 4347 | 1521 | 356 | 4217 |  |
| Peak－hour factor，PHF | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 |
| Adj．Flow（vph） | 33 | 197 | 234 | 194 | 113 | 242 | 140 | 972 | 159 | 147 | 547 | 6 |
| RTOR Reduction（vph） | 0 | 0 | 203 | ， | 0 | 192 | 0 | 0 | 76 | 0 | ， | 0 |
| Lane Group Flow（vph） | 33 | 197 | 31 | 194 | 113 | 50 | 140 | 972 | 83 | 147 | 553 | 0 |
| Heavy Vehicles（\％） | 20\％ | 7\％ | 17\％ | 18\％ | 30\％ | 17\％ | 46\％ | 18\％ | 5\％ | 23\％ | 21\％ | 60\％ |
| Turn Type | pm＋pt | NA | Perm | pm＋pt | NA | Perm | pm＋pt | NA | Perm | pm＋pt | NA |  |
| Protected Phases | 7 | 4 |  | 3 | 8 |  | 5 | 2 |  | 1 | 6 |  |
| Permitted Phases | 4 |  | 4 | 8 |  | 8 | 2 |  | 2 | 6 |  |  |
| Actuated Green，G（s） | 22.9 | 17.8 | 17.8 | 37.1 | 28.0 | 28.0 | 80.7 | 70.4 | 70.4 | 80.1 | 70.1 |  |
| Effective Green， $\mathrm{g}(\mathrm{s})$ | 22.9 | 17.8 | 17.8 | 37.1 | 28.0 | 28.0 | 80.7 | 70.4 | 70.4 | 80.1 | 70.1 |  |
| Actuated g／C Ratio | 0.17 | 0.13 | 0.13 | 0.27 | 0.21 | 0.21 | 0.60 | 0.52 | 0.52 | 0.59 | 0.52 |  |
| Clearance Time（s） | 4.0 | 6.6 | 6.6 | 4.0 | 6.6 | 6.6 | 4.0 | 6.9 | 6.9 | 4.0 | 6.9 |  |
| Vehicle Extension（s） | 3.0 | 5.0 | 5.0 | 3.0 | 5.0 | 5.0 | 3.0 | 5.0 | 5.0 | 3.0 | 5.0 |  |
| Lane Grp Cap（vph） | 196 | 439 | 179 | 299 | 569 | 283 | 357 | 2266 | 793 | 286 | 2189 |  |
| v／s Ratio Prot | 0.01 | 0.06 |  | c0．07 | 0.04 |  | 0.03 | 0.22 |  | c0．04 | 0.13 |  |
| v／s Ratio Perm | 0.02 |  | 0.02 | c0．10 |  | 0.04 | 0.20 |  | 0.05 | c0．27 |  |  |
| v／c Ratio | 0.17 | 0.45 | 0.17 | 0.65 | 0.20 | 0.18 | 0.39 | 0.43 | 0.10 | 0.51 | 0.25 |  |
| Uniform Delay，d1 | 47.6 | 54.1 | 52.1 | 40.8 | 44.2 | 44.0 | 12.4 | 19.9 | 16.3 | 12.9 | 18.0 |  |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |
| Incremental Delay，d2 | 0.4 | 1.5 | 1.0 | 4.8 | 0.4 | 0.6 | 0.7 | 0.6 | 0.3 | 1.6 | 0.3 |  |
| Delay（s） | 48.0 | 55.6 | 53.0 | 45.6 | 44.6 | 44.7 | 13.2 | 20.5 | 16.6 | 14.5 | 18.2 |  |
| Level of Service | D | E | D | D | D | D | B | C | B | B | B |  |
| Approach Delay（s） |  | 53.8 |  |  | 45.0 |  |  | 19.2 |  |  | 17.4 |  |
| Approach LOS |  | D |  |  | D |  |  | B |  |  | B |  |


| Intersection Summary |  |  |  |
| :--- | ---: | :--- | ---: |
| HCM 2000 Control Delay | 28.9 | HCM 2000 Level of Service | C |
| HCM 2000 Volume to Capacity ratio | 0.57 |  | 21.5 |
| Actuated Cycle Length（s） | 135.0 | Sum of lost time（s） | B |
| Intersection Capacity Utilization | $60.2 \%$ | ICU Level of Service |  |

C Critical Lane Group

|  |  | $4$ |  |  | $1$ | $\frac{1}{\square}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |  |
| Lane Configurations | ${ }^{7 * 1}$ | F | 444 |  |  | 444 |  |
| Traffic Volume (vph) | 342 | 0 | 1018 | 0 | 0 | 1243 |  |
| Future Volume (vph) | 342 | 0 | 1018 | 0 | 0 | 1243 |  |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |  |
| Lane Width | 3.8 | 3.8 | 3.4 | 3.4 | 3.4 | 3.4 |  |
| Total Lost time (s) | 6.2 |  | 6.4 |  |  | 6.4 |  |
| Lane Util. Factor | 0.97 |  | 0.91 |  |  | 0.91 |  |
| Frt | 1.00 |  | 1.00 |  |  | 1.00 |  |
| Flt Protected | 0.95 |  | 1.00 |  |  | 1.00 |  |
| Satd. Flow (prot) | 3314 |  | 4569 |  |  | 4696 |  |
| Flt Permitted | 0.95 |  | 1.00 |  |  | 1.00 |  |
| Satd. Flow (perm) | 3314 |  | 4569 |  |  | 4696 |  |
| Peak-hour factor, PHF | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 |  |
| Adj. Flow (vph) | 364 | 0 | 1083 | 0 | 0 | 1322 |  |
| RTOR Reduction (vph) | 0 | 0 | 0 | 0 | 0 | 0 |  |
| Lane Group Flow (vph) | 364 | 0 | 1083 | 0 | 0 | 1322 |  |
| Heavy Vehicles (\%) | 8\% | 0\% | 11\% | 0\% | 0\% | 8\% |  |
| Turn Type | Prot | Perm | NA |  |  | NA |  |
| Protected Phases | 8 |  | 2 |  |  | 6 |  |
| Permitted Phases |  | 8 |  |  |  |  |  |
| Actuated Green, G (s) | 12.2 |  | 37.0 |  |  | 37.0 |  |
| Effective Green, g (s) | 12.2 |  | 37.0 |  |  | 37.0 |  |
| Actuated g/C Ratio | 0.20 |  | 0.60 |  |  | 0.60 |  |
| Clearance Time (s) | 6.2 |  | 6.4 |  |  | 6.4 |  |
| Vehicle Extension (s) | 3.0 |  | 4.4 |  |  | 4.4 |  |
| Lane Grp Cap (vph) | 654 |  | 2735 |  |  | 2811 |  |
| v/s Ratio Prot | c0.11 |  | 0.24 |  |  | c0.28 |  |
| v/s Ratio Perm |  |  |  |  |  |  |  |
| v/c Ratio | 0.56 |  | 0.40 |  |  | 0.47 |  |
| Uniform Delay, d1 | 22.4 |  | 6.5 |  |  | 6.9 |  |
| Progression Factor | 1.00 |  | 1.00 |  |  | 1.00 |  |
| Incremental Delay, d2 | 1.0 |  | 0.4 |  |  | 0.6 |  |
| Delay (s) | 23.4 |  | 7.0 |  |  | 7.5 |  |
| Level of Service | C |  | A |  |  | A |  |
| Approach Delay (s) | 23.4 |  | 7.0 |  |  | 7.5 |  |
| Approach LOS | C |  | A |  |  | A |  |
| Intersection Summary |  |  |  |  |  |  |  |
| HCM 2000 Control Delay |  |  | 9.4 |  | HCM 2000 | evel of Service | A |
| HCM 2000 Volume to Capacity ratio |  |  | 0.49 |  |  |  |  |
| Actuated Cycle Length (s) |  |  | 61.8 |  | Sum of los | ime (s) | 12.6 |
| Intersection Capacity Utilization |  |  | 44.3\% |  | CU Level | Service | A |
| Analysis Period (min) |  |  | 15 |  |  |  |  |

C Critical Lane Group


Analysis Period (min) 15
c Critical Lane Group


## c Critical Lane Group



Analysis Period (min) 15
c Critical Lane Group

Intersection: 1: Tremaine Road/Dublin Line \& Campbellville Road/James Snow Parkway

| Movement | EB | EB | WB | WB | NB | NB | SB |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | LT | R | LT | R | LT | R | LTR |
| Maximum Queue $(\mathrm{m})$ | 71.6 | 29.5 | 940.3 | 935.3 | 89.6 | 160.7 | 70.5 |
| Average Queue $(\mathrm{m})$ | 27.1 | 14.1 | 917.2 | 898.8 | 19.8 | 79.3 | 23.5 |
| 95th Queue $(\mathrm{m})$ | 52.0 | 24.0 | 933.2 | 1032.6 | 79.2 | 168.3 | 53.1 |
| Link Distance $(\mathrm{m})$ | 622.3 | 622.3 | 1788.0 | 1788.0 | 764.7 | 764.7 | 71.8 |
| Upstream BIk Time (\%) |  |  |  |  |  |  | 3 |
| Queuing Penalty (veh) |  |  |  |  |  |  | 0 |

Storage Bay Dist (m)
Storage Blk Time (\%)
Queuing Penalty (veh)
Intersection: 2: Regional Road 25 \& James Snow Parkway

| Movement | EB | EB | EB | EB | WB | WB | WB | WB | NB | NB | NB | NB |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Directions Served | L | T | T | R | L | T | T | R | L | T | T | T |
| Maximum Queue (m) | 26.2 | 39.5 | 41.2 | 40.4 | 84.4 | 38.5 | 40.4 | 58.3 | 63.5 | 104.4 | 69.8 | 73.3 |
| Average Queue (m) | 6.6 | 19.0 | 22.5 | 20.6 | 45.2 | 14.8 | 13.0 | 25.5 | 23.8 | 38.8 | 39.1 | 38.0 |
| 95th Queue (m) | 18.5 | 35.7 | 35.6 | 34.5 | 74.9 | 30.3 | 29.9 | 46.4 | 48.0 | 81.3 | 65.6 | 67.5 |
| Link Distance (m) |  | 1788.0 | 1788.0 |  |  | 728.6 | 728.6 |  |  | 744.3 | 744.3 | 744.3 |
| Upstream Blk Time (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |  |  |  |  |  |  |  |
| Storage Bay Dist (m) | 80.0 |  |  | 115.0 | 85.0 |  |  | 35.0 | 35.0 |  |  |  |
| Storage Blk Time (\%) |  |  |  |  | 0 |  | 1 | 4 | 3 | 9 |  |  |
| Queuing Penalty (veh) |  |  |  |  | 0 |  | 2 | 2 | 10 | 11 |  |  |

Intersection: 2: Regional Road 25 \& James Snow Parkway

| Movement | NB | SB | SB | SB | SB |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Directions Served | R | L | T | T | TR |
| Maximum Queue (m) | 29.2 | 55.6 | 49.0 | 51.2 | 45.4 |
| Average Queue $(\mathrm{m})$ | 7.5 | 21.2 | 23.6 | 25.2 | 13.5 |
| 95th Queue $(\mathrm{m})$ | 19.9 | 41.7 | 42.3 | 44.1 | 33.0 |
| Link Distance $(\mathrm{m})$ | 744.3 |  | 994.0 | 994.0 | 994.0 |
| Upstream Blk Time (\%) |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |
| Storage Bay Dist (m) |  | 75.0 |  |  |  |
| Storage Blk Time (\%) |  | 0 |  |  |  |
| Queuing Penalty (veh) |  | 0 |  |  |  |

Intersection: 3: Regional Road 25 \& Hwy 401 Westbound Off-Ramp

| Movement | WB | WB | NB | NB | NB | SB | SB | SB |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | L | L | T | T | T | T | T | T |
| Maximum Queue $(\mathrm{m})$ | 44.8 | 54.0 | 57.7 | 56.2 | 57.0 | 50.5 | 55.8 | 51.5 |
| Average Queue $(\mathrm{m})$ | 18.5 | 32.0 | 26.7 | 23.9 | 22.5 | 24.2 | 25.5 | 23.0 |
| 95th Queue $(\mathrm{m})$ | 37.8 | 48.3 | 48.7 | 45.6 | 45.9 | 41.9 | 46.3 | 42.2 |
| Link Distance $(\mathrm{m})$ |  |  | 339.1 | 339.1 | 339.1 | 744.3 | 744.3 | 744.3 |
| Upstream Blk Time (\%) |  |  |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |  |  |  |
| Storage Bay Dist (m) | 80.0 | 80.0 |  |  |  |  |  |  |
| Storage Blk Time (\%) |  |  |  |  |  |  |  |  |

Intersection: 4: Regional Road 25 \& Hwy 401 Eastbound Off-Ramp/Carpool Lot

| Movement | EB | EB | EB | WB | NB | NB | NB | SB | SB | SB | SB |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Directions Served | L | TR | R | LTR | T | T | TR | L | T | T | T |
| Maximum Queue (m) | 74.9 | 58.0 | 54.8 | 34.0 | 122.4 | 106.8 | 68.6 | 20.1 | 53.9 | 64.1 | 62.9 |
| Average Queue (m) | 30.8 | 30.0 | 24.1 | 12.2 | 65.0 | 51.0 | 27.6 | 6.2 | 28.5 | 31.4 | 35.4 |
| 95th Queue (m) | 58.2 | 49.0 | 44.1 | 25.3 | 104.7 | 90.3 | 57.9 | 16.1 | 48.6 | 54.7 | 56.6 |
| Link Distance (m) |  | 434.1 |  | 85.8 | 183.3 | 183.3 | 183.3 |  | 339.1 | 339.1 | 339.1 |
| Upstream Blk Time (\%) |  |  |  |  |  |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |  |  |  |  |  |  |
| Storage Bay Dist (m) | 130.0 |  | 130.0 |  |  |  |  | 30.0 |  |  |  |
| Storage Blk Time (\%) |  |  |  |  |  |  |  | 0 | 6 |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |  |  | 0 | 1 |  |  |

Intersection: 5: Tremaine Road \& Hwy 401 Westbound Off-Ramp

| Movement | WB | WB | WB | NB | NB | SB | SB |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Directions Served | L | L | R | T | T | T | T |
| Maximum Queue (m) | 84.4 | 74.6 | 37.7 | 71.2 | 78.3 | 52.4 | 51.4 |
| Average Queue (m) | 50.1 | 43.9 | 15.9 | 38.2 | 39.1 | 27.3 | 27.1 |
| 95th Queue (m) | 73.7 | 66.9 | 30.7 | 64.8 | 66.9 | 45.6 | 44.0 |
| Link Distance (m) | 387.2 | 387.2 |  | 301.3 | 301.3 | 764.7 | 764.7 |
| Upstream Blk Time (\%) |  |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |
| Storage Blk Time (\%) |  |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |  |  |

Intersection: 6: Tremaine Road \& Hwy 401 Eastbound Off-Ramp/Carpool Lot

| Movement | EB | EB | EB | WB | WB | NB | NB | SB | SB | SB |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Directions Served | L | TR | R | L | R | T | TR | L | T | T |
| Maximum Queue (m) | 65.0 | 60.6 | 58.8 | 30.7 | 28.5 | 95.8 | 86.7 | 18.9 | 98.0 | 101.0 |
| Average Queue (m) | 30.7 | 33.3 | 29.0 | 11.9 | 8.8 | 56.7 | 43.1 | 4.8 | 52.5 | 57.5 |
| 95th Queue (m) | 57.0 | 53.7 | 50.8 | 24.5 | 20.3 | 87.4 | 77.8 | 14.3 | 86.7 | 90.3 |
| Link Distance (m) |  | 455.1 |  | 125.3 |  | 250.9 | 250.9 |  | 301.3 | 301.3 |
| Upstream Blk Time (\%) |  |  |  |  |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |  |  |  |  |  |
| Storage Bay Dist (m) | 300.0 |  | 165.0 |  | 20.0 |  |  | 120.0 |  |  |
| Storage Blk Time (\%) |  |  |  | 5 | 1 |  |  |  | 0 |  |
| Queuing Penalty (veh) |  |  |  | 2 | 0 |  |  |  | 0 |  |

## Network Summary

Network wide Queuing Penalty: 30


| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Right Turn Channelized |  |  |  |  |  |  |  |  |  |  |  |  |
| Traffic Volume (veh/h) | 4 | 299 | 222 | 1259 | 446 | 18 | 172 | 51 | 690 | 23 | 51 | 10 |
| Future Volume (veh/h) | 4 | 299 | 222 | 1259 | 446 | 18 | 172 | 51 | 690 | 23 | 51 | 10 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Hourly flow rate (vph) | 4 | 325 | 241 | 1368 | 485 | 20 | 187 | 55 | 750 | 25 | 55 | 11 |
| Approach Volume (veh/h) |  | 570 |  |  | 1873 |  |  | 992 |  |  | 91 |  |
| Crossing Volume (veh/h) |  | 1448\# |  |  | 246 |  |  | 354 |  |  | 2040\# |  |
| High Capacity (veh/h) |  | 429 |  |  | 1142 |  |  | 1049 |  |  | 259 |  |
| High v/c (veh/h) |  | 1.33 |  |  | 1.64 |  |  | 0.95 |  |  | 0.35 |  |
| Low Capacity (veh/h) |  | 319 |  |  | 941 |  |  | 857 |  |  | 182 |  |
| Low v/c (veh/h) |  | 1.78 |  |  | 1.99 |  |  | 1.16 |  |  | 0.50 |  |

Intersection Summary

| Maximum v/c High | 1.64 |  |  |
| :--- | ---: | :--- | :--- |
| Maximum v/c Low | 1.99 |  | H |
| Intersection Capacity Utilization | $127.2 \%$ | ICU Level of Service |  |
| $\#$ Crossing flow exceeds 1200, method is not applicable |  |  |  |


| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | ${ }^{4}$ | 个4 | 「 | \％ | 个4 | 「 | \％ | 个中4 | 「 | ${ }_{1}$ | 个中t |  |
| Traffic Volume（vph） | 30 | 177 | 160 | 175 | 102 | 218 | 75 | 875 | 143 | 132 | 492 | 5 |
| Future Volume（vph） | 30 | 177 | 160 | 175 | 102 | 218 | 75 | 875 | 143 | 132 | 492 | 5 |
| Ideal Flow（vphpl） | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.0 | 3.5 | 3.5 | 3.0 | 3.5 | 3.5 |
| Total Lost time（s） | 4.0 | 6.6 | 6.6 | 4.0 | 6.6 | 6.6 | 4.0 | 6.9 | 6.9 | 4.0 | 6.9 |  |
| Lane Util．Factor | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.91 | 1.00 | 1.00 | 0.91 |  |
| Frpb，ped／bikes | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.99 | 1.00 | 1.00 |  |
| Flpb，ped／bikes | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 |  |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |  |
| Satd．Flow（prot） | 1487 | 3336 | 1365 | 1513 | 2746 | 1365 | 1154 | 4347 | 1499 | 1370 | 4217 |  |
| Flt Permitted | 0.68 | 1.00 | 1.00 | 0.49 | 1.00 | 1.00 | 0.43 | 1.00 | 1.00 | 0.24 | 1.00 |  |
| Satd．Flow（perm） | 1066 | 3336 | 1365 | 788 | 2746 | 1365 | 527 | 4347 | 1499 | 350 | 4217 |  |
| Peak－hour factor，PHF | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 |
| Adj．Flow（vph） | 33 | 197 | 178 | 194 | 113 | 242 | 83 | 972 | 159 | 147 | 547 | 6 |
| RTOR Reduction（vph） | 0 | 0 | 155 | 0 | 0 | 192 | 0 | 0 | 76 | 0 | 0 | 0 |
| Lane Group Flow（vph） | 33 | 197 | 23 | 194 | 113 | 50 | 83 | 972 | 83 | 147 | 553 | 0 |
| Confl．Peds．（\＃／hr） |  |  |  |  |  |  |  |  | 2 | 2 |  |  |


| Heavy Vehicles（\％） | $20 \%$ | $7 \%$ | $17 \%$ | $18 \%$ | $30 \%$ | $17 \%$ | $46 \%$ | $18 \%$ | $5 \%$ | $23 \%$ | $21 \%$ | $60 \%$ |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Turn Type | $\mathrm{pm}+\mathrm{pt}$ | NA | Perm | $\mathrm{pm}+\mathrm{pt}$ | NA | Perm | $\mathrm{pm}+\mathrm{pt}$ | NA | Perm | $\mathrm{pm}+\mathrm{pt}$ | NA |  |
| Protected Phases | 7 | 4 |  | 3 | 8 |  | 5 | 2 |  | 1 | 6 |  |


| Permitted Phases | 4 |  | 4 | 8 |  | 8 | 2 |  | 2 | 6 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Actuated Green，G（s） | 22.5 | 17.4 | 17.4 | 36.7 | 27.6 | 27.6 | 79.1 | 70.1 | 70.1 | 81.1 | 71.1 |
| Effective Green， g （s） | 22.5 | 17.4 | 17.4 | 36.7 | 27.6 | 27.6 | 79.1 | 70.1 | 70.1 | 81.1 | 71.1 |
| Actuated g／C Ratio | 0.17 | 0.13 | 0.13 | 0.27 | 0.21 | 0.21 | 0.59 | 0.52 | 0.52 | 0.60 | 0.53 |
| Clearance Time（s） | 4.0 | 6.6 | 6.6 | 4.0 | 6.6 | 6.6 | 4.0 | 6.9 | 6.9 | 4.0 | 6.9 |
| Vehicle Extension（s） | 3.0 | 5.0 | 5.0 | 3.0 | 5.0 | 5.0 | 3.0 | 5.0 | 5.0 | 3.0 | 5.0 |
| Lane Grp Cap（vph） | 194 | 432 | 176 | 297 | 564 | 280 | 352 | 2268 | 782 | 287 | 2232 |
| v／s Ratio Prot | 0.01 | 0.06 |  | c0．07 | 0.04 |  | 0.02 | 0.22 |  | c0．04 | 0.13 |
| v／s Ratio Perm | 0.02 |  | 0.02 | c0．10 |  | 0.04 | 0.12 |  | 0.06 | c0． 27 |  |
| v／c Ratio | 0.17 | 0.46 | 0.13 | 0.65 | 0.20 | 0.18 | 0.24 | 0.43 | 0.11 | 0.51 | 0.25 |
| Uniform Delay，d1 | 47.6 | 54.1 | 51.8 | 40.8 | 44.2 | 44.0 | 12.2 | 19.8 | 16.2 | 12.4 | 17.1 |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Incremental Delay，d2 | 0.4 | 1.6 | 0.7 | 5.1 | 0.4 | 0.6 | 0.3 | 0.6 | 0.3 | 1.5 | 0.3 |
| Delay（s） | 48.0 | 55.7 | 52.5 | 45.9 | 44.6 | 44.6 | 12.6 | 20.4 | 16.5 | 13.9 | 17.4 |


| Level of Service | D | E | D | D | D | D | B | C | B | B | B |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Approach Delay（s） |  | 53.7 |  |  | 45.1 |  |  | 19.3 |  |  | 16.7 |
| Approach LOS |  | D |  |  | D |  |  | B |  | B |  |


| Intersection Summary |  |  |  |
| :--- | ---: | :--- | ---: |
| HCM 2000 Control Delay | 28.5 | HCM 2000 Level of Service | C |
| HCM 2000 Volume to Capacity ratio | 0.58 |  | 21.5 |
| Actuated Cycle Length（s） | 134.3 | Sum of lost time（s） | D |
| Intersection Capacity Utilization | $73.3 \%$ | ICU Level of Service |  |
| Analysis Period（min） | 15 |  |  |
| c Critical Lane Group |  |  |  |



Analysis Period (min)
15
c Critical Lane Group

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | ${ }^{*}$ | $\hat{\beta}$ | F |  | \$ |  |  | 楽 |  | \% | 4个4 |  |
| Traffic Volume (vph) | 121 | 18 | 451 | 34 | 0 | 22 | 0 | 1345 | 23 | 25 | 992 | 0 |
| Future Volume (vph) | 121 | 18 | 451 | 34 | 0 | 22 | 0 | 1345 | 23 | 25 | 992 | 0 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width | 3.8 | 3.8 | 3.8 | 3.2 | 3.7 | 3.5 | 3.4 | 3.4 | 3.4 | 3.0 | 3.4 | 3.4 |
| Total Lost time (s) | 6.6 | 6.6 | 6.6 |  | 6.8 |  |  | 6.6 |  | 3.0 | 6.6 |  |
| Lane Util. Factor | 1.00 | 0.95 | 0.95 |  | 1.00 |  |  | 0.91 |  | 1.00 | 0.91 |  |
| Frpb, ped/bikes | 1.00 | 0.99 | 0.99 |  | 1.00 |  |  | 1.00 |  | 1.00 | 1.00 |  |
| Flpb, ped/bikes | 1.00 | 1.00 | 1.00 |  | 1.00 |  |  | 1.00 |  | 1.00 | 1.00 |  |
| Frt | 1.00 | 0.86 | 0.85 |  | 0.95 |  |  | 1.00 |  | 1.00 | 1.00 |  |
| Flt Protected | 0.95 | 1.00 | 1.00 |  | 0.97 |  |  | 1.00 |  | 0.95 | 1.00 |  |
| Satd. Flow (prot) | 1398 | 1432 | 1420 |  | 1624 |  |  | 4774 |  | 1452 | 4785 |  |
| Flt Permitted | 0.95 | 1.00 | 1.00 |  | 0.97 |  |  | 1.00 |  | 0.10 | 1.00 |  |
| Satd. Flow (perm) | 1398 | 1432 | 1420 |  | 1624 |  |  | 4774 |  | 147 | 4785 |  |
| Peak-hour factor, PHF | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 |
| Adj. Flow (vph) | 134 | 20 | 501 | 38 | 0 | 24 | 0 | 1494 | 26 | 28 | 1102 | 0 |
| RTOR Reduction (vph) | 0 | 186 | 186 | 0 | 57 | 0 | 0 | 1 | 0 | 0 | 0 | 0 |
| Lane Group Flow (vph) | 134 | 74 | 75 | 0 | 5 | 0 | 0 | 1519 | 0 | 28 | 1102 | 0 |
| Confl. Peds. (\#/hr) |  |  | 1 | 1 |  |  |  |  |  |  |  |  |


| Heavy Vehicles (\%) | 32\% | 18\% | 9\% | 3\% | 0\% | 18\% | 0\% | 6\% | 4\% | 16\% | 6\% | 0\% |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Turn Type | Split | NA | Perm | Split | NA |  |  | NA |  | pm+pt | NA |  |
| Protected Phases | , | 4 |  | 8 | 8 |  |  | 2 |  | 1 | 6 |  |
| Permitted Phases |  |  | 4 |  |  |  |  |  |  | 6 |  |  |
| Actuated Green, G (s) | 16.2 | 16.2 | 16.2 |  | 7.6 |  |  | 44.0 |  | 49.7 | 49.7 |  |
| Effective Green, g (s) | 16.2 | 16.2 | 16.2 |  | 7.6 |  |  | 44.0 |  | 49.7 | 49.7 |  |
| Actuated g/C Ratio | 0.17 | 0.17 | 0.17 |  | 0.08 |  |  | 0.47 |  | 0.53 | 0.53 |  |
| Clearance Time (s) | 6.6 | 6.6 | 6.6 |  | 6.8 |  |  | 6.6 |  | 3.0 | 6.6 |  |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 |  | 3.0 |  |  | 3.0 |  | 3.0 | 3.0 |  |
| Lane Grp Cap (vph) | 242 | 248 | 246 |  | 132 |  |  | 2246 |  | 115 | 2543 |  |
| v/s Ratio Prot | c0.10 | 0.05 |  |  | c0.00 |  |  | c0.32 |  | 0.01 | c0.23 |  |
| v/s Ratio Perm |  |  | 0.05 |  |  |  |  |  |  | 0.12 |  |  |
| v/c Ratio | 0.55 | 0.30 | 0.30 |  | 0.04 |  |  | 0.68 |  | 0.24 | 0.43 |  |
| Uniform Delay, d1 | 35.3 | 33.7 | 33.7 |  | 39.6 |  |  | 19.2 |  | 12.5 | 13.3 |  |
| Progression Factor | 1.00 | 1.00 | 1.00 |  | 1.00 |  |  | 1.00 |  | 1.00 | 1.00 |  |
| Incremental Delay, d2 | 2.7 | 0.7 | 0.7 |  | 0.1 |  |  | 1.7 |  | 1.1 | 0.5 |  |
| Delay (s) | 38.1 | 34.4 | 34.4 |  | 39.7 |  |  | 20.9 |  | 13.6 | 13.9 |  |
| Level of Service | D | C | C |  | D |  |  | C |  | B | B |  |
| Approach Delay (s) |  | 35.2 |  |  | 39.7 |  |  | 20.9 |  |  | 13.9 |  |
| Approach LOS |  | D |  |  | D |  |  | C |  |  | B |  |


| Intersection Summary |  |  | C |
| :--- | ---: | :--- | ---: |
| HCM 2000 Control Delay | 21.6 | HCM 2000 Level of Service |  |
| HCM 2000 Volume to Capacity ratio | 0.57 |  | 23.0 |
| Actuated Cycle Length (s) | 93.5 | Sum of lost time (s) | B |
| Intersection Capacity Utilization | $62.9 \%$ | ICU Level of Service |  |

C Critical Lane Group


Analysis Period (min) 15
c Critical Lane Group


Analysis Period (min) 15
c Critical Lane Group

Intersection: 1: Tremaine Road/Dublin Line \& Campbellville Road /James Snow Parkway

| Movement | EB | EB | WB | WB | NB | NB | SB |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | LT | R | LT | R | LT | R | LTR |
| Maximum Queue $(m)$ | 60.4 | 29.9 | 952.6 | 928.4 | 71.0 | 151.1 | 26.4 |
| Average Queue $(\mathrm{m})$ | 26.4 | 14.2 | 920.8 | 888.0 | 18.2 | 67.1 | 8.8 |
| 95th Queue $(\mathrm{m})$ | 47.1 | 24.4 | 940.8 | 1040.0 | 50.1 | 135.5 | 20.5 |
| Link Distance $(\mathrm{m})$ | 622.3 | 622.3 | 1788.0 | 1788.0 | 764.7 | 764.7 | 71.8 |
| Upstream Blk Time $(\%)$ |  |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |  |  |
| Storage Bay Dist $(\mathrm{m})$ |  |  |  |  |  |  |  | | Storage Blk Time $(\%)$ |
| :--- |
| Queuing Penalty (veh) |

Intersection: 2: Regional Road 25 \& James Snow Parkway

| Movement | EB | EB | EB | EB | WB | WB | WB | WB | NB | NB | NB | NB |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Directions Served | L | T | T | R | L | T | T | R | L | T | T | T |
| Maximum Queue (m) | 29.1 | 39.0 | 38.5 | 32.3 | 83.0 | 37.8 | 48.9 | 66.9 | 46.8 | 82.0 | 80.5 | 77.2 |
| Average Queue (m) | 6.6 | 19.5 | 22.1 | 16.6 | 41.3 | 16.1 | 14.1 | 26.0 | 14.1 | 36.9 | 37.7 | 35.5 |
| 95th Queue (m) | 18.9 | 35.2 | 35.1 | 27.7 | 72.9 | 32.0 | 34.2 | 49.3 | 33.3 | 67.3 | 68.4 | 67.6 |
| Link Distance (m) |  | 1788.0 | 1788.0 |  |  | 728.6 | 728.6 |  |  | 744.3 | 744.3 | 744.3 |
| Upstream BIk Time (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |  |  |  |  |  |  |  |
| Storage Bay Dist (m) | 80.0 |  |  | 115.0 | 85.0 |  |  | 35.0 | 35.0 |  |  |  |
| Storage Blk Time (\%) |  |  |  |  | 0 |  | 1 | 4 | 1 | 9 |  |  |
| Queuing Penalty (veh) |  |  |  |  | 0 |  | 2 | 2 | 3 | 7 |  |  |

Intersection: 2: Regional Road 25 \& James Snow Parkway

| Movement | NB | SB | SB | SB | SB |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Directions Served | R | L | T | T | TR |
| Maximum Queue $(\mathrm{m})$ | 25.7 | 49.9 | 46.8 | 47.2 | 42.1 |
| Average Queue $(\mathrm{m})$ | 7.2 | 21.4 | 22.0 | 23.8 | 12.6 |
| 95th Queue $(\mathrm{m})$ | 18.6 | 42.3 | 39.4 | 42.1 | 31.6 |
| Link Distance $(\mathrm{m})$ | 744.3 |  | 994.0 | 994.0 | 994.0 |
| Upstream Blk Time (\%) |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |
| Storage Bay Dist (m) |  | 75.0 |  |  |  |
| Storage Blk Time (\%) |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |

Intersection: 3: Regional Road 25 \& Hwy 401 Westbound Off-Ramp

| Movement | WB | WB | NB | NB | NB | SB | SB | SB |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | L | L | T | T | T | T | T | T |
| Maximum Queue (m) | 47.9 | 55.4 | 51.5 | 54.0 | 55.5 | 47.1 | 49.8 | 46.0 |
| Average Queue $(\mathrm{m})$ | 18.1 | 32.2 | 23.3 | 24.4 | 22.3 | 24.1 | 25.0 | 21.9 |
| 95th Queue $(\mathrm{m})$ | 38.2 | 49.3 | 44.3 | 46.9 | 47.0 | 40.2 | 43.0 | 40.0 |
| Link Distance $(\mathrm{m})$ |  |  | 339.1 | 339.1 | 339.1 | 744.3 | 744.3 | 744.3 |
| Upstream Blk Time (\%) |  |  |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |  |  |  |
| Storage Bay Dist (m) | 80.0 | 80.0 |  |  |  |  |  |  |
| Storage Blk Time (\%) |  |  |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |  |  |  |

Intersection: 4: Regional Road 25 \& Hwy 401 Eastbound Off-Ramp/Carpool Lot

| Movement | EB | EB | EB | WB | NB | NB | NB | SB | SB | SB | SB |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Directions Served | L | TR | R | LTR | T | T | TR | L | T | T | T |
| Maximum Queue (m) | 72.2 | 55.3 | 53.4 | 30.9 | 112.0 | 99.2 | 67.7 | 23.8 | 59.6 | 63.6 | 69.0 |
| Average Queue (m) | 28.9 | 28.2 | 22.8 | 13.2 | 62.9 | 50.0 | 26.1 | 6.6 | 28.3 | 31.1 | 35.1 |
| 95th Queue (m) | 56.9 | 45.9 | 41.6 | 27.4 | 100.2 | 87.8 | 57.9 | 16.9 | 49.8 | 54.3 | 59.4 |
| Link Distance (m) |  | 434.1 |  | 85.8 | 183.3 | 183.3 | 183.3 |  | 339.1 | 339.1 | 339.1 |
| Upstream Blk Time (\%) |  |  |  |  |  |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |  |  |  |  |  |  |
| Storage Bay Dist (m) | 130.0 |  | 130.0 |  |  |  |  | 30.0 |  |  |  |
| Storage Blk Time (\%) |  |  |  |  |  |  |  | 0 | 6 |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |  |  | 0 | 2 |  |  |

Intersection: 5: Tremaine Road \& Hwy 401 Westbound Off-Ramp

| Movement | WB | WB | WB | NB | NB | SB | SB |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Directions Served | L | L | R | T | T | T | T |
| Maximum Queue (m) | 78.6 | 73.0 | 49.1 | 71.7 | 74.8 | 61.2 | 52.6 |
| Average Queue (m) | 49.3 | 43.9 | 20.4 | 37.9 | 39.4 | 30.9 | 30.2 |
| 95th Queue (m) | 69.6 | 66.3 | 37.8 | 65.3 | 66.9 | 51.9 | 47.4 |
| Link Distance (m) | 387.2 | 387.2 |  | 301.3 | 301.3 | 764.7 | 764.7 |
| Upstream Blk Time (\%) |  |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |
| Storage Blk Time (\%) |  |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |  |  |

Intersection: 6: Tremaine Road \& Hwy 401 Eastbound Off-Ramp/Carpool Lot

| Movement | EB | EB | EB | WB | WB | NB | NB | SB | SB | SB |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | L | TR | R | L | R | T | TR | L | T | T |
| Maximum Queue $(\mathrm{m})$ | 71.7 | 61.6 | 57.3 | 32.3 | 31.0 | 94.6 | 84.1 | 22.4 | 94.3 | 96.9 |
| Average Queue $(\mathrm{m})$ | 31.9 | 33.0 | 26.8 | 11.8 | 8.6 | 54.8 | 42.6 | 5.0 | 49.7 | 55.5 |
| 95th Queue $(\mathrm{m})$ | 60.6 | 53.8 | 49.9 | 25.5 | 20.2 | 86.0 | 75.1 | 15.0 | 82.5 | 87.5 |
| Link Distance $(\mathrm{m})$ |  | 455.1 |  | 125.3 |  | 250.9 | 250.9 |  | 301.3 | 301.3 |
| Upstream Blk Time (\%) |  |  |  |  |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |  |  |  |  |  |
| Storage Bay Dist (m) | 300.0 |  | 165.0 |  | 20.0 |  |  | 120.0 |  |  |
| Storage Blk Time (\%) |  |  |  | 5 | 1 |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  | 2 | 0 |  |  |  |  |  |

## Network Summary

Network wide Queuing Penalty: 18

## Junctions 9

## ARCADY 9 - Roundabout Module

Version: 9.5.1.7462
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Filename: 10108_Milton Quarry_v3_20221216_90percent.j9
Path: G:\Projects\2021\10108 - Milton Quarry Expansion TIS\03 Analysis 104 ARCADY101 RTC Volume Update Report generation date: 2022-12-16 4:34:34 PM
„90\% Intercept Adjustment - 2021 Existing, AM
„90\% Intercept Adjustment - 2021 Existing, PM
»90\% Intercept Adjustment - 2026 Total, AM
»90\% Intercept Adjustment - 2026 Total, PM

## Summary of intersection performance

|  | AM |  |  |  |  |  | PM |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 95\% Queue (Veh) | Delay (s) | v/c Ratio | LOS | Intersection Delay (s) | Intersection LOS | 95\% Queue (Veh) | Delay <br> (s) | V/C Ratio | LOS | $\begin{aligned} & \text { Intersection } \\ & \text { Delay (s) } \end{aligned}$ | $\begin{aligned} & \text { Intersection } \\ & \text { LOS } \end{aligned}$ |
|  | 90\% Intercept Adjustment - 2021 Existing |  |  |  |  |  |  |  |  |  |  |  |
| 1 - James Snow Parkway | 1.1 | 2.36 | 0.22 | A | 3.45 | A | 0.5 | 1.77 | 0.20 | A | 2.39 | A |
| 2 - Dublin Line | 1.1 | 6.67 | 0.27 | A |  |  | 0.5 | 5.07 | 0.12 | A |  |  |
| 3 - Campbellville Road | 0.5 | 2.26 | 0.20 | A |  |  | 0.5 | 2.26 | 0.16 | A |  |  |
| 4 - Tremaine Road | $\sim 1$ | 0.00 | 0.00 | A |  |  | $\sim 1$ | 0.00 | 0.00 | A |  |  |
|  | 90\% Intercept Adjustment - 2026 Total |  |  |  |  |  |  |  |  |  |  |  |
| 1 - James Snow Parkway | 1.5 | 3.07 | 0.49 | A | 5.22 | A | 6.9 | 5.42 | 0.75 | A | 6.79 | A |
| 2 - Dublin Line | 2.3 | 13.82 | 0.43 | B |  |  | 3.6 | 39.25 | 0.52 | E |  |  |
| 3 - Campbellville Road | 1.4 | 4.77 | 0.52 | A |  |  | 1.4 | 7.35 | 0.55 | A |  |  |
| 4 - Tremaine Road | 1.2 | 5.22 | 0.22 | A |  |  | 0.5 | 4.16 | 0.18 | A |  |  |

There are warnings associated with one or more model runs - see the 'Data Errors and Warnings' tables for each Analysis or Demand Set.
Values shown are the highest values encountered over all time segments. Delay is the maximum value of average delay per arriving vehicle. Intersection LOS and Intersection Delay are demand-weighted averages.

File summary
File Description

| Title | (untitled) |
| :--- | :--- |
| Location |  |
| Site number |  |
| Date | $2019-02-20$ |
| Version |  |
| Status | (new file) |
| Identifier |  |
| Client |  |
| Jobnumber |  |
| Analyst | HQTMIGMkrodgers |
| Description |  |

Units

| Distance units | Speed units | Traffic units input | Traffic units results | Flow units | Average delay units | Total delay units | Rate of delay units |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| m | kph | Veh | Veh | perHour | s | - Min | perMin |



4 - Tremaine Road

Flows show original traticic demand (Vehhr).
The intersection diagram reflects the last run of Intersections.

## Analysis Options

| Vehicle length (m) | Calculate Queue Percentiles | Calculate detailed queueing delay | Calculate residual capacity | V/C Ratio <br> Threshold | Average Delay threshold (s) | Queue threshold (PCE) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 5.75 | $\checkmark$ |  |  | 0.85 | 36.00 | 20.00 |

## Demand Set Summary

| ID | Scenario name | Time Period name | Traffic profile type | Start time (HH:mm) | Finish time (HH:mm) | Time segment length (min) | Run automatically |
| :--- | :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| D1 | 2021 Existing | AM | PHF | $08: 00$ | $09: 00$ | 15 |  |
| D2 | 2021 Existing | PM | PHF | $17: 00$ | $18: 00$ | 15 |  |
| D3 | 2026 Total | AM | PHF | $08: 00$ | $09: 00$ | 15 |  |
| D4 | 2026 Total | PM | PHF | $17: 00$ | $18: 00$ |  |  |

## Analysis Set Details

| ID | Name | Include in report | Network flow scaling factor (\%) | Network capacity scaling factor (\%) |
| :---: | :---: | :---: | :---: | :---: |
| A1 | $90 \%$ Intercept Adjustment | $\checkmark$ | 100.000 | 100.000 |

## 90\% Intercept Adjustment - 2021 Existing, AM

Data Errors and Warnings

| Severity | Area | Item | Description |
| :---: | :---: | :---: | :---: |
| Warning | Pedestrian Crossing | 1 - James Snow Parkway - Pedestrian crossing | Pedestrian crossing uses default settings only. Is this correct? |
| Warning | Pedestrian Crossing | 1 - James Snow Parkway - Pedestrian crossing | Pedestrian crossing uses default flow of 0 . Is this correct? |
| Warning | Pedestrian Crossing | 2 - Dublin Line - <br> Pedestrian crossing | Pedestrian crossing uses default settings only. Is this correct? |
| Warning | Pedestrian Crossing | 2 - Dublin Line Pedestrian crossing | Pedestrian crossing uses default flow of 0 . Is this correct? |
| Warning | Pedestrian Crossing | 3 - Campbellville Road <br> - Pedestrian crossing | Pedestrian crossing uses default settings only. Is this correct? |
| Warning | Pedestrian Crossing | 3 - Campbellville Road <br> - Pedestrian crossing | Pedestrian crossing uses default flow of 0 . Is this correct? |
| Warning | Pedestrian Crossing | 4 - Tremaine Road Pedestrian crossing | Pedestrian crossing uses default settings only. Is this correct? |
| Warning | Pedestrian Crossing | 4 - Tremaine Road Pedestrian crossing | Pedestrian crossing uses default flow of 0 . Is this correct? |
| Warning | Queue variations | Analysis Options | Queue percentiles may be unreliable if the mean queue in any time segment is very low or very high. |

## Intersection Network

## Intersections

| Intersection | Name | Intersection type | Use circulating lanes | Leg order | Intersection Delay (s) | Intersection LOS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathbf{1}$ | untitled | Standard Roundabout |  | $1,2,3,4$ | 3.45 | A |

## Intersection Network Options

| Driving side | Lighting |
| :---: | :---: |
| Right | Normal/unknown |

## Legs

## Legs

| Leg | Name | Description |
| :---: | :--- | :--- |
| $\mathbf{1}$ | James Snow Parkway |  |
| $\mathbf{2}$ | Dublin Line |  |
| $\mathbf{3}$ | Campbellville Road |  |
| $\mathbf{4}$ | Tremaine Road |  |

Roundabout Geometry

| Leg | V - Approach road half-width (m) | E-Entry width (m) | I' - Effective flare length (m) | R - Entry radius (m) | D - Inscribed circle diameter (m) | PHI - Conflict (entry) angle (deg) | Exit only |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 - James Snow Parkway | 9.80 | 10.15 | 7.5 | 25.0 | 57.0 | 9.0 |  |
| 2 - Dublin Line | 3.90 | 7.00 | 11.7 | 32.0 | 57.0 | 16.0 |  |
| 3 - Campbellville Road | 7.30 | 9.94 | 8.6 | 25.0 | 57.0 | 25.0 |  |
| 4 - Tremaine Road | 3.40 | 6.00 | 12.4 | 31.0 | 57.0 | 28.0 |  |

## Bypass

| Leg | Leg has bypass | Bypass utilisation (\%) |
| :--- | :---: | :---: |
| 1- James Snow Parkway |  |  |
| 2 - Dublin Line |  |  |
| 3-Campbellville Road |  |  |
| 4 - Tremaine Road | $\checkmark$ | 100 |

## Unsignalled Pedestrian Crossing Crossings

| Leg | Space between crossing and intersection entry (Unsignalled Pedestrian Crossing) (PCE) | Vehicles queueing on exit (Unsignalled Pedestrian Crossing) (PCE) | Central Refuge | Crossing data type | Crossing length (entry side) (m) | Crossing time (entry side) (s) | Crossing length (exit side) (m) | Crossing time (exit side) (s) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1-James Snow Parkway | 1.00 | 1.00 | $\checkmark$ | Distance | 0.00 | 0.00 | 0.00 | 0.00 |
| 2 - Dublin Line | 1.00 | 1.00 | $\checkmark$ | Distance | 0.00 | 0.00 | 0.00 | 0.00 |
| 3 - Campbellville Road | 1.00 | 1.00 | $\checkmark$ | Distance | 0.00 | 0.00 | 0.00 | 0.00 |
| 4 - Tremaine Road | 1.00 | 1.00 | $\checkmark$ | Distance | 0.00 | 0.00 | 0.00 | 0.00 |

## Slope / Intercept / Capacity

Leg Intercept Adjustments

| Leg | Type | Reason | Percentage intercept adjustment (\%) |
| :--- | :---: | :---: | :---: |
| 1 - James Snow Parkway | Percentage |  | 90.00 |
| 2 - Dublin Line | Percentage |  | 90.00 |
| 3 - Campbellville Road | Percentage |  | 90.00 |
| 4 - Tremaine Road | Percentage |  | 90.00 |

Roundabout Slope and Intercept used in model

| Leg | Final slope | Final intercept (PCE/hr) |
| :--- | :---: | :---: |
| 1 - James Snow Parkway | 0.884 | 2983 |
| 2 - Dublin Line | 0.610 | 1622 |
| 3 - Campbellville Road | 0.757 | 2418 |
| 4 - Tremaine Road | 0.551 | 1384 |

The slope and intercept shown above include any corrections and adjustments.

Leg Capacity Adjustments

| Leg | Type | Reason | Percentage capacity adjustment (\%) |
| :---: | :---: | :---: | :---: |
| 4- Tremaine Road | Percentage |  | 100.00 |

## Traffic Demand

## Demand Set Details

| ID | Scenario name | Time Period name | Traffic profile type | Start time (HH:mm) | Finish time (HH:mm) | Time segment length (min) | Run automatically |
| :--- | :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| D1 | 2021 Existing | AM | PHF | $08: 00$ | $09: 00$ | 15 | $\checkmark$ |


| Vehicle mix varies over turn | Vehicle mix varies over entry | Vehicle mix source | PCE Factor for a Truck (PCE) |
| :---: | :---: | :---: | :---: |
| $\checkmark$ | $\checkmark$ | Truck Percentages | 2.00 |

## Demand overview (Traffic)

| Leg | Linked leg | Profile type | Use O-D data | Average Demand (Veh/hr) | Scaling Factor (\%) |
| :--- | :---: | :---: | :---: | :---: | :---: |
| 1- James Snow Parkway |  | PHF | $\checkmark$ | 388 | 100.000 |
| 2 - Dublin Line |  | PHF | $\checkmark$ | 174 | 100.000 |
| 3 - Campbellville Road |  | PHF | $\checkmark$ | 357 | 100.000 |
| 4 - Tremaine Road |  | PHF | $\checkmark$ | 0 | 100.000 |

## Peak Hour Factor Data (Traffic)

| Leg | Hourly volume (Veh/hr) | Peak hour factor | Peak time segment |
| :--- | :---: | :---: | :---: |
| 1 - James Snow Parkway | 388 | 0.89 | SecondQuarter |
| 2 - Dublin Line | 174 | 0.89 | SecondQuarter |
| 3 - Campbellville Road | 357 | 0.89 | SecondQuarter |
| 4 Tremaine Road | 0 | 0.89 | SecondQuarter |

## Demand overview (Pedestrians)

| Leg | Profile type | Average pedestrian flow (Ped/hr) |
| :--- | :---: | :---: |
| 1 - James Snow Parkway | $[\mathrm{PHF}]$ | 0.00 |
| 2 - Dublin Line | $[\mathrm{PHF}]$ | 0.00 |
| 3 - Campbellville Road | $[\mathrm{PHF}]$ | 0.00 |
| 4 - Tremaine Road | $[\mathrm{PHF}]$ | 0.00 |

## Peak Hour Factor Data (Pedestrians)

| Leg | Hourly volume (Ped/hr) | Peak hour factor | Peak time segment |
| :--- | :---: | :---: | :---: |
| 1 - James Snow Parkway | 0.00 | 1.00 | SecondQuarter |
| 2 - Dublin Line | 0.00 | 1.00 | SecondQuarter |
| 3 - Campbellville Road | 0.00 | 1.00 | SecondQuarter |
| 4 - Tremaine Road | 0.00 | 1.00 | SecondQuarter |

## Origin-Destination Data

Demand (Veh/hr)

|  | To |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| From | 1 - James Snow Parkway | 2 - Dublin Line | 3 - Campbellville Road | 4 - Tremaine Road |  |
|  | 1- James Snow Parkway | 0 | 169 | 219 | 0 |
|  | 2 - Dublin Line | 167 | 0 | 7 | 0 |
|  | 3 - Campbellville Road | 349 | 8 | 0 | 0 |
|  | 4 - Tremaine Road | 0 | 0 | 0 | 0 |

## Vehicle Mix

Truck Percentages

|  | To |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| From |  |  |  |  |  |  | 1-James Snow Parkway | 2 - Dublin Line | 3 - Campbellville Road | 4 - Tremaine Road |
|  | 1 - James Snow Parkway | 0 | 96 | 17 | 0 |  |  |  |  |  |
|  | 2 - Dublin Line | 98 | 0 | 71 | 0 |  |  |  |  |  |
|  | 3 - Campbellville Road | 6 | 63 | 0 | 0 |  |  |  |  |  |
|  | 4 - Tremaine Road | 0 | 0 | 0 | 0 |  |  |  |  |  |

## Results

Results Summary for whole modelled period

| Leg | Max V/C Ratio | Max Delay (s) | Max Queue (Veh) | Max 95th percentile Queue (Veh) | Max LOS | Average Demand (Veh/hr) | Total Intersection Arrivals (Veh) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 - James Snow Parkway | 0.22 | 2.36 | 0.3 | 1.1 | A | 388 | 388 |
| 2 - Dublin Line | 0.27 | 6.67 | 0.4 | 1.1 | A | 174 | 174 |
| 3 - Campbellville Road | 0.20 | 2.26 | 0.3 | 0.5 | A | 357 | 357 |
| 4 - Tremaine Road | 0.00 | 0.00 | 0.0 | $\sim 1$ | A | 0 | 0 |

THE FUTURE

## 90\% Intercept Adjustment - 2021 Existing, PM

Data Errors and Warnings

| Severity | Area | Item | Description |
| :--- | :--- | :--- | :--- |
| Warning | Pedestrian Crossing | 1-James Snow <br> Parkway - Pedestrian <br> crossing | Pedestrian crossing uses default settings only. Is this correct? |
| Warning | Pedestrian Crossing | 1-James Snow <br> Parkway - Pedestrian <br> crossing | Pedestrian crossing uses default flow of 0. Is this correct? |
| Warning | Pedestrian Crossing | 2-Dublin Line - <br> Pedestrian crossing | Pedestrian crossing uses default settings only. Is this correct? |
| Warning | Pedestrian Crossing | 2-Dublin Line - <br> Pedestrian crossing | Pedestrian crossing uses default flow of 0. Is this correct? |
| Warning | Pedestrian Crossing | 3-Campbellville Road <br> - -Pedestrian crossing | Pedestrian crossing uses default settings only. Is this correct? |
| Warning | Pedestrian Crossing | 3-Campbellville Road <br> - Pedestrian crossing | Pedestrian crossing uses default flow of 0. Is this correct? |
| Warning | Pedestrian Crossing | 4-Tremaine Road - <br> Pedestrian crossing | Pedestrian crossing uses default settings only. Is this correct? |
| Warning | Pedestrian Crossing | 4-Tremaine Road - <br> Pedestrian crossing | Pedestrian crossing uses default flow of 0. Is this correct? |
| Warning | Queue variations | Analysis Options | Queue percentiles may be unreliable if the mean queue in any time segment is very low or very high. |

## Intersection Network

## Intersections

| Intersection | Name | Intersection type | Use circulating lanes | Leg order | Intersection Delay (s) | Intersection LOS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathbf{1}$ | untitled | Standard Roundabout |  | $1,2,3,4$ | 2.39 | A |

## Intersection Network Options

| Driving side | Lighting |
| :---: | :---: |
| Right | Normal/unknown |

## Traffic Demand

## Demand Set Details

| ID | Scenario name | Time Period name | Traffic profile type | Start time (HH:mm) | Finish time (HH:mm) | Time segment length (min) | Run automatically |
| :--- | :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| D2 | 2021 Existing | PM | PHF | $17: 00$ | $18: 00$ | 15 | $\checkmark$ |


| Vehicle mix varies over turn | Vehicle mix varies over entry | Vehicle mix source | PCE Factor for a Truck (PCE) |
| :---: | :---: | :---: | :---: |
| $\checkmark$ | $\checkmark$ | Truck Percentages | 2.00 |

## Demand overview (Traffic)

| Leg | Linked leg | Profile type | Use O-D data | Average Demand (Veh/hr) | Scaling Factor (\%) |
| :--- | :---: | :---: | :---: | :---: | :---: |
| 1- James Snow Parkway |  | PHF | $\checkmark$ | 454 | 100.000 |
| 2 - Dublin Line |  | PHF | $\checkmark$ | 84 | 100.000 |
| 3 - Campbellville Road |  | PHF | $\checkmark$ | 262 | 100.000 |
| 4- Tremaine Road |  | PHF | $\checkmark$ | 0 | 100.000 |

## Peak Hour Factor Data (Traffic)

| Leg | Hourly volume (Veh/hr) | Peak hour factor | Peak time segment |
| :--- | :---: | :---: | :---: |
| 1 - James Snow Parkway | 454 | 0.89 | SecondQuarter |
| 2 - Dublin Line | 84 | 0.89 | SecondQuarter |
| 3 - Campbellville Road | 262 | 0.89 | SecondQuarter |
| 4 Tremaine Road | 0 | 0.89 | SecondQuarter |

## Demand overview (Pedestrians)

| Leg | Profile type | Average pedestrian flow (Ped/hr) |
| :--- | :---: | :---: |
| 1- James Snow Parkway | $[P H F]$ | 0.00 |
| 2 - Dublin Line | $[P H F]$ | 0.00 |
| 3- Campbellville Road | $[P H F]$ | 0.00 |
| 4- Tremaine Road | $[P H F]$ | 0.00 |

## Peak Hour Factor Data (Pedestrians)

| Leg | Hourly volume (Ped/hr) | Peak hour factor | Peak time segment |
| :--- | :---: | :---: | :---: |
| 1 - James Snow Parkway | 0.00 | 1.00 | SecondQuarter |
| 2 - Dublin Line | 0.00 | 1.00 | SecondQuarter |
| 3 - Campbellville Road | 0.00 | 1.00 | SecondQuarter |
| 4 - Tremaine Road | 0.00 | 1.00 | SecondQuarter |

## Origin-Destination Data

Demand (Veh/hr)

|  | To |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| From | 1 - James Snow Parkway | 2 - Dublin Line | 3 - Campbellville Road | 4 - Tremaine Road |  |
|  | 1- James Snow Parkway | 0 | 69 | 385 | 0 |
|  | 2 - Dublin Line | 74 | 0 | 10 | 0 |
|  | 3 - Campbellville Road | 258 | 4 | 0 | 0 |
|  | 4 - Tremaine Road | 0 | 0 | 0 | 0 |

## Vehicle Mix

Truck Percentages

|  | To |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| From |  |  |  |  |  |  | 1-James Snow Parkway | 2 - Dublin Line | 3 - Campbellville Road | 4 - Tremaine Road |
|  | 1 - James Snow Parkway | 0 | 78 | 6 | 0 |  |  |  |  |  |
|  | 2 - Dublin Line | 73 | 0 | 20 | 0 |  |  |  |  |  |
|  | 3 - Campbellville Road | 22 | 50 | 0 | 0 |  |  |  |  |  |
|  | 4 - Tremaine Road | 0 | 0 | 0 | 0 |  |  |  |  |  |

## Results

Results Summary for whole modelled period

| Leg | Max V/C Ratio | Max Delay (s) | Max Queue (Veh) | Max 95th percentile Queue (Veh) | Max LOS | Average Demand (Veh/hr) | Total Intersection Arrivals (Veh) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 - James Snow Parkway | 0.20 | 1.77 | 0.2 | 0.5 | A | 454 | 454 |
| 2 - Dublin Line | 0.12 | 5.07 | 0.1 | 0.5 | A | 84 | 84 |
| 3-Campbellville Road | 0.16 | 2.26 | 0.2 | 0.5 | A | 262 | 262 |
| 4 - Tremaine Road | 0.00 | 0.00 | 0.0 | $\sim 1$ | A | 0 | 0 |

## 90\% Intercept Adjustment - 2026 Total, AM

Data Errors and Warnings

| Severity | Area | Item | Description |
| :---: | :---: | :---: | :---: |
| Warning | Pedestrian Crossing | 1 - James Snow Parkway - Pedestrian crossing | Pedestrian crossing uses default settings only. Is this correct? |
| Warning | Pedestrian Crossing | 1 - James Snow Parkway - Pedestrian crossing | Pedestrian crossing uses default flow of 0 . Is this correct? |
| Warning | Pedestrian Crossing | 2 - Dublin Line - <br> Pedestrian crossing | Pedestrian crossing uses default settings only. Is this correct? |
| Warning | Pedestrian Crossing | 2 - Dublin Line Pedestrian crossing | Pedestrian crossing uses default flow of 0 . Is this correct? |
| Warning | Pedestrian Crossing | 3 - Campbellville Road <br> - Pedestrian crossing | Pedestrian crossing uses default settings only. Is this correct? |
| Warning | Pedestrian Crossing | 3 - Campbellville Road <br> - Pedestrian crossing | Pedestrian crossing uses default flow of 0 . Is this correct? |
| Warning | Pedestrian Crossing | 4 - Tremaine Road Pedestrian crossing | Pedestrian crossing uses default settings only. Is this correct? |
| Warning | Pedestrian Crossing | 4 - Tremaine Road Pedestrian crossing | Pedestrian crossing uses default flow of 0 . Is this correct? |
| Warning | Queue variations | Analysis Options | Queue percentiles may be unreliable if the mean queue in any time segment is very low or very high. |

## Intersection Network

## Intersections

| Intersection | Name | Intersection type | Use circulating lanes | Leg order | Intersection Delay (s) | Intersection LOS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathbf{1}$ | untitled | Standard Roundabout |  | $1,2,3,4$ | 5.22 | A |

## Intersection Network Options

| Driving side | Lighting |
| :---: | :---: |
| Right | Normal/unknown |

## Traffic Demand

## Demand Set Details

| ID | Scenario name | Time Period name | Traffic profile type | Start time (HH:mm) | Finish time (HH:mm) | Time segment length (min) | Run automatically |
| :--- | :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| D3 | 2026 Total | AM | PHF | $08: 00$ | $09: 00$ | 15 | $\checkmark$ |


| Vehicle mix varies over turn | Vehicle mix varies over entry | Vehicle mix source | PCE Factor for a Truck (PCE) |
| :---: | :---: | :---: | :---: |
| $\checkmark$ | $\checkmark$ | Truck Percentages | 2.00 |

## Demand overview (Traffic)

| Leg | Linked leg | Profile type | Use O-D data | Average Demand (Veh/hr) | Scaling Factor (\%) |
| :--- | :---: | :---: | :---: | :---: | :---: |
| 1- James Snow Parkway |  | PHF | $\checkmark$ | 998 | 100.000 |
| 2 - Dublin Line |  | PHF | $\checkmark$ | 174 | 100.000 |
| 3 - Campbellville Road |  | PHF | $\checkmark$ | 722 | 100.000 |
| 4- Tremaine Road |  | PHF | $\checkmark$ | 890 | 100.000 |

## Peak Hour Factor Data (Traffic)

| Leg | Hourly volume (Veh/hr) | Peak hour factor | Peak time segment |
| :--- | :---: | :---: | :---: |
| 1 - James Snow Parkway | 998 | 0.89 | SecondQuarter |
| 2 - Dublin Line | 174 | 0.89 | SecondQuarter |
| 3 - Campbellville Road | 722 | 0.89 | SecondQuarter |
| 4 - Tremaine Road | 890 | 0.89 | SecondQuarter |

## Demand overview (Pedestrians)

| Leg | Profile type | Average pedestrian flow (Ped/hr) |
| :--- | :---: | :---: |
| 1 - James Snow Parkway | $[\mathrm{PHF}]$ | 0.00 |
| 2 - Dublin Line | $[\mathrm{PHF}]$ | 0.00 |
| 3 - Campbellville Road | $[\mathrm{PHF}]$ | 0.00 |
| 4 - Tremaine Road | $[\mathrm{PHF}]$ | 0.00 |

## Peak Hour Factor Data (Pedestrians)

| Leg | Hourly volume (Ped/hr) | Peak hour factor | Peak time segment |
| :--- | :---: | :---: | :---: |
| 1 - James Snow Parkway | 0.00 | 1.00 | SecondQuarter |
| 2 - Dublin Line | 0.00 | 1.00 | SecondQuarter |
| 3 - Campbellville Road | 0.00 | 1.00 | SecondQuarter |
| 4 - Tremaine Road | 0.00 | 1.00 | SecondQuarter |

## Origin-Destination Data

Demand (Veh/hr)

|  | To |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| From | 1 - James Snow Parkway | 2 - Dublin Line | 3 - Campbellville Road | 4 - Tremaine Road |  |
|  | 1- James Snow Parkway | 0 | 169 | 254 | 575 |
|  | 2 - Dublin Line | 167 | 0 | 7 | 0 |
|  | 3 - Campbellville Road | 405 | 8 | 0 | 309 |
|  | 4 - Tremaine Road | 712 | 0 | 178 | 0 |

## Vehicle Mix

Truck Percentages

|  | To |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| From |  |  |  |  |  |  | 1-James Snow Parkway | 2 - Dublin Line | 3 - Campbellville Road | 4 - Tremaine Road |
|  | 1 - James Snow Parkway | 0 | 96 | 17 | 2 |  |  |  |  |  |
|  | 2 - Dublin Line | 98 | 0 | 71 | 0 |  |  |  |  |  |
|  | 3 - Campbellville Road | 6 | 63 | 0 | 2 |  |  |  |  |  |
|  | 4 - Tremaine Road | 2 | 0 | 2 | 0 |  |  |  |  |  |

## Results

Results Summary for whole modelled period

| Leg | Max V/C Ratio | Max Delay (s) | Max Queue (Veh) | Max 95th <br> percentile Queue <br> (Veh) | Max Los | Average Demand <br> (Veh/hr) | Total Intersection <br> Arrivals (Veh) |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1- James Snow Parkway | 0.49 | 3.07 | 1.0 | 1.5 | A | 998 |  |
| 2 - Dublin Line | 0.43 | 13.82 | 0.7 | 2.3 | B | 174 |  |
| 3-Campbellville Road | 0.52 | 4.77 | 1.1 | 1.4 | A | 722 | 174 |
| 4- Tremaine Road | 0.22 | 5.22 | 0.3 | 1.2 | A | 722 |  |

## 90\% Intercept Adjustment - 2026 Total, PM

Data Errors and Warnings

| Severity | Area | Item |  |
| :--- | :--- | :--- | :--- |
| Warning | Pedestrian Crossing | 1 - James Snow <br> Parkway - Pedestrian <br> crossing | Pedestrian crossing uses default settings only. Is this correct? |
| Warning | Pedestrian Crossing | 1 - James Snow <br> Parkway - Pedestrian <br> crossing | Pedestrian crossing uses default flow of 0. Is this correct? |
| Warning | Pedestrian Crossing | 2 - Dublin Line - <br> Pedestrian crossing | Pedestrian crossing uses default settings only. Is this correct? |
| Warning | Pedestrian Crossing | 2 - Dublin Line - <br> Pedestrian crossing | Pedestrian crossing uses default flow of 0. Is this correct? |
| Warning | Pedestrian Crossing | 3 - Campbellville Road <br> - - Pedestrian crossing | Pedestrian crossing uses default settings only. Is this correct? |
| Warning | Pedestrian Crossing | 3 - Campbellville Road <br> - Pedestrian crossing | Pedestrian crossing uses default flow of 0. Is this correct? |
| Warning | Pedestrian Crossing | 4 - Tremaine Road - <br> Pedestrian crossing | Pedestrian crossing uses default settings only. Is this correct? |
| Warning | Pedestrian Crossing | 4 - Tremaine Road - <br> Pedestrian crossing | Pedestrian crossing uses default flow of 0 . Is this correct? |
| Warning | Queue variations | Analysis Options | Queue percentiles may be unreliable if the mean queue in any time segment is very low or very high. |

## Intersection Network

## Intersections

| Intersection | Name | Intersection type | Use circulating lanes | Leg order | Intersection Delay (s) | Intersection LOS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathbf{1}$ | untitled | Standard Roundabout |  | $1,2,3,4$ | 6.79 | A |

## Intersection Network Options

| Driving side | Lighting |
| :---: | :---: |
| Right | Normal/unknown |

## Traffic Demand

## Demand Set Details

| ID | Scenario name | Time Period name | Traffic profile type | Start time (HH:mm) | Finish time (HH:mm) | Time segment length (min) | Run automatically |
| :--- | :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| D4 | 2026 Total | PM | PHF | $17: 00$ | $18: 00$ | 15 | $\checkmark$ |


| Vehicle mix varies over turn | Vehicle mix varies over entry | Vehicle mix source | PCE Factor for a Truck (PCE) |
| :---: | :---: | :---: | :---: |
| $\checkmark$ | $\checkmark$ | Truck Percentages | 2.00 |

## Demand overview (Traffic)

| Leg | Linked leg | Profile type | Use O-D data | Average Demand (Veh/hr) | Scaling Factor (\%) |
| :--- | :---: | :---: | :---: | :---: | :---: |
| 1 - James Snow Parkway |  | PHF | $\checkmark$ | 1774 | 100.000 |
| 2 - Dublin Line |  | PHF | $\checkmark$ | 84 | 100.000 |
| 3 - Campbellville Road |  | PHF | $\checkmark$ | 525 | 100.000 |
| 4 - Tremaine Road |  | PHF | $\checkmark$ | 862 | 100.000 |

## Peak Hour Factor Data (Traffic)

| Leg | Hourly volume (Veh/hr) | Peak hour factor | Peak time segment |
| :--- | :---: | :---: | :---: |
| 1 - James Snow Parkway | 1774 | 0.89 | SecondQuarter |
| 2 - Dublin Line | 84 | 0.89 | SecondQuarter |
| 3 - Campbellville Road | 525 | 0.89 | SecondQuarter |
| 4 - Tremaine Road | 862 | 0.89 | SecondQuarter |

## Demand overview (Pedestrians)

| Leg | Profile type | Average pedestrian flow (Ped/hr) |
| :--- | :---: | :---: |
| 1 - James Snow Parkway | $[\mathrm{PHF}]$ | 0.00 |
| 2 - Dublin Line | $[\mathrm{PHF}]$ | 0.00 |
| 3 - Campbellville Road | $[\mathrm{PHF}]$ | 0.00 |
| 4 - Tremaine Road | $[\mathrm{PHF}]$ | 0.00 |

## Peak Hour Factor Data (Pedestrians)

| Leg | Hourly volume (Ped/hr) | Peak hour factor | Peak time segment |
| :--- | :---: | :---: | :---: |
| 1 - James Snow Parkway | 0.00 | 1.00 | SecondQuarter |
| 2 - Dublin Line | 0.00 | 1.00 | SecondQuarter |
| 3 - Campbellville Road | 0.00 | 1.00 | SecondQuarter |
| 4 - Tremaine Road | 0.00 | 1.00 | SecondQuarter |

## Origin-Destination Data

Demand (Veh/hr)

|  | To |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| From |  | 1 - James Snow Parkway | 2 - Dublin Line | 3 - Campbellville Road | 4 - Tremaine Road |
|  | 1- James Snow Parkway | 0 | 69 | 446 | 1259 |
|  | 2 - Dublin Line | 74 | 0 | 10 | 0 |
|  | 3-Campbellville Road | 299 | 4 | 0 | 222 |
|  | 4-Tremaine Road | 690 | 0 | 172 | 0 |

## Vehicle Mix

Truck Percentages

|  | To |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| From |  |  |  |  |  |  | 1-James Snow Parkway | 2 - Dublin Line | 3 - Campbellville Road | 4 - Tremaine Road |
|  | 1 - James Snow Parkway | 0 | 78 | 6 | 2 |  |  |  |  |  |
|  | 2 - Dublin Line | 73 | 0 | 20 | 0 |  |  |  |  |  |
|  | 3 - Campbellville Road | 22 | 50 | 0 | 2 |  |  |  |  |  |
|  | 4 - Tremaine Road | 2 | 0 | 2 | 0 |  |  |  |  |  |

## Results

Results Summary for whole modelled period

| Leg | Max V/C Ratio | Max Delay (s) | Max Queue (Veh) | Max 95th percentile Queue (Veh) | Max LOS | Average Demand (Veh/hr) | Total Intersection Arrivals (Veh) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 - James Snow Parkway | 0.75 | 5.42 | 3.0 | 6.9 | A | 1774 | 1774 |
| 2 - Dublin Line | 0.52 | 39.25 | 1.0 | 3.6 | E | 84 | 84 |
| 3 - Campbellville Road | 0.55 | 7.35 | 1.2 | 1.4 | A | 525 | 525 |
| 4 - Tremaine Road | 0.18 | 4.16 | 0.2 | 0.5 | A | 862 | 172 |

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## 'TYLin

Table 32026 Future Traffic Operations - Queues

| Intersection | Control Type | Available Storage (m) | Existing Haul Route |  |  |  | Future Haul Route |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | AM Peak Hour |  | PM Peak Hour |  | AM Peak Hour |  | PM Peak Hour |  |
| Turning Movement | - | - | 95 ${ }^{\text {th }} \%$ <br> Queue <br> (m) | 50 ${ }^{\text {th }} \%$ <br> Queue <br> (m) | 95 ${ }^{\text {th }} \%$ <br> Queue <br> (m) | 50 ${ }^{\text {th }} \%$ <br> Queue <br> (m) | 95 ${ }^{\text {th }} \%$ <br> Queue <br> (m) | 50 ${ }^{\text {th }} \%$ <br> Queue <br> (m) | 95 ${ }^{\text {th }} \%$ <br> Queue <br> (m) | 50 ${ }^{\text {th }} \%$ <br> Queue <br> (m) |
| Tremaine Road at Highway 401 Westbound Off-Ramp | Signal | - | - | - | - | - | - | - | - | - |
| Westbound Left | - | 970 | 47 | 30 | 74 | 50 | 58 | 29 | 70 | 49 |
| Westbound Right | - | 230 | 56 | 33 | 31 | 16 | 83 | 50 | 38 | 20 |
| Northbound Through | - | 300 | 46 | 27 | 67 | 39 | 48 | 27 | 67 | 39 |
| Southbound Through |  | >300 | 42 | 26 | 46 | 27 | 66 | 41 | 52 | 31 |
| Tremaine Road at Highway 401 Eastbound Off-Ramp | Signal | - | - | - | - | - | - | - | - | - |
| Eastbound Left | - | 300 | 34 | 18 | 57 | 31 | 34 | 17 | 61 | 32 |
| Eastbound Through / Right | - | 975 | 19 | 11 | 54 | 33 | 20 | 11 | 54 | 33 |
| Eastbound Right | - | 165 | 13 | 5 | 51 | 29 | 13 | 5 | 50 | 27 |
| Westbound Left | - | 50 | 19 | 7 | 25 | 12 | 19 | 7 | 26 | 12 |
| Westbound Right | - | 20 | 15 | 5 | 20 | 8 | 15 | 5 | 20 | 9 |
| Northbound Through | - | 370 | 65 | 36 | 87 | 57 | 67 | 36 | 86 | 55 |
| Northbound Through / Right | - | 370 | 53 | 23 | 78 | 43 | 56 | 23 | 75 | 43 |
| Southbound Left | - | 120 | 18 | 7 | 14 | 5 | 20 | 8 | 15 | 5 |
| Southbound Through | - | 300 | 52 | 28 | 90 | 58 | 58 | 31 | 88 | 56 |
| Regional Road 25 / James Snow Parkway | Signal | - | - | - | - | - | - | - | - | - |
| Eastbound Left | - | 80 | 13 | 3 | 19 | 7 | 15 | 5 | 19 | 7 |
| Eastbound Through | - |  | 21 | 9 | 36 | 23 | 21 | 9 | 35 | 22 |
| Eastbound Right | - | 115 | 39 | 23 | 35 | 21 | 19 | 7 | 28 | 17 |

## 'MIAin

| Intersection | Control Type | Available Storage (m) | Existing Haul Route |  |  |  | Future Haul Route |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | AM Peak Hour |  | PM Peak Hour |  | AM Peak Hour |  | PM Peak Hour |  |
| Turning Movement | - | - | 95 ${ }^{\text {th }} \%$ <br> Queue <br> (m) | $50^{\text {th }} \%$ <br> Queue <br> (m) | $95^{\text {th }} \%$ <br> Queue <br> (m) | $50^{\text {th }} \%$ <br> Queue <br> (m) | $95^{\text {th }} \%$ <br> Queue (m) | $50^{\text {th }} \%$ <br> Queue <br> (m) | $95^{\text {th }} \%$ <br> Queue <br> (m) | 50 ${ }^{\text {th }} \%$ <br> Queue <br> (m) |
| Westbound Left | - | 85 | 43 | 20 | 75 | 45 | 40 | 19 | 73 | 41 |
| Westbound Through | - | - | 32 | 17 | 30 | 15 | 31 | 17 | 34 | 16 |
| Westbound Right | - | 35 | 25 | 12 | 46 | 26 | 24 | 11 | 49 | 26 |
| Northbound Left | - | 35 | 69 | 39 | 48 | 24 | 37 | 18 | 33 | 14 |
| Northbound Through | - | - | 45 | 22 | 81 | 39 | 46 | 23 | 68 | 38 |
| Northbound Right | - | - | 62 | 23 | 20 | 8 | 48 | 22 | 19 | 7 |
| Southbound Left | - | 75 | 62 | 34 | 42 | 21 | 55 | 29 | 42 | 21 |
| Southbound Through | - | - | 43 | 22 | 44 | 25 | 41 | 20 | 42 | 24 |
| Southbound Through / Right | - | - | 35 | 15 | 33 | 14 | 32 | 12 | 32 | 13 |
| Regional Road 25 / Highway 401 Westbound Off-Ramp | Signal | - | - | - | - | - | - | - | - | - |
| Westbound Left | - | 80 (390) | 51 | 33 | 48 | 32 | 52 | 34 | 49 | 32 |
| Northbound Through | - | - | 41 | 21 | 49 | 27 | 46 | 24 | 47 | 24 |
| Southbound Through | - | - | 44 | 24 | 46 | 26 | 40 | 22 | 43 | 25 |
| Regional Road 25 / Highway 401 Eastbound Off-Ramp | Signal | - | - | - | - | - | - | - | - | - |
| Eastbound Left | - | 130 (470) | 141 | 94 | 58 | 31 | 154 | 99 | 57 | 29 |
| Eastbound Through / Right | - | - (470) | 100 | 43 | 49 | 30 | 167 | 57 | 46 | 28 |
| Eastbound Right | - | 130 (240) | 59 | 33 | 44 | 24 | 82 | 38 | 42 | 23 |
| Westbound Left / Through / Right | - | - | 26 | 12 | 25 | 12 | 24 | 12 | 27 | 13 |
| Northbound Through | - | - | 98 | 65 | 105 | 65 | 94 | 62 | 100 | 63 |
| Northbound Through / Right | - | - | 55 | 28 | 58 | 28 | 54 | 30 | 58 | 26 |

## 'MYin

| Intersection | Control Type | Available Storage (m) | Existing Haul Route |  |  |  | Future Haul Route |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | AM Peak Hour |  | PM Peak Hour |  | AM Peak Hour |  | PM Peak Hour |  |
| Turning Movement | - | - | 95 ${ }^{\text {th }} \%$ <br> Queue <br> (m) | 50 ${ }^{\text {th }} \%$ <br> Queue <br> (m) | 95 ${ }^{\text {th }} \%$ <br> Queue <br> (m) | 50 ${ }^{\text {th }} \%$ <br> Queue <br> (m) | 95 ${ }^{\text {th }} \%$ <br> Queue <br> (m) | 50 ${ }^{\text {th }} \%$ <br> Queue <br> (m) | 95 ${ }^{\text {th }} \%$ <br> Queue <br> (m) | $50^{\text {th }} \%$ <br> Queue <br> (m) |
| Southbound Left | - | 30 | 19 | 7 | 16 | 6 | 17 | 6 | 17 | 7 |
| Southbound Through | - | - | 73 | 46 | 57 | 35 | 71 | 46 | 59 | 35 |

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\text { Attachment } 7
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## 'Y/Lin

Table 42026 Future Traffic Operations - Roundabout Queues

| Intersection | Control Type | Available Storage (m) | Existing Haul Route |  |  |  | Future Haul Route |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | AM Peak Hour |  | PM Peak Hour |  | AM Peak Hour |  | PM Peak Hour |  |
| Turning Movement | - | - | $95^{\text {th }} \%$ <br> Queue (veh) | 95 ${ }^{\text {th }} \%$ <br> Queue <br> (m) | $95^{\text {th }} \%$ <br> Queue (veh) | 95 ${ }^{\text {th }} \%$ <br> Queue <br> (m) | 95 ${ }^{\text {th }} \%$ <br> Queue (veh) | 95 ${ }^{\text {th }} \%$ Queue (m) | 95 ${ }^{\text {th }} \%$ <br> Queue (veh) | 95 ${ }^{\text {th }} \%$ <br> Queue <br> (m) |
| Dublin Line / Tremaine Road at James Snow Parkway / Campbellville Road | Roundabout | - | - | - | - | - | - | - | - | - |
| James Snow Parkway (Westbound Approach) | - | - | 1.5 | 9 | 6.9 | 40 | 1.8 | 10 | 6.2 | 36 |
| Dublin Line (Southbound Approach) | - | - | 2.3 | 13 | 3.6 | 21 | 2.3 | 13 | 3.6 | 21 |
| Campbellville Road (Eastbound Approach) | - | - | 1.4 | 8 | 1.4 | 8 | 1.4 | 8 | 1.4 | 8 |
| Tremaine Road (Northbound Approach) |  | - | 1.2 | 7 | 0.5 | 3 | 1.4 | 8 | 1.2 | 7 |

